

模拟集成电路设计原理

(Principle of Analog Integrated Circuit Design, INF0130025.02)

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<http://rfic.fudan.edu.cn/Courses.htm>

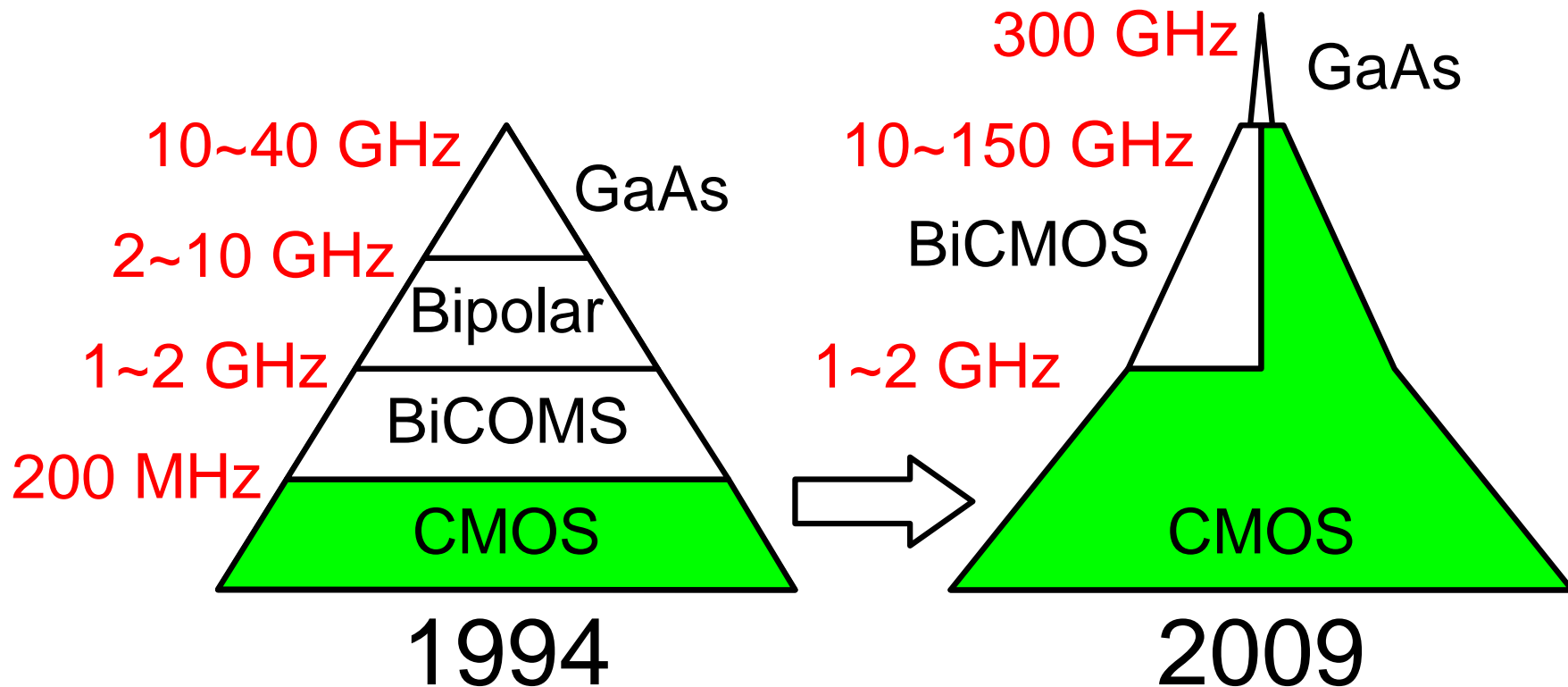
复旦大学/微电子学院/射频集成电路设计研究小组

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集成电路器件和模型

- pn结模型
- BJT型晶体管模型
- MOS型晶体管模型
- MOS型与BJT型晶体管的比较

从双极型到MOS晶体管

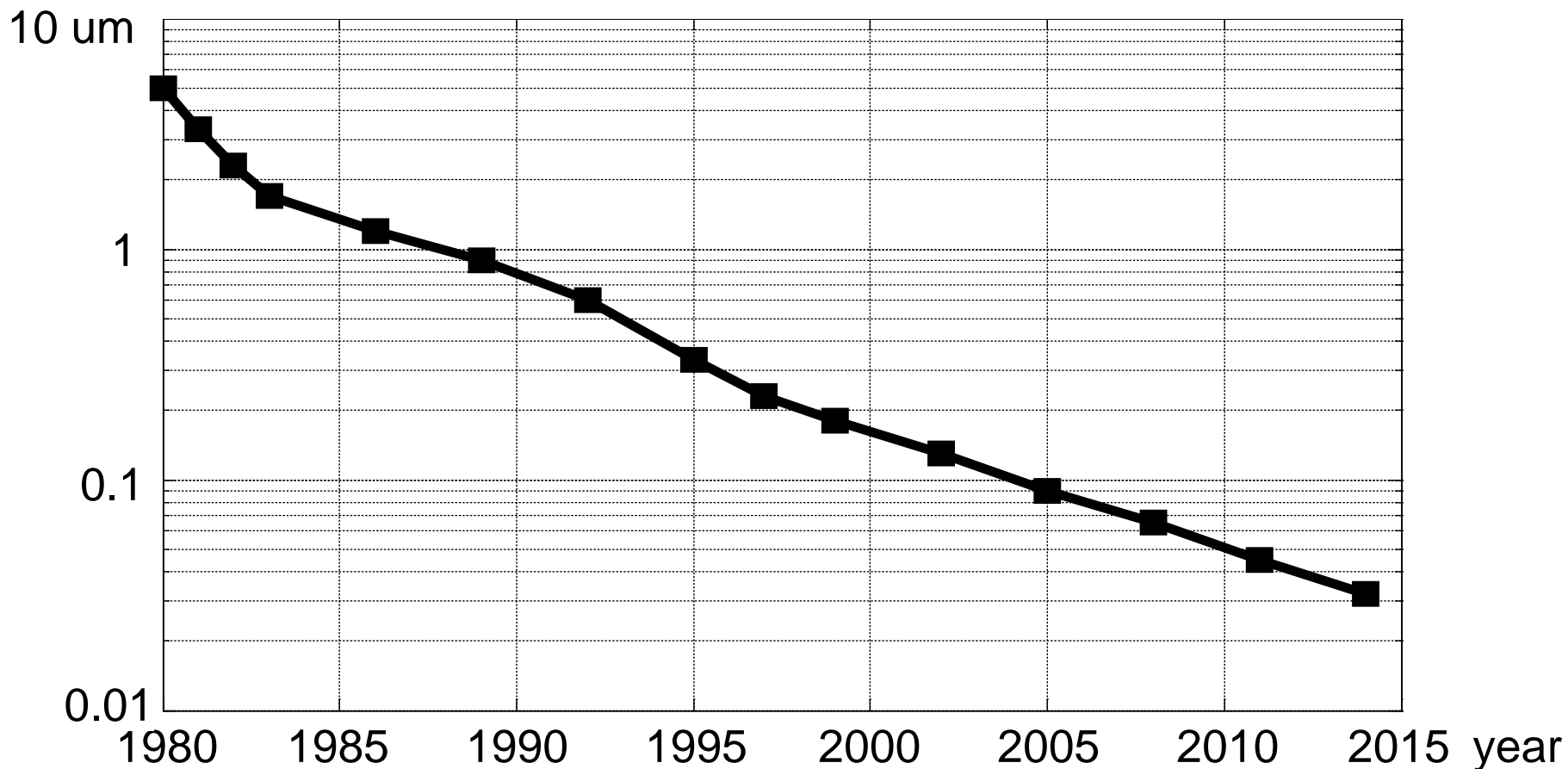


Ref.: Toshiba & ISSCC2009

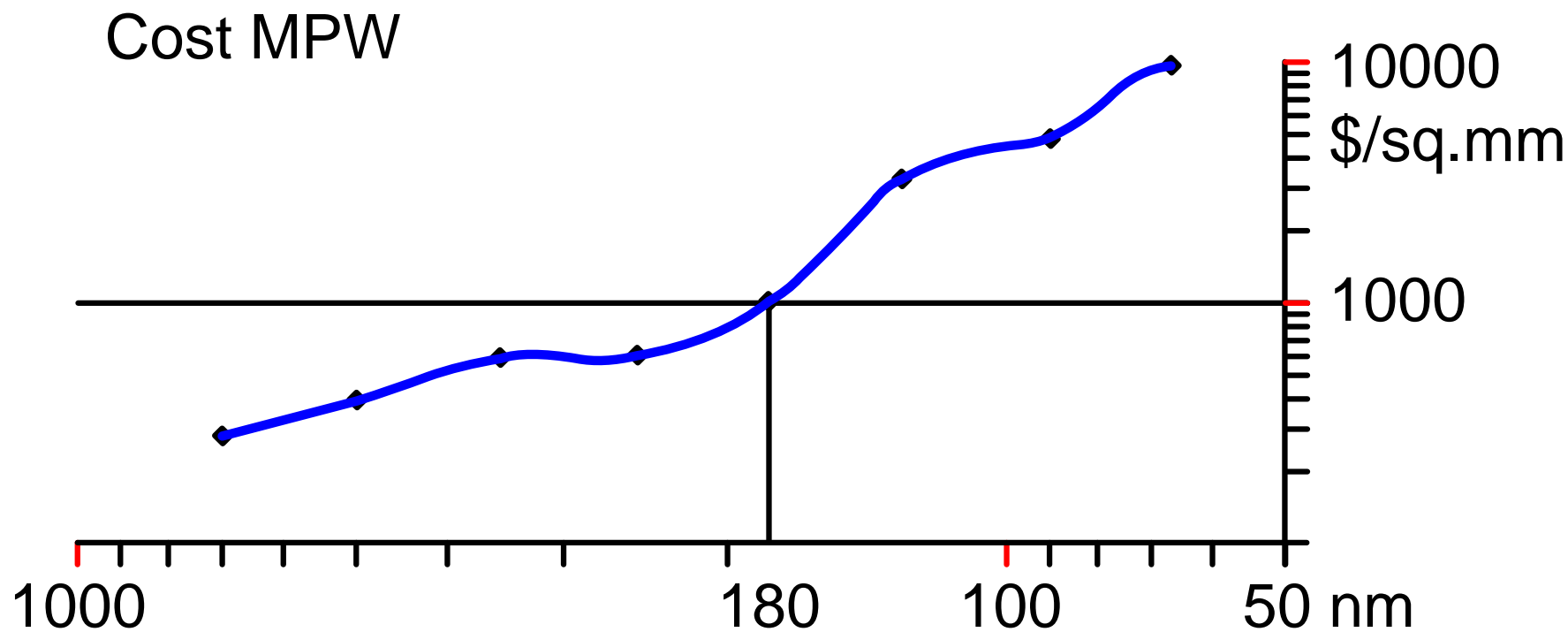
SIA线路图

Year	L_{\min} μm	Bits/chip Gb/chip	Trans/chip millions/chip	Clock MHz	Wiring
1995	0.35	0.064	4	300	4-5
1998	0.25	0.256	7	450	5
2001	0.18	1	13	600	5-6
2004	0.13	4	25	800	6
2007	0.09	16	50	1000	6-7
2010	0.065	64	90	1100	7-8
2013	0.045				
2016	0.032				

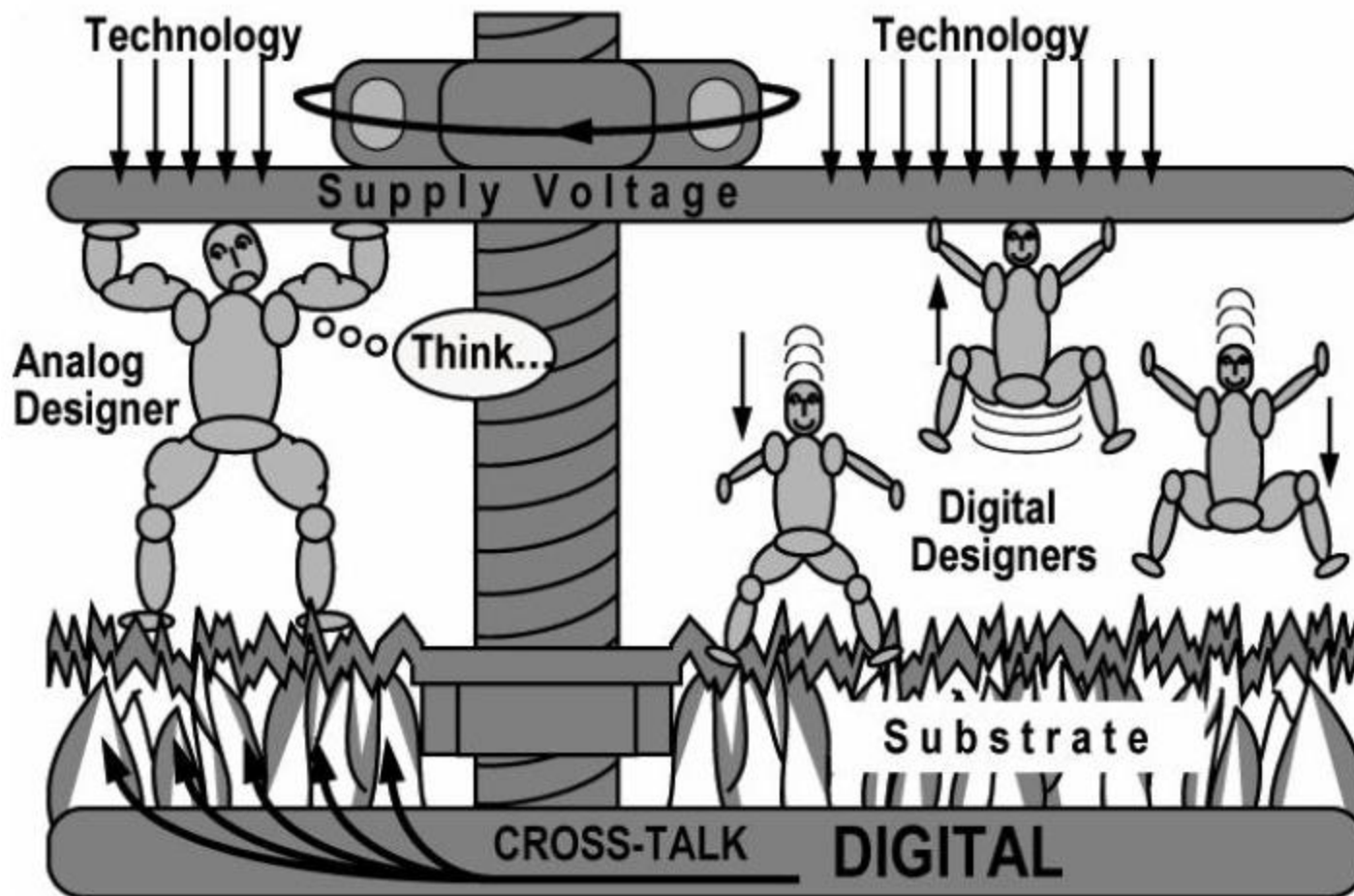
摩尔定律(The law of Moore)



使用不同特征尺寸的MPW价格

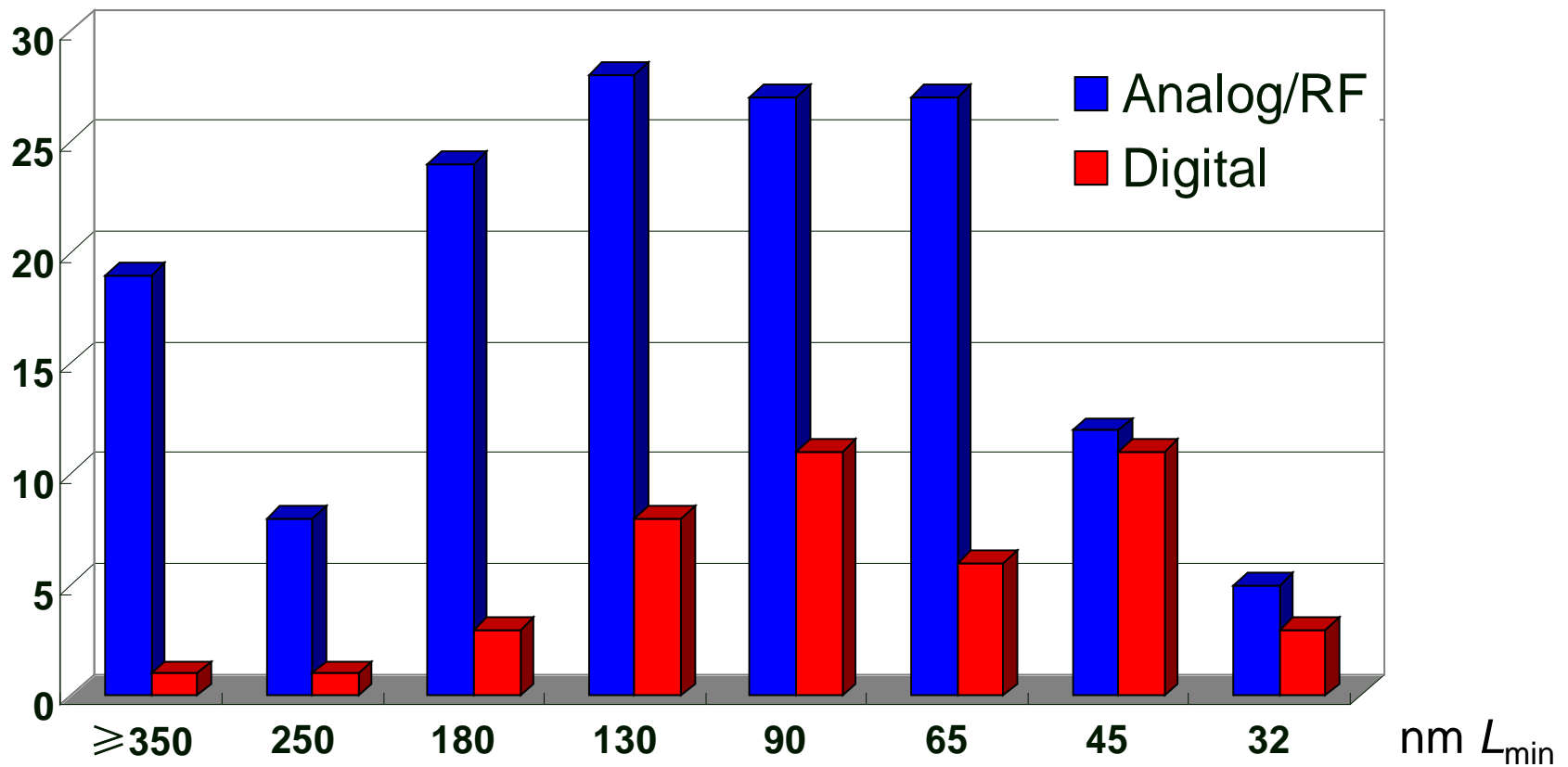


在深亚微米工艺下模拟设计的挑战



Ref.: SNUG2004, San Jose

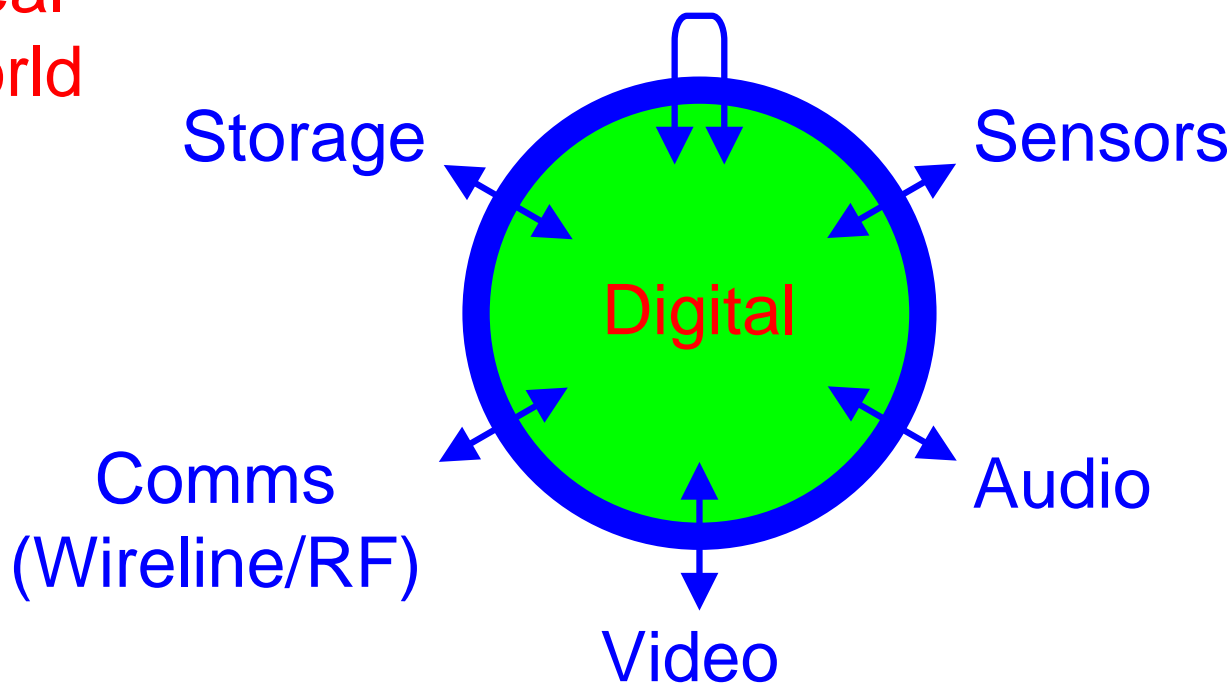
ISSCC 2009论文分布情况



混合信号 “蛋壳”

Analog
Real
World

High speed digital
(PLL, DLL)



Ref.: SNUG2004, San Jose

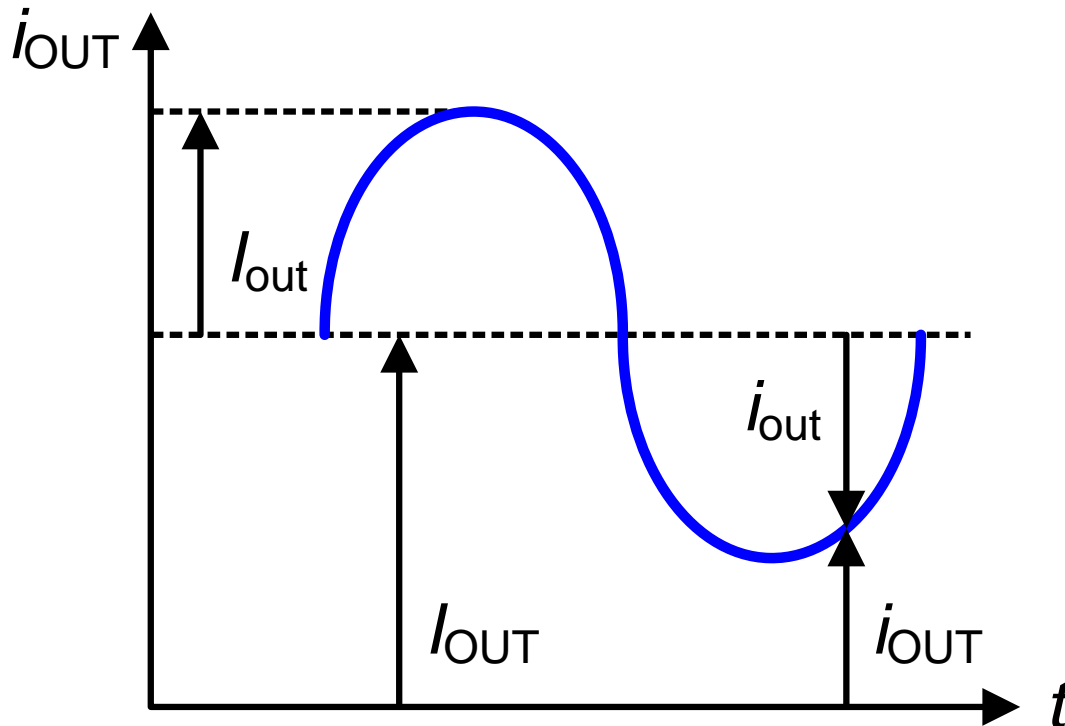
符号说明

i_{OUT} total instantaneous value

I_{OUT} DC or average value

I_{out} amplitude of AC value

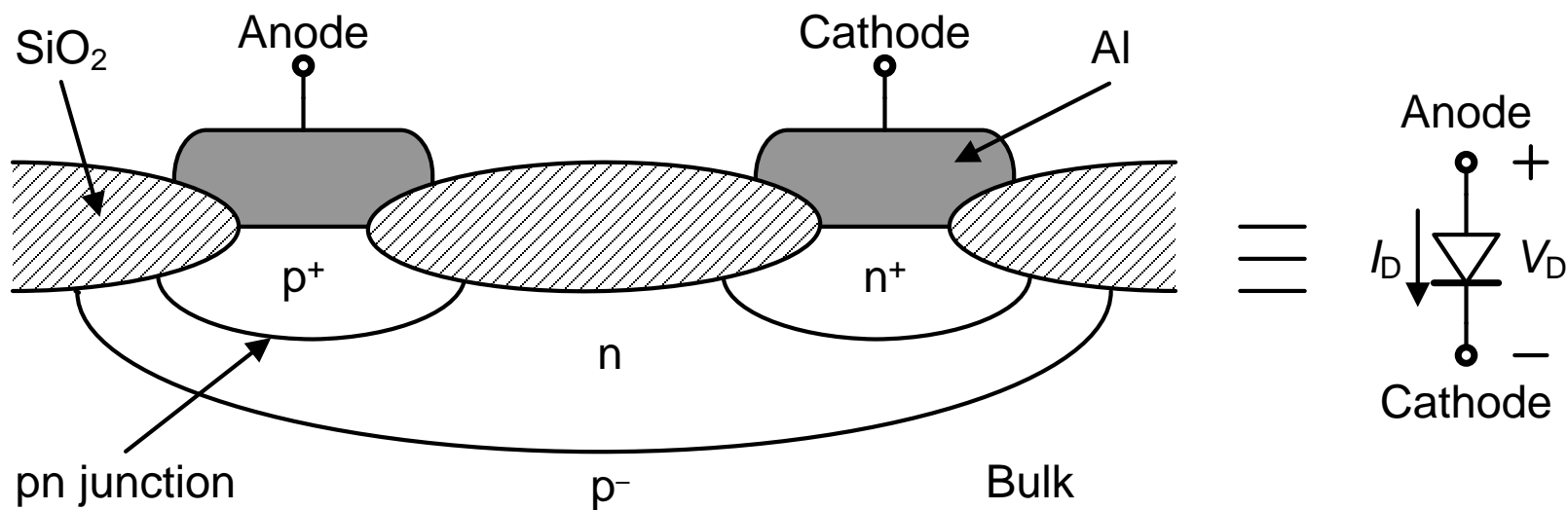
i_{out} instantaneous value of AC component



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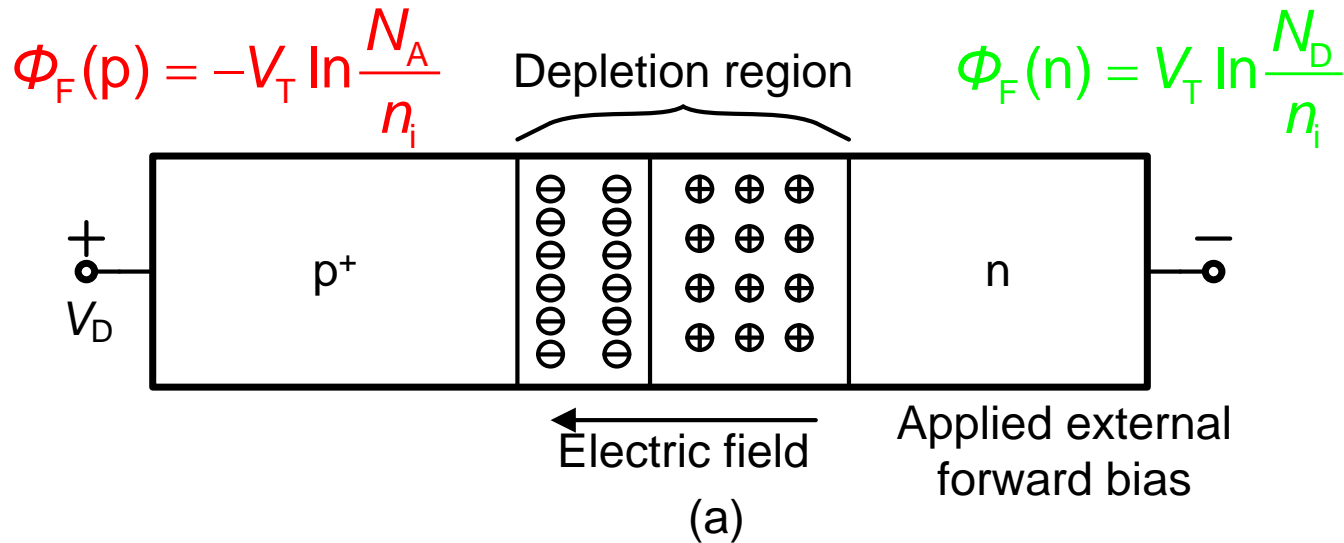
- pn结模型
 - 耗尽区宽度
 - 耗尽区电容
 - 击穿电压
 - I - V 关系曲线
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 - 小信号模型

pn结的剖面图和符号



A cross section of a pn junction.

正偏pn结示意图：突变结



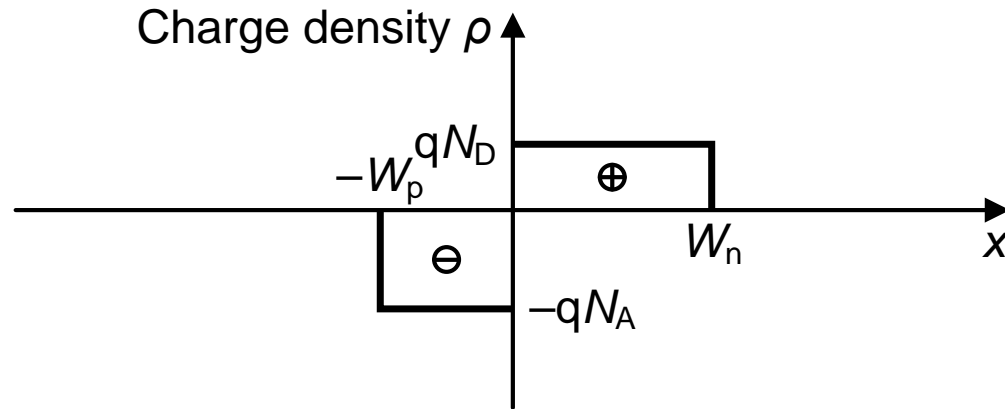
0 V偏压条件下，pn结中内建电势为：
$$\Phi_0 = V_T \ln \frac{N_A N_D}{n_i^2}$$

其中， n_i 为本征载流子浓度：
$$n_i = \sqrt{N_C N_V} e^{-\frac{E_g}{2kT}}$$

在300 K时，
$$V_T = \frac{kT}{q} \approx 26 \text{ mV}$$

$$n_i \approx 1.5 \times 10^{10} \text{ cm}^{-3}$$

空间电荷密度

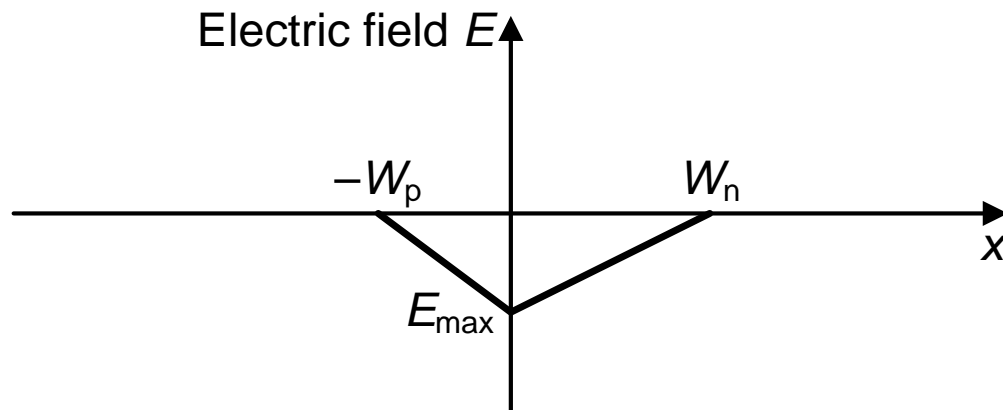


由电中性原则知，耗尽区内： $W_p N_A = W_n N_D$

由泊松方程，当 $-W_p < x < 0$ ， $\frac{d^2 V(x)}{dx^2} = -\frac{\rho}{\epsilon_{si}} = \frac{qN_A}{\epsilon_{si}}$

其中 $\epsilon_{si} = K_{si} \epsilon_0$ ，积分得： $E(x) = -\frac{dV(x)}{dx} = -\left(\frac{qN_A}{\epsilon_{si}} x + C_1\right)$

电场强度

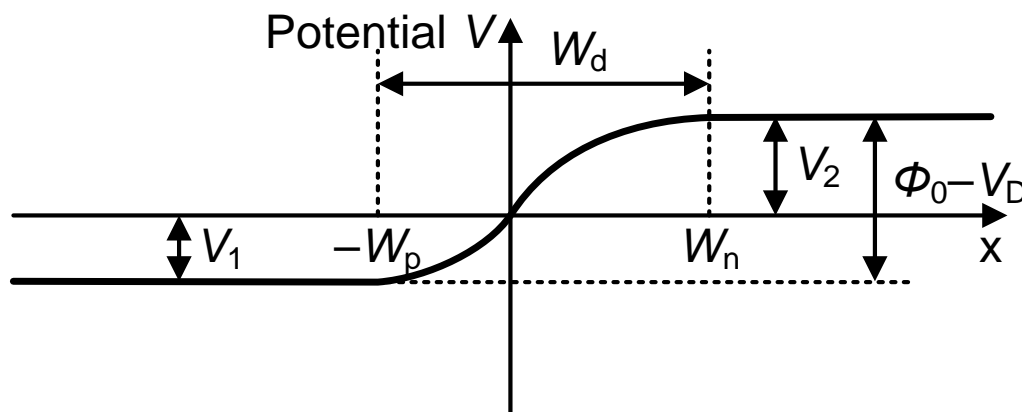


第一个边界条件 $E(-W_p)=0$,

$$E(x) = -\frac{qN_A}{\epsilon_{si}}(x + W_p) = -\frac{dV(x)}{dx}$$

$$V(x) = \frac{qN_A}{\epsilon_{si}} \left(\frac{x^2}{2} + W_p x \right) + C_2$$

静电势



第二个边界条件 $V(0)=0$,
$$V(x) = \frac{qN_A}{\epsilon_{si}} \left(\frac{x^2}{2} + W_p x \right)$$

令 $V(-W_p) = -V_1$,
$$V_1 = \frac{qN_A}{\epsilon_{si}} \frac{W_p^2}{2}$$

同理，从 $x=0$ 到 $x=W_n$ 的电压为 V_2 ,
$$V_2 = \frac{qN_D}{\epsilon_{si}} \frac{W_n^2}{2}$$

耗尽区宽度

pn结上的总静电势为：

$$\phi_0 - V_D = V_1 + V_2 = \frac{q}{2\epsilon_{\text{si}}} (N_A W_p^2 + N_D W_n^2) = \frac{q W_p^2 N_A}{2\epsilon_{\text{si}}} \left(1 + \frac{N_A}{N_D} \right)$$

耗尽区总宽度：

$$W_d = W_p + W_n = \left[\frac{2\epsilon_{\text{si}} (N_A + N_D)}{q N_A N_D} \right]^{1/2} (\phi_0 - V_D)^{1/2}$$

其中，p型区和n型区的宽度分别为：

$$W_p = \left[\frac{2\epsilon_{\text{si}} (\phi_0 - V_D)}{q N_A \left(1 + \frac{N_A}{N_D} \right)} \right]^{1/2} \quad W_n = \left[\frac{2\epsilon_{\text{si}} (\phi_0 - V_D)}{q N_D \left(1 + \frac{N_D}{N_A} \right)} \right]^{1/2}$$

例题1:

一个硅材料pn结的掺杂浓度 $N_A=10^{16}$ 原子/cm³和 $N_D=10^{17}$ 原子/cm³，在10 V反偏电压下，计算结的内建势和耗尽区宽度。

解：在300K时，内建势：

$$\phi_0 = V_T \ln \frac{N_A N_D}{n_i^2} = 0.026 \ln \frac{10^{16} \times 10^{17}}{2.25 \times 10^{20}} = 757 \text{ mV}$$

p型区的耗尽区宽度

$$W_p = \left[\frac{2\epsilon_{\text{si}} (\phi_0 - V_D)}{qN_A \left(1 + \frac{N_A}{N_D}\right)} \right]^{1/2} = \left[\frac{2 \times 1.04 \times 10^{-12} \times 10.757}{1.6 \times 10^{-19} \times 10^{16} \times 1.1} \right]^{1/2} = 1.1 \times 10^{-4} \text{ cm} = 1.1 \mu\text{m}$$

n型区的耗尽区宽度 $W_n = W_p (N_A / N_D) = 0.11 \mu\text{m}$

耗尽区内的固定电荷

$$Q_j = Q^+ = Q^- = qN_D W_n = \left[\frac{2qN_D \epsilon_{si} (\Phi_0 - V_D)}{\left(1 + \frac{N_D}{N_A}\right)} \right]^{1/2}$$

当 $N_A \gg N_D$ 时 $Q_j \approx [2q\epsilon_{si} (\Phi_0 - V_D) N_D]^{1/2}$

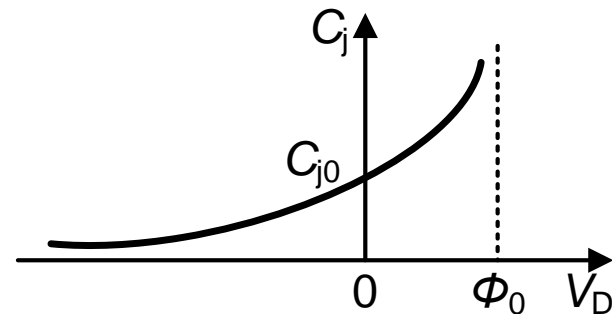
耗尽电容

$$C_j = \left| \frac{dQ_j}{dV_D} \right| = \left[\frac{q\epsilon_{si}}{2(\phi_0 - V_D)} \frac{N_A N_D}{N_A + N_D} \right]^{1/2} = \frac{\epsilon_{si}}{W_d} = \boxed{\frac{C_{j0}}{\sqrt{1 - \frac{V_D}{\phi_0}}}}$$

其中，
$$C_{j0} = \sqrt{\frac{q\epsilon_{si}}{2\phi_0} \frac{N_A N_D}{N_A + N_D}}$$

当 $N_A \gg N_D$ 时，
$$C_{j0} \approx \sqrt{\frac{q\epsilon_{si} N_D}{2\phi_0}}$$

$$Q_j \approx 2C_{j0} \phi_0 \sqrt{1 - \frac{V_D}{\phi_0}}$$



Depletion capacitance as a function of externally applied junction voltage

例题2:

一个硅材料pn结的掺杂浓度 $N_A=10^{16}$ 原子/cm³和 $N_D=10^{17}$ 原子/cm³，计算面积 $10\ \mu\text{m} \times 10\ \mu\text{m}$ 的pn结在0 V偏压下的耗尽电容？在3 V反偏电压下，pn结耗尽电容是多少？

解：0 V偏压下，面耗尽电容为，

$$C_{j0} = \sqrt{\frac{q\epsilon_{\text{si}}}{2\Phi_0} \frac{N_A N_D}{N_A + N_D}} = \sqrt{\frac{1.6 \times 10^{-19} \times 1.04 \times 10^{-12} \times 10^{17}}{2 \times 0.757 \times 11}}$$

$$= 3.16 \times 10^{-8} \text{ F/cm}^2 = 0.316 \text{ fF}/\mu\text{m}^2$$

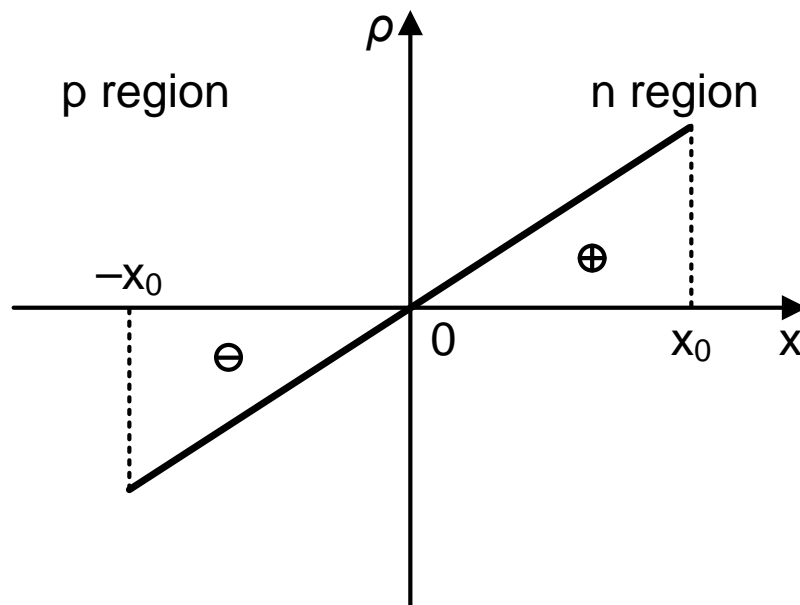
面积 $10\ \mu\text{m} \times 10\ \mu\text{m}$ 的pn结的耗尽电容为31.6 fF

3 V反偏电压下，耗尽电容为，

$$C_{T,j} = \frac{C_{T,j0}}{\sqrt{1 - \frac{V_D}{\Phi_0}}} = \frac{3.16 \text{ fF}}{\sqrt{1 - \frac{-3}{0.757}}} = 1.42 \text{ fF}$$

练习1：缓变pn结

缓变pn结的掺杂浓度梯度为 a ，请推导缓变pn结的空间电荷和耗尽电容。



Space charge density in a linearly graded pn junction

击穿电压

耗尽区内的最大电场：
$$E_{\max} = -\frac{qN_A}{\epsilon_{\text{si}}} W_p$$

当忽略 Φ_0 ，
$$|E_{\max}| \approx \left[\frac{2qN_A N_D V_D}{\epsilon_{\text{si}} (N_A + N_D)} \right]^{1/2}$$

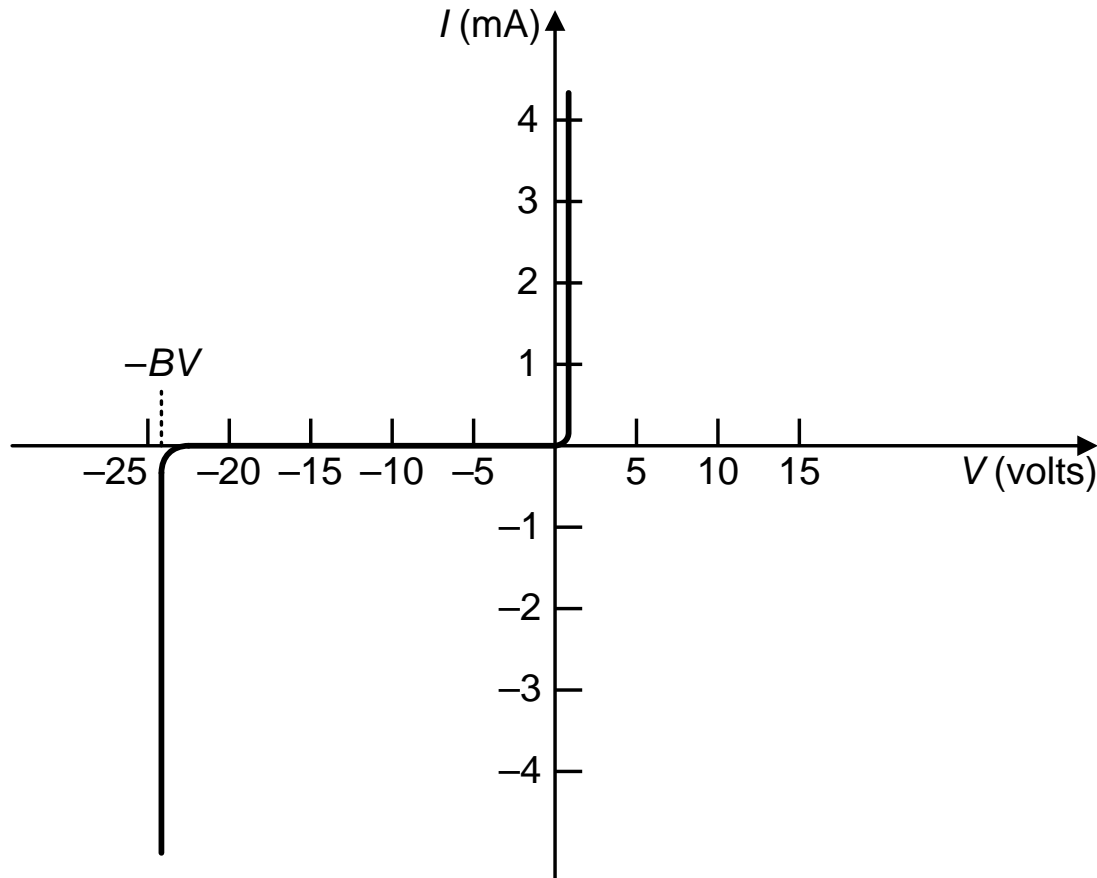
击穿时的临界电场为 E_{crit} ，则击穿电压为：

$$BV = \frac{\epsilon_{\text{si}} (N_A + N_D)}{2qN_A N_D} E_{\text{crit}}^2$$

当 $N_A \gg N_D$ 时，

$$BV \approx \frac{\epsilon_{\text{si}} E_{\text{crit}}^2}{2qN_D}$$

击穿电压反偏电流



击穿电压附近的反偏电流为：

$$I_{RA} = M I_R$$

其中 I_R 为pn结正常反偏电流， M 为倍增因子， $n=3\sim 6$

$$M = \frac{1}{1 - \left(\frac{-V_D}{BV} \right)^n}$$

Typical I - V characteristic of a junction diode showing avalanche breakdown

例题2:

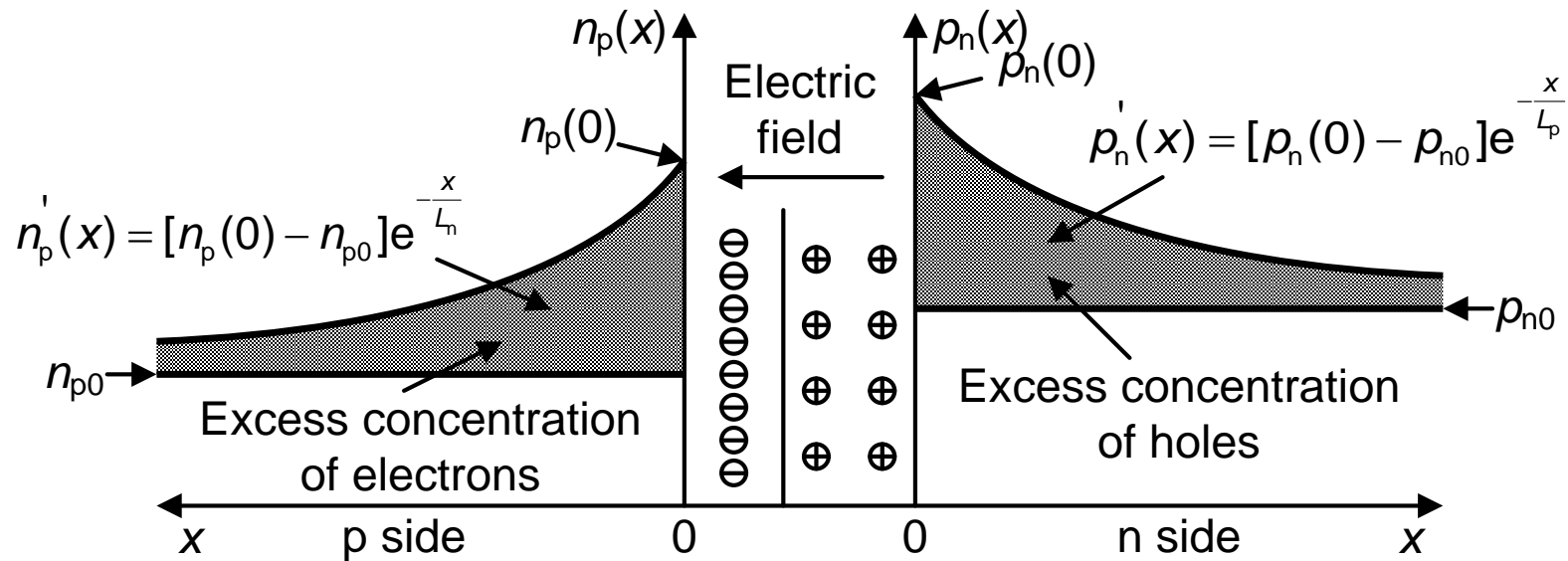
一个硅材料pn结的掺杂浓度 $N_A=10^{16}$ 原子/cm³和 $N_D=10^{17}$ 原子/cm³，假设临界电场 $E_{\text{crit}}=3 \times 10^5$ V/cm，计算击穿电压。

解：击穿电压：

$$BV = \frac{\epsilon_{\text{si}}(N_A + N_D)}{2qN_A N_D} E_{\text{crit}}^2 = \frac{1.04 \times 10^{-12} \times 11}{2 \times 1.6 \times 10^{-19} \times 10^{17}} \times 9 \times 10^{10}$$

$$= 32 \text{ V}$$

pn结中少数载流子分布图



Impurity concentration profile for diffused pn junction

p型和n型半导体中的少子浓度分别为：

$$n_p(0) = n_{p0} e^{\frac{V_D}{V_T}}$$

$$p_n(0) = p_{n0} e^{\frac{V_D}{V_T}}$$

非平衡少子的扩散

非平衡少子与扩散的距离之间是指数关系：

n型区的空穴：

$$p_n'(x) = p_n'(0)e^{-\frac{x}{L_p}} = [p_n(0) - p_{n0}]e^{-\frac{x}{L_p}} = p_{n0}(e^{\frac{V_D}{V_T}} - 1)e^{-\frac{x}{L_p}}$$

p型区的电子：

$$n_p'(x) = n_p'(0)e^{-\frac{x}{L_n}} = [n_p(0) - n_{p0}]e^{-\frac{x}{L_n}} = n_{p0}(e^{\frac{V_D}{V_T}} - 1)e^{-\frac{x}{L_n}}$$

其中 L_p 和 L_n 分别是n型和p型中空穴和电子的扩散长度。

$$p_n'(x) = p_n(x) - p_{n0}$$

$$n_p'(x) = n_p(x) - n_{p0}$$

非平衡少子的扩散电流密度

n型区的空穴:

$$J_p(0) = -qD_p \left. \frac{dp_n'(x)}{dx} \right|_{x=0} = \frac{qD_p p_{n0}}{L_p} \left(e^{\frac{V_D}{V_T}} - 1 \right)$$

p型区的电子:

$$J_n(0) = -qD_n \left. \frac{dn_p'(x)}{dx} \right|_{x=0} = \frac{qD_n n_{p0}}{L_n} \left(e^{\frac{V_D}{V_T}} - 1 \right)$$

其中， D_n 和 D_p 分别是电子和空穴扩散系数

pn结的总电流密度

$$J(0) = J_p(0) + J_n(0) = q \left(\frac{D_p p_{n0}}{L_p} + \frac{D_n n_{p0}}{L_n} \right) \left(e^{\frac{V_D}{V_T}} - 1 \right)$$

I-V关系曲线

横切面积为A的pn结电流:

$$\begin{aligned}
 I_D &= AJ_n(0) = qA \left(\frac{D_p p_{n0}}{L_p} + \frac{D_n n_{p0}}{L_n} \right) \left(e^{\frac{V_D}{V_T}} - 1 \right) \\
 &= qA \left(\frac{D_p n_i^2}{L_p N_D} + \frac{D_n n_i^2}{L_n N_A} \right) \left(e^{\frac{V_D}{V_T}} - 1 \right) = I_s \left(e^{\frac{V_D}{V_T}} - 1 \right)
 \end{aligned}$$

其中 I_s 为pn结反向饱和电流，为常数。

非平衡少数载流子电荷

n型区的空穴:

$$Q_p = qA \int_0^\infty p'_n(x) dx = qA \int_0^\infty [p_n(0) - p_{n0}] e^{-\frac{x}{L_p}} dx$$

$$= qAL_p [p_n(0) - p_{n0}] = \frac{qAL_p n_i^2}{N_D} (e^{\frac{V_D}{V_T}} - 1)$$

p型区的电子:

$$Q_n = qA \int_0^\infty n'_p(x) dx = qA \int_0^\infty [n_p(0) - n_{p0}] e^{-\frac{x}{L_n}} dx$$

$$= qAL_n [n_p(0) - n_{p0}] = \frac{qAL_n n_i^2}{N_A} (e^{\frac{V_D}{V_T}} - 1)$$

扩散电容

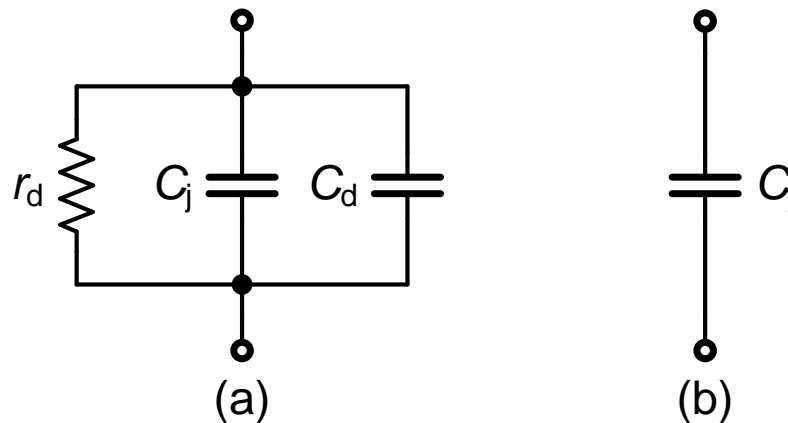
$$C_d = \frac{dQ_d}{dV_D} = \frac{d(Q_n + Q_p)}{dV_D} = \frac{qAn_i^2}{V_T} e^{\frac{V_D}{V_T}} \left(\frac{L_n}{N_A} + \frac{L_p}{N_D} \right)$$

$$\approx \frac{I_D}{V_T} \frac{L_n^2 L_p + L_p^2 L_n \frac{N_A}{N_D}}{L_p D_n + L_n D_p \frac{N_A}{N_D}}$$

重掺杂一侧少子的电荷存储可以忽略，假设n区重掺杂， $N_D \gg N_A$ ，扩散电荷 $Q_d \approx Q_n$ ：其中 τ_T 为二极管的渡越时间

$$C_d \approx \frac{L_n^2}{D_n} \frac{I_D}{V_T} = \tau_T \frac{I_D}{V_T}$$

pn结的小信号模型



The small-signal model for a junction.
(a) forward bias. (b) reverse bias.

正偏输出阻抗 r_d

$$\frac{1}{r_d} = \frac{dI_D}{dV_D} = I_s \frac{e^{V_D/V_T}}{V_T} \approx \frac{I_D}{V_T}$$

$$C_d = \frac{\tau_T}{r_d}$$

例题3:

二极管的渡越时间为100 pS，正向偏置电流为1 mA，问其小信号输出阻抗和扩散电容分别是多少？

解：

小信号是输出阻抗：

$$r_d = \frac{V_T}{I_D} = \frac{26 \text{ mV}}{1 \text{ mA}} = 26 \Omega$$

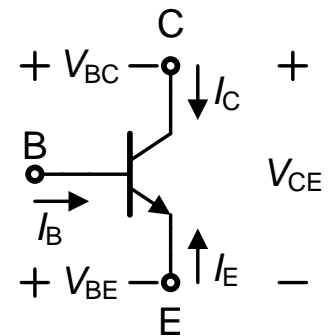
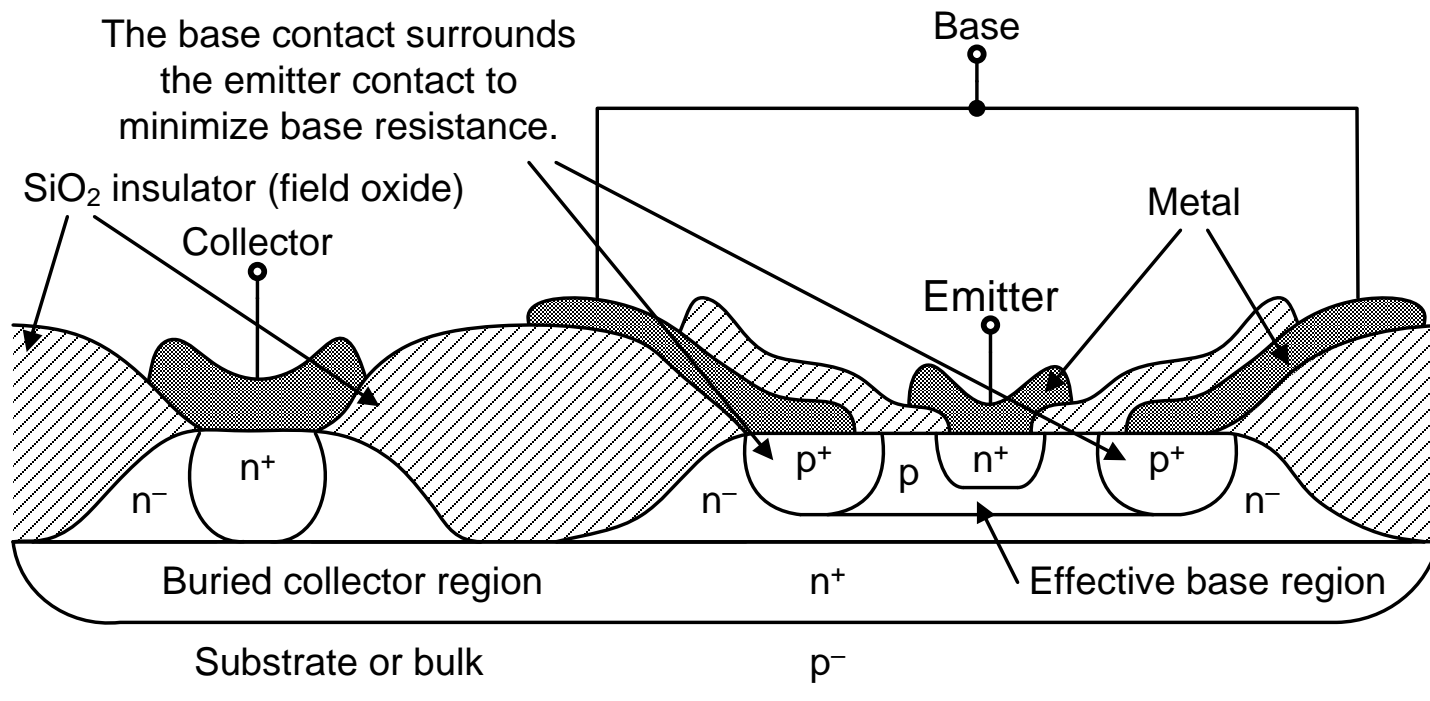
扩散电容：

$$C_d = \frac{\tau_T}{r_d} = \frac{100 \text{ pS}}{26 \Omega} = 3.8 \text{ pF}$$

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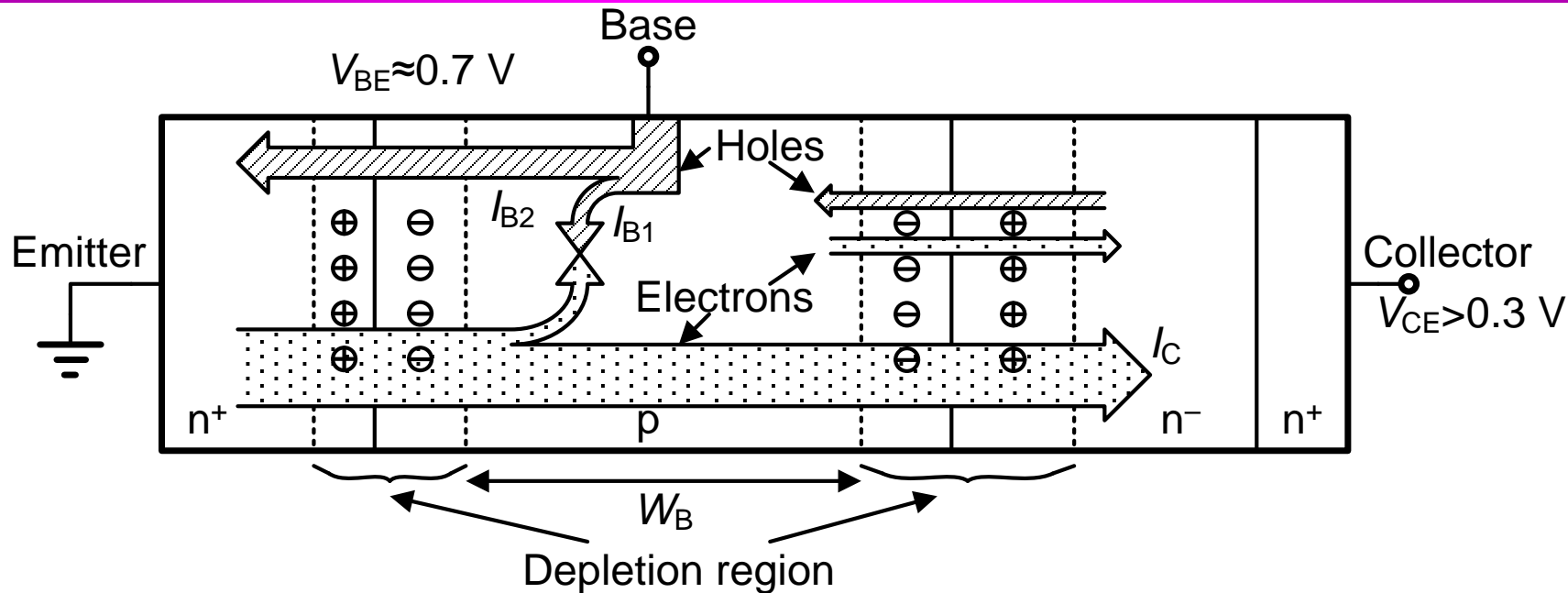
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 - 厄利效应
 - 饱和区和反向工作区
 - 击穿电压
 - 电流增益 β_F 与工作条件的关系
 - 小信号模型
 - 低频小信号模型
 - 高频小信号模型
 - 模拟评价指标
 - 器件模型概要

BJT型晶体管的剖面图和符号



A cross section of an npn bipolar-junction transistor.

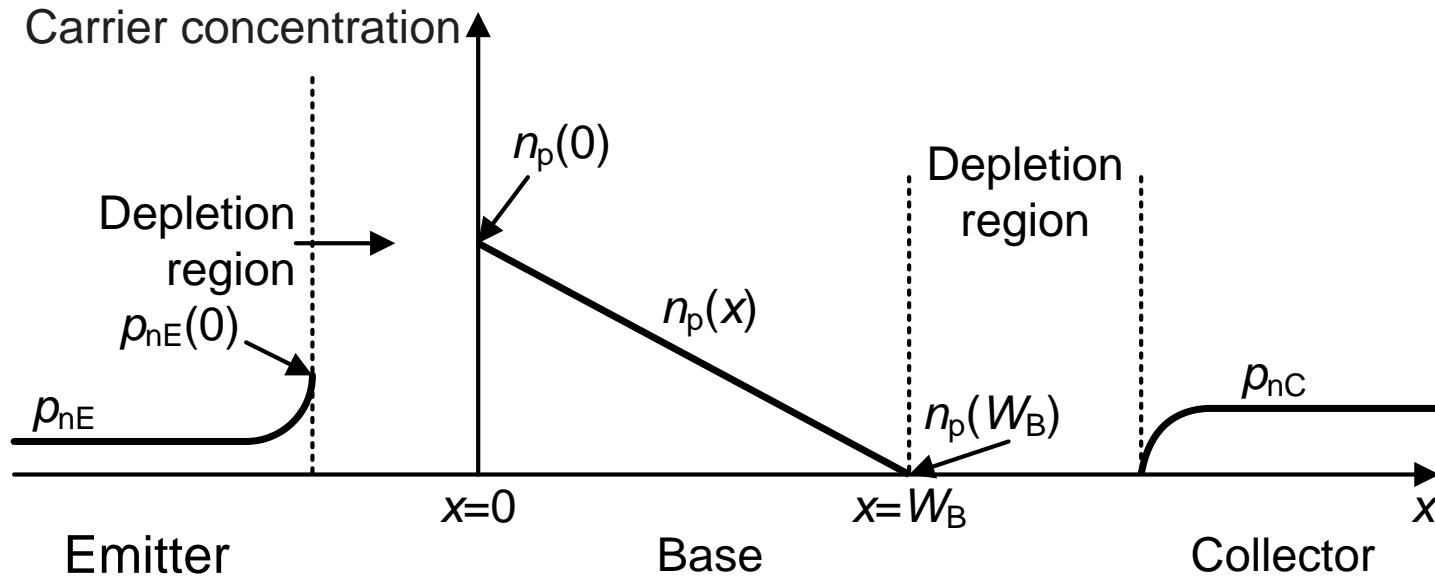
nnp型BJT晶体管的电流



Various components of the currents of an npn transistor.

发射结正偏，集电结反偏

少数载流子浓度分布图



Carrier concentrations along the cross section

基区中耗尽区边缘的少数载流子浓度:

$$n_p(0) = n_{p0} e^{\frac{V_{BE}}{V_T}} \quad n_p(W_B) = n_{p0} e^{\frac{V_{BC}}{V_T}} \approx 0$$

集电极电流

基区中电子引起的扩散电流密度：

$$J_n = qD_n \frac{dn_p(x)}{dx} = -qD_n \frac{n_p(0)}{W_B}$$

集电极电流：

$$I_C = qAD_n \frac{n_p(0)}{W_B} = \frac{qAD_n n_{p0}}{W_B} e^{\frac{V_{BE}}{V_T}} = I_S e^{\frac{V_{BE}}{V_T}}$$

其中 A 为发射区面积， I_S 为基极-发射极结反向饱和电流

$$I_S = \frac{qAD_n n_{p0}}{W_B} = \frac{qAD_n n_i^2}{W_B N_B} = \frac{qA \overline{D_n} n_i^2}{Q_B} \quad n_{p0} = \frac{n_i^2}{N_B}$$

$Q_B (=W_B N_B)$ 是基区中单位面积的掺杂原子数，

$\overline{D_n}$ 是电子平均扩散系数。

基极电流之一：复合电流

基区中少数载流子电荷为：

$$Q_e = \frac{1}{2} n_p(0) W_B q A$$

基极复合电流为：

$$I_{B1} = \frac{Q_e}{\tau_b} = \frac{1}{2} \frac{n_p(0) W_B q A}{\tau_b} = \frac{1}{2} \frac{n_{p0} W_B q A}{\tau_b} e^{\frac{V_{BE}}{V_T}}$$

其中 τ_b 是基区中少数载流子的存活时间。

基极电流之二：发射区的空穴电流

由基区注入发射区的空穴所引起扩散电流的：

$$I_{B2} = \frac{qAD_p}{L_p} p_{nE}(0) = \frac{qAD_p}{L_p} p_{nE0} e^{\frac{V_{BE}}{V_T}} = \frac{qAD_p}{L_p} \frac{n_i^2}{N_E} e^{\frac{V_{BE}}{V_T}}$$

其中 L_p 是空穴在发射区的扩散长度， D_p 是空穴的扩散系数。 $p_{nE}(0)$ 是发射区耗尽层边缘的空穴浓度。

基极总电流：

$$I_B = I_{B1} + I_{B2} = \left(\frac{1}{2} \frac{n_{p0} W_B q A}{\tau_b} + \frac{qAD_p}{L_p} \frac{n_i^2}{N_E} \right) e^{\frac{V_{BE}}{V_T}}$$

共射极电流增益

正向放大区的电流增益：

典型值为50~500

$$\beta_F = \frac{I_C}{I_B} = \frac{\frac{qAD_n n_{p0}}{W_B}}{\frac{1}{2} \frac{n_{p0} W_B qA}{\tau_b} + \frac{qAD_p n_i^2}{L_p N_E}} = \frac{1}{\frac{W_B^2}{2\tau_b D_n} + \frac{D_p}{D_n} \frac{W_B}{L_p} \frac{N_B}{N_E}}$$

发射极与基极和集电极电流关系：

$$I_E = -(I_C + I_B) = -\left(I_C + \frac{I_C}{\beta_F}\right) = -\frac{I_C}{\alpha_F}$$

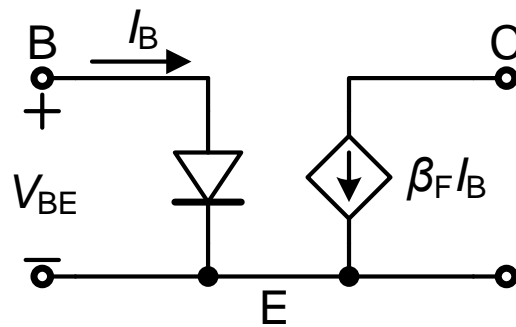
共基极电流增益

$$\alpha_F = -\frac{I_C}{I_E} = \frac{\beta_F}{1 + \beta_F} = \frac{1}{1 + \frac{1}{\beta_F}} = \frac{1}{1 + \frac{W_B^2}{2\tau_b D_n} + \frac{D_p}{D_n} \frac{W_B}{L_p} \frac{N_B}{N_E}} \approx \alpha_T \gamma$$

基区输运系数:
$$\alpha_T = \frac{1}{1 + \frac{W_B^2}{2\tau_b D_n}}$$

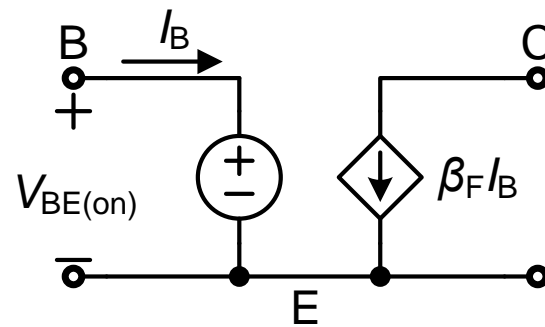
发射极注入效率:
$$\gamma = \frac{1}{1 + \frac{D_p}{D_n} \frac{W_B}{L_p} \frac{N_B}{N_E}}$$

大信号模型



$$I_B = \frac{I_S}{\beta_F} e^{\frac{V_{BE}}{V_T}}$$

(a)



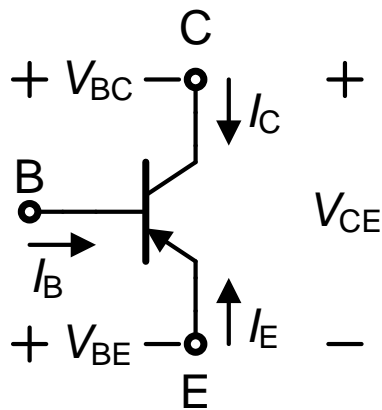
(b)

Large-signal models of npn transistors for use in bias calculations.

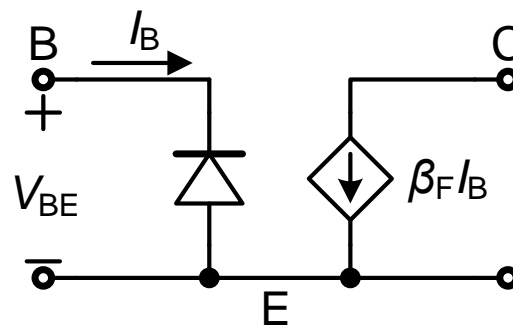
(a) Circuit incorporating an input diode.

(b) Simplified circuit with an input voltage source.

pnp型BJT晶体管的大信号模型

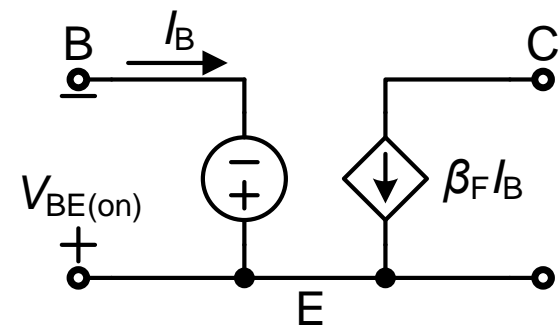


(a)



$$I_B = -\frac{I_S}{\beta_F} e^{-\frac{V_{BE}}{V_T}}$$

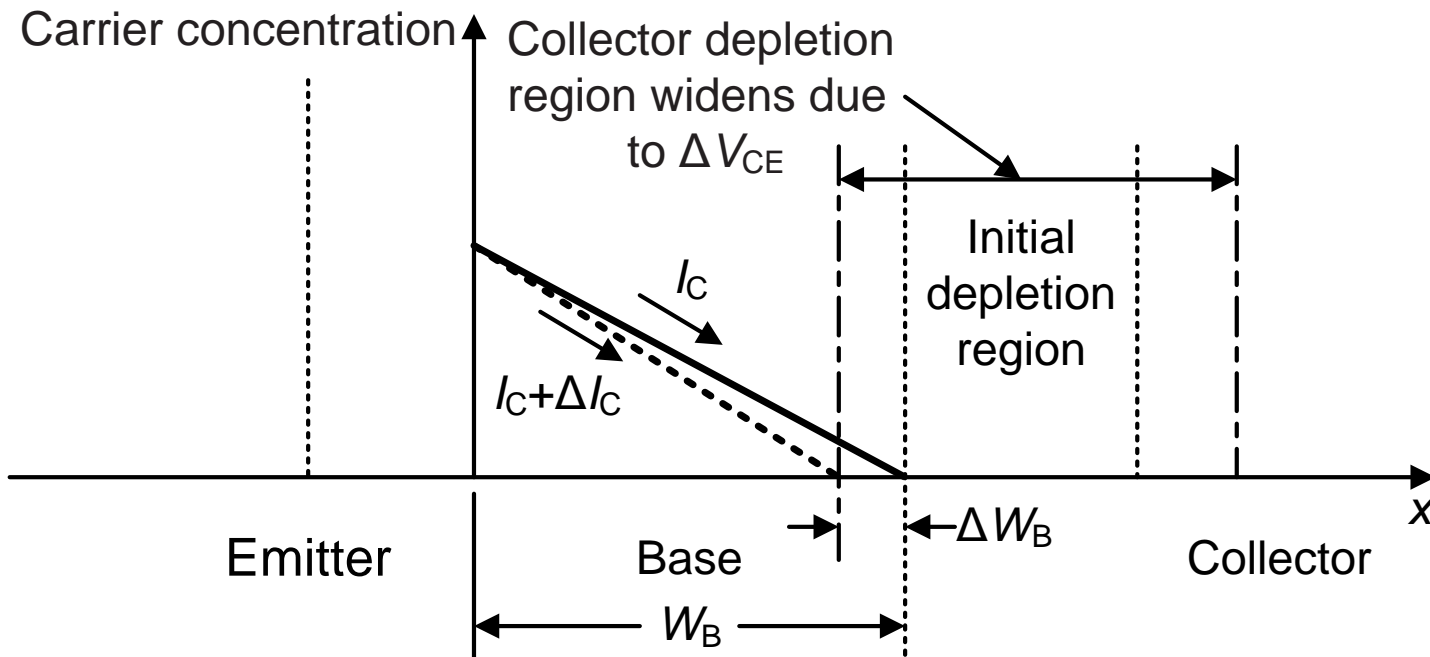
(b)



(c)

(a) pnp Bipolar transistor sign convention. (b),(c) Large-signal models of pnp transistors corresponding to npn transistors

厄利效应：(1)



Effect of increases in V_{CE} on the collector depletion region and base width of a bipolar transistor.

集电极电流:

$$I_C = \frac{qAD_n \bar{n}_i^2}{Q_B} e^{\frac{V_{BE}}{V_T}}$$

厄利效应：(2)

$$\frac{\partial I_C}{\partial V_{CE}} = -\frac{qAD_n \bar{n}_i^2}{Q_B^2} e^{\frac{V_{BE}}{V_T}} \frac{dQ_B}{dV_{CE}} = -\frac{I_C}{Q_B} \frac{dQ_B}{dV_{CE}}$$

对于一个均匀掺杂基区晶体管 $Q_B = W_B N_B$ ，且 V_{BE} 固定时

$$\frac{\partial I_C}{\partial V_{CE}} = -\frac{I_C}{W_B} \frac{dW_B}{dV_{CE}}$$

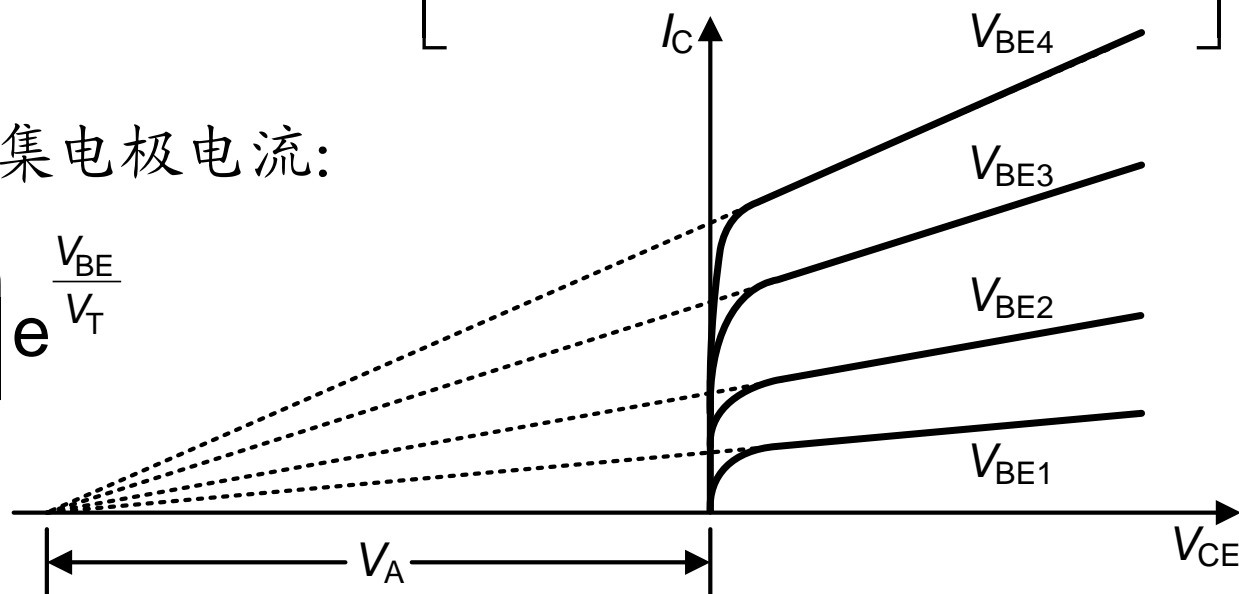
$$\left| \frac{dW_B}{dV_{CE}} \right| = \left| \frac{dW_B}{dV_{CB}} \right| = \left[\frac{\epsilon_{si}}{2qN_B \left(1 + \frac{N_B}{N_C} \right) (\phi_0 + V_{CB})} \right]^{1/2}$$

厄利电压

$$V_A = \frac{I_C}{\frac{\partial I_C}{\partial V_{CE}}} = -W_B \frac{dV_{CE}}{dW_B} = -W_B \left[\frac{2qN_B \left(1 + \frac{N_B}{N_C} \right) (\Phi_0 + V_{CB})}{\epsilon_{Si}} \right]^{1/2}$$

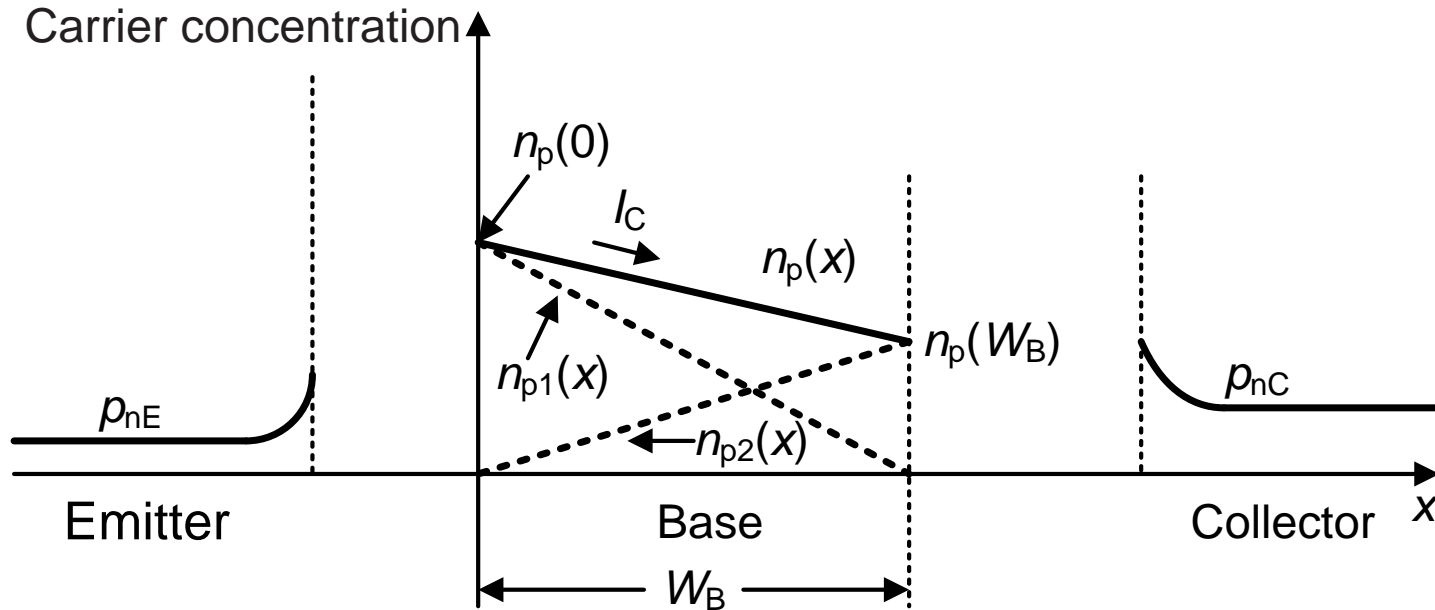
考虑厄利效应的集电极电流:

$$I_C = I_S \left(1 + \frac{V_{CE}}{V_A} \right) e^{\frac{V_{BE}}{V_T}}$$



Bipolar transistor output characteristics showing the Early voltage, V_A

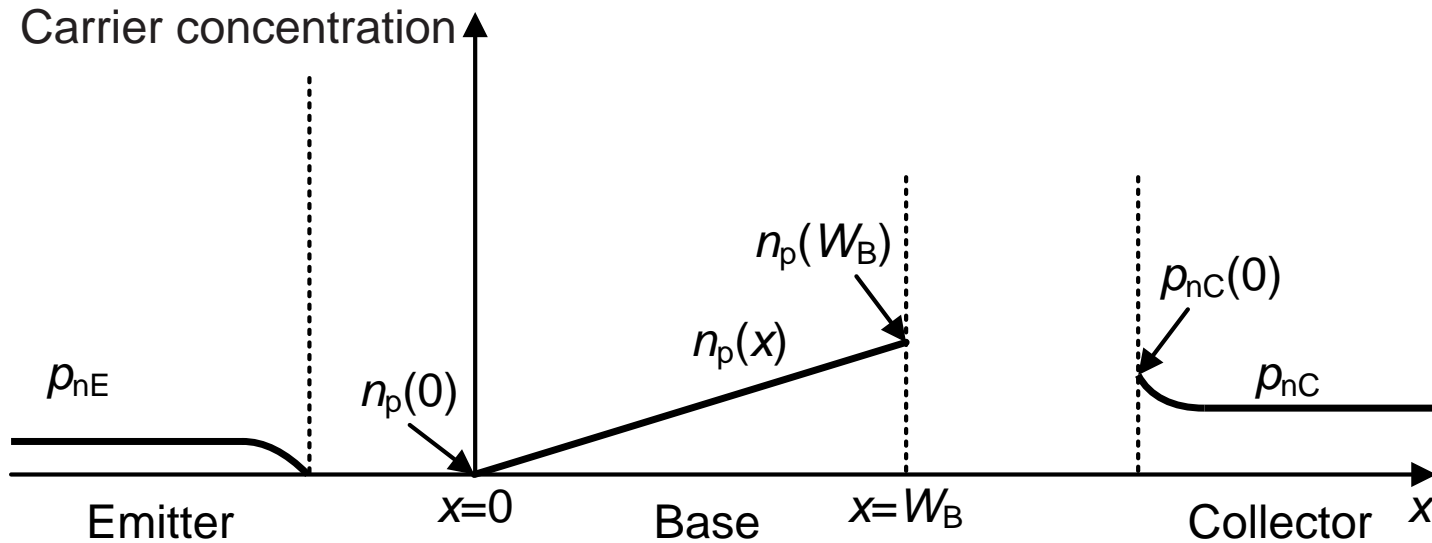
饱和区



Carrier concentrations in a saturated npn transistor. (Not to scale.)

发射结正偏，集电结正偏

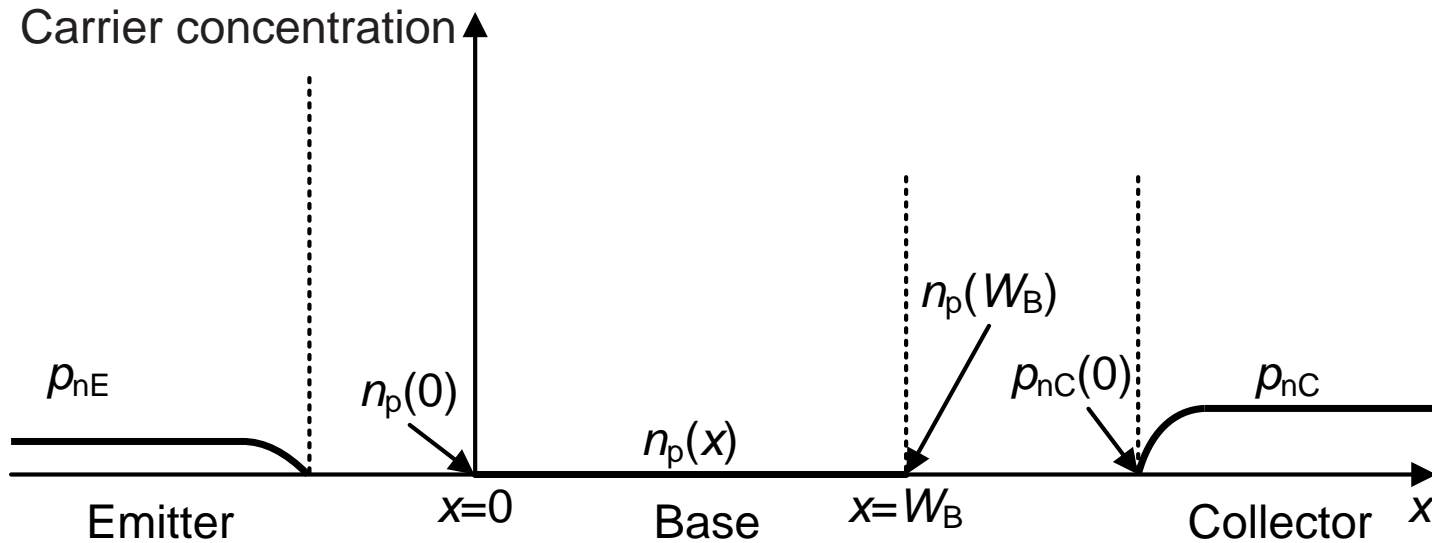
反向放大区



Carrier concentrations in a reversed npn transistor. (Not to scale.)

发射结反偏，集电结正偏

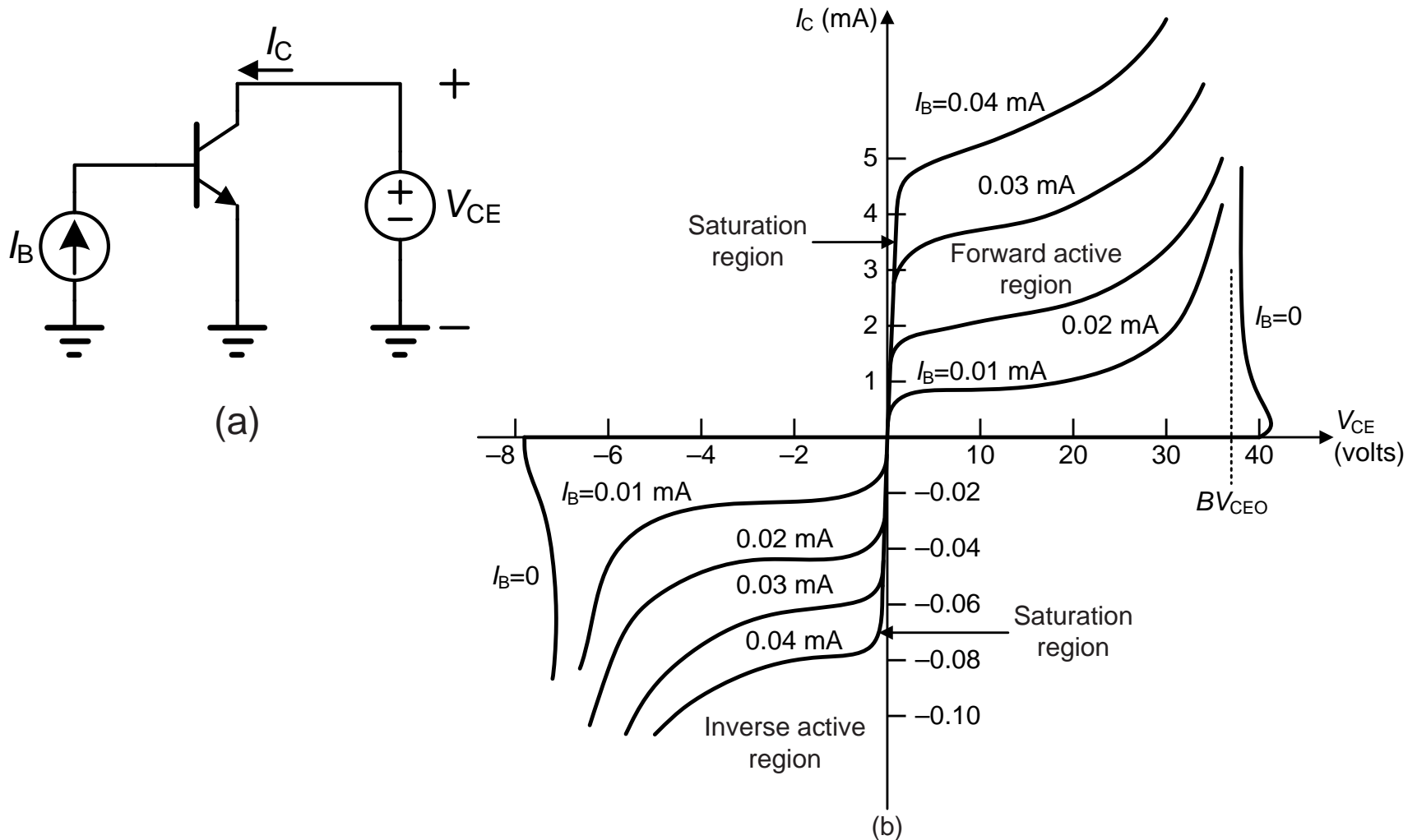
截止区



Carrier concentrations in a cutoff npn transistor. (Not to scale.)

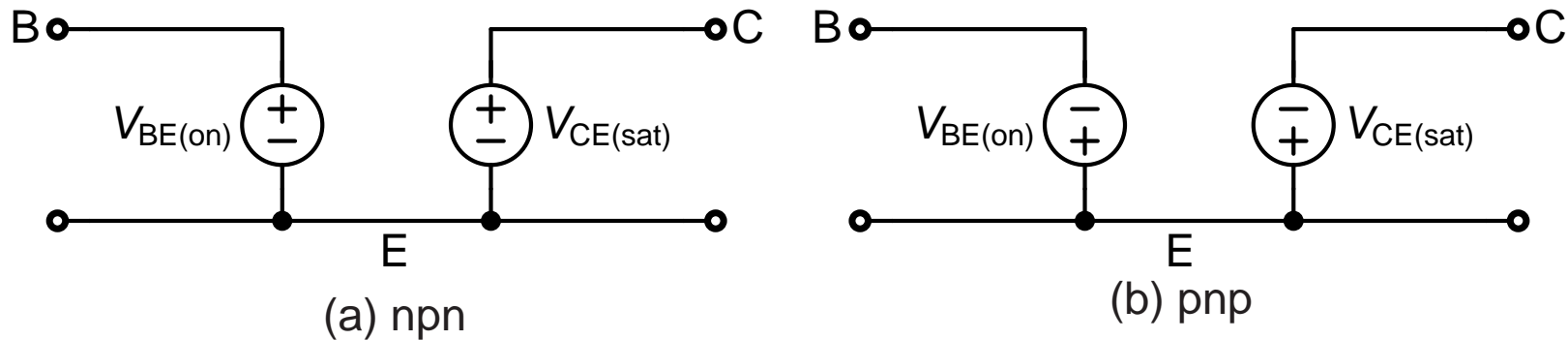
发射结反偏，集电结反偏

典型 I_C - V_{CE} 特性曲线图



(a) Test circuit. (b) Typical I_C - V_{CE} characteristics for an npn bipolar transistor. Note the different scales for positive and negative currents and voltages.

饱和区大信号模型



Large-signal models for bipolar transistors in the saturation region.

Ebers-Moll模型：(1)

基区中集电极耗尽区边缘的少数载流子浓度：

$$n_p(W_B) = n_{p0} e^{\frac{V_{BC}}{V_T}}$$

基极-集电极结正偏电流： $I_{CR} = -I_{CS} (e^{\frac{V_{BC}}{V_T}} - 1)$

基极-发射极结正偏电流： $I_{EF} = -I_{ES} (e^{\frac{V_{BE}}{V_T}} - 1)$

Ebers-Moll模型：正向/反向放大共基极电流增益 α_F, α_R

$$\begin{cases} I_C = \alpha_F I_{ES} (e^{\frac{V_{BE}}{V_T}} - 1) - I_{CS} (e^{\frac{V_{BC}}{V_T}} - 1) \\ I_E = -I_{ES} (e^{\frac{V_{BE}}{V_T}} - 1) + \alpha_R I_{CS} (e^{\frac{V_{BC}}{V_T}} - 1) \end{cases}$$

Ebers-Moll模型：(2)

在正向放大区， V_{BE} 为正， V_{BC} 为负，

$$\begin{cases} I_C = \alpha_F I_{ES} (e^{\frac{V_{BE}}{V_T}} - 1) + I_{CS} \\ I_E = -I_{ES} (e^{\frac{V_{BE}}{V_T}} - 1) - \alpha_R I_{CS} \end{cases}$$

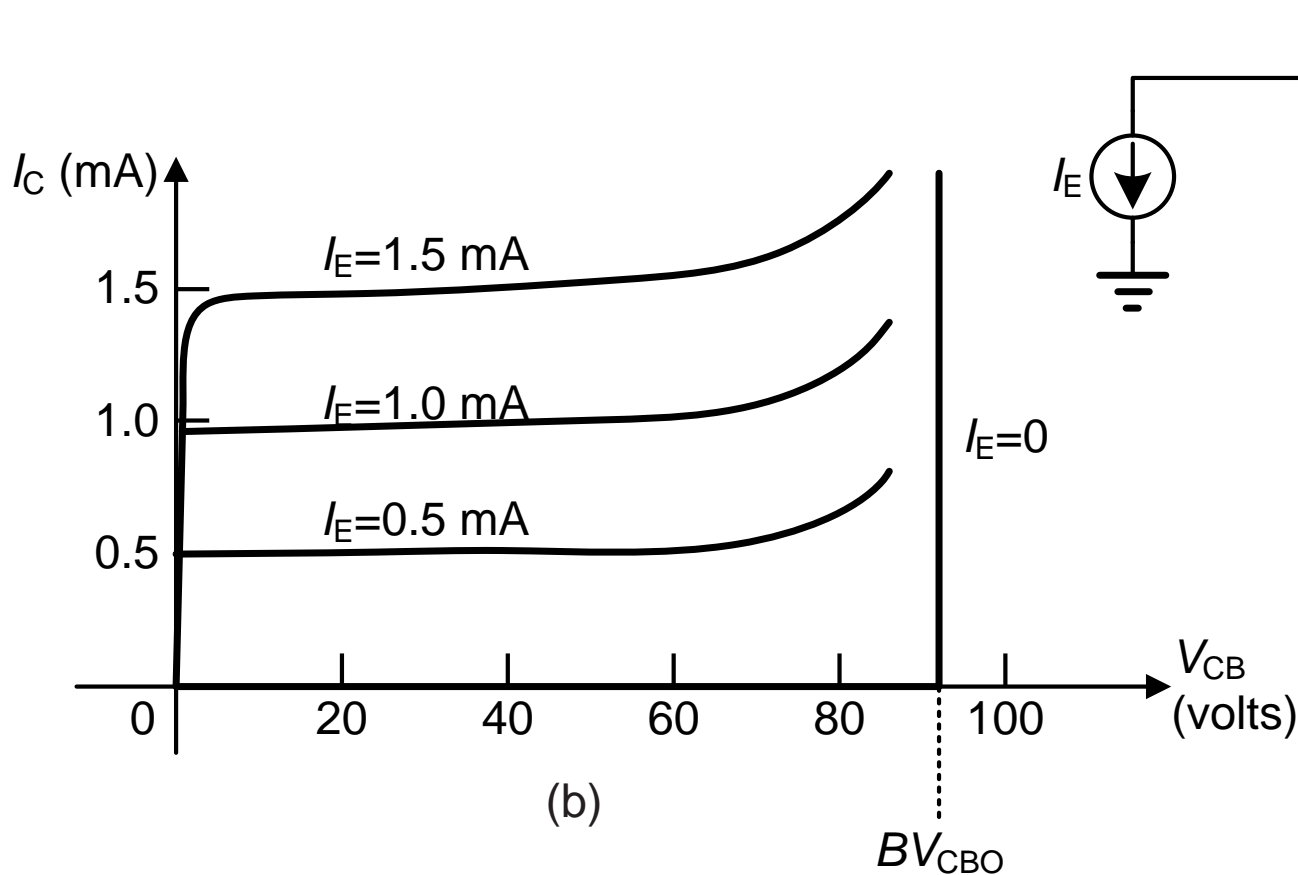
正向/反向放大区共射极电流增益： $\beta_F = \frac{\alpha_F}{1 - \alpha_F}$ $\beta_R = \frac{\alpha_R}{1 - \alpha_R}$

集电极电流： $I_C = \alpha_F I_{ES} (e^{\frac{V_{BE}}{V_T}} - 1) + I_{CS} = \alpha_F (-I_E - \alpha_R I_{CS}) + I_{CS}$
 $= -\alpha_F I_E + I_{CS} (1 - \alpha_R \alpha_F) = -\alpha_F I_E + I_{CO}$

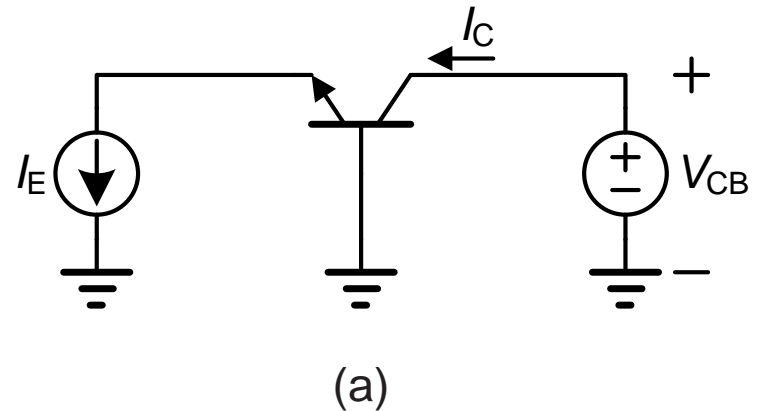
基极电流：

$$I_B = -(I_C + I_E) = \frac{1 - \alpha_F}{\alpha_F} I_C - \frac{I_{CO}}{\alpha_F} = \frac{I_C}{\beta_F} - \frac{I_{CO}}{\alpha_F} \quad I_{CO} = I_{CS} (1 - \alpha_R \alpha_F)$$

共基击穿电压



Common-base transistor connection. (a) Test circuit. (b) $I_C - V_{CB}$ characteristics.



$$I_C = -\alpha_F I_E M$$

$$M = \frac{1}{1 - \left(\frac{V_{CB}}{BV_{CBO}}\right)^n}$$

共射与共基击穿电压的关系

$$I_B = -(I_C + I_E) \qquad I_C = \frac{M\alpha_F}{1 - M\alpha_F} I_B$$

令 $M\alpha_F=1$ ，且 $V_{CB} \approx V_{CE}$ ，

$$\frac{\alpha_F}{1 - \left(\frac{BV_{CEO}}{BV_{CBO}}\right)^n} = 1$$

$$\frac{BV_{CEO}}{BV_{CBO}} = \sqrt[n]{1 - \alpha_F} = \sqrt[n]{\frac{\alpha_F}{\beta_F}} \approx \frac{1}{\sqrt[n]{\beta_F}}$$

$$BV_{CEO} \approx \frac{BV_{CBO}}{\sqrt[n]{\beta_F}}$$

β_F 和 n 典型为100和4

例题4:

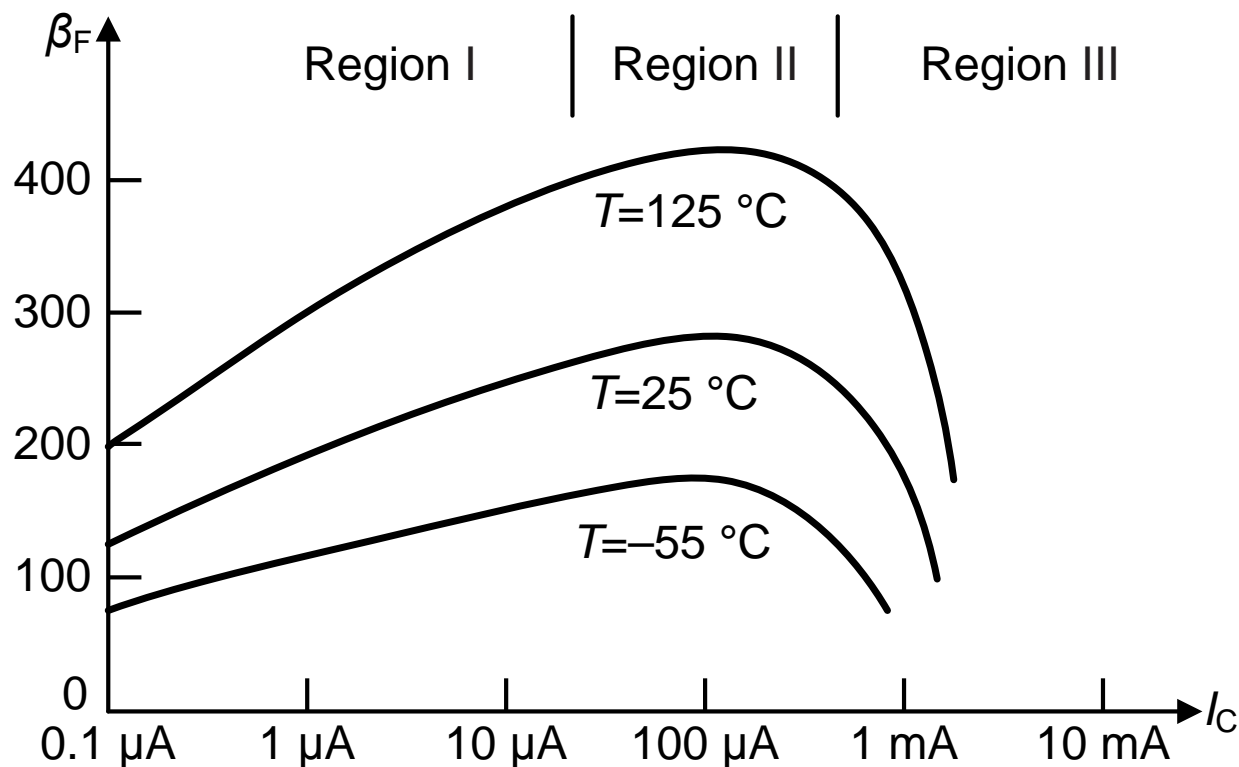
BJT晶体管的集电极掺杂浓度远小于基极浓度，当集电极浓度为 2×10^{15} 原子/cm³，临界电场 $E_{\text{crit}} = 3 \times 10^5$ V/cm， $\beta = 100$ 和 $n = 4$ ，计算击穿电压 BV_{CEO} 。

解：因为 $N_{\text{B}} \gg N_{\text{C}}$ ，

$$BV_{\text{CBO}} = \frac{\epsilon_{\text{si}} E_{\text{crit}}^2}{2qN_{\text{C}}} = \frac{1.04 \times 10^{-12} \times 9 \times 10^{10}}{2 \times 1.6 \times 10^{-19} \times 2 \times 10^{15}} = 146 \text{ V}$$

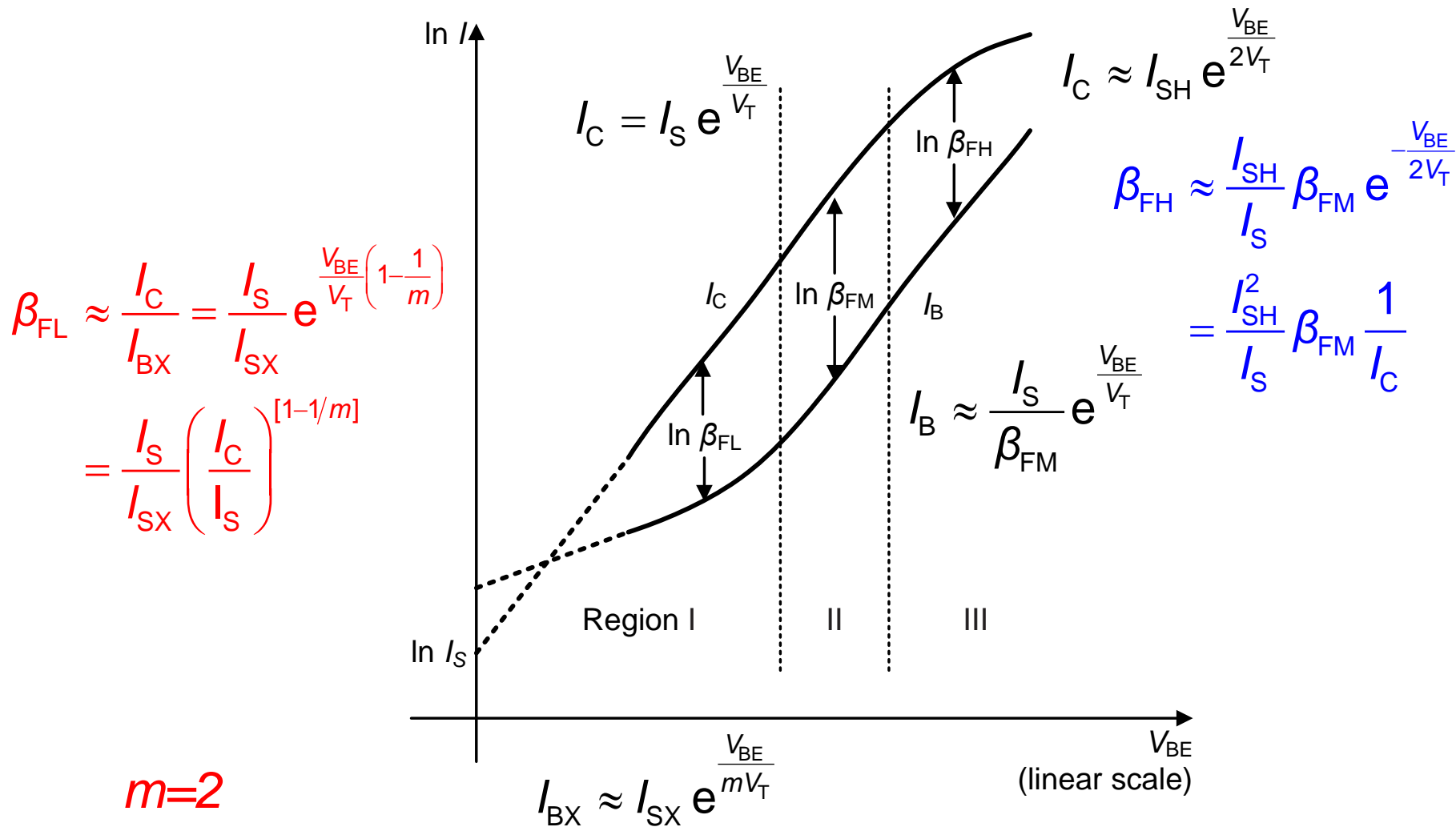
$$BV_{\text{CEO}} \approx \frac{BV_{\text{CBO}}}{\sqrt[n]{\beta_{\text{F}}}} = \frac{146}{\sqrt[4]{100}} = 46 \text{ V}$$

电流增益 β_F 与工作条件的关系



Typical curves of β_F versus I_C for an npn integrated-circuit transistor with $6\ \mu\text{m}^2$ emitter area.

In I - V_{BE} 关系



$$\beta_{FL} \approx \frac{I_C}{I_{BX}} = \frac{I_S}{I_{SX}} e^{\frac{V_{BE}}{V_T} (1 - \frac{1}{m})}$$

$$= \frac{I_S}{I_{SX}} \left(\frac{I_C}{I_S} \right)^{[1 - 1/m]}$$

$m=2$

$$I_{BX} \approx I_{SX} e^{\frac{V_{BE}}{mV_T}}$$

$$I_C \approx I_{SH} e^{\frac{V_{BE}}{2V_T}}$$

$$\beta_{FH} \approx \frac{I_{SH}}{I_S} \beta_{FM} e^{-\frac{V_{BE}}{2V_T}}$$

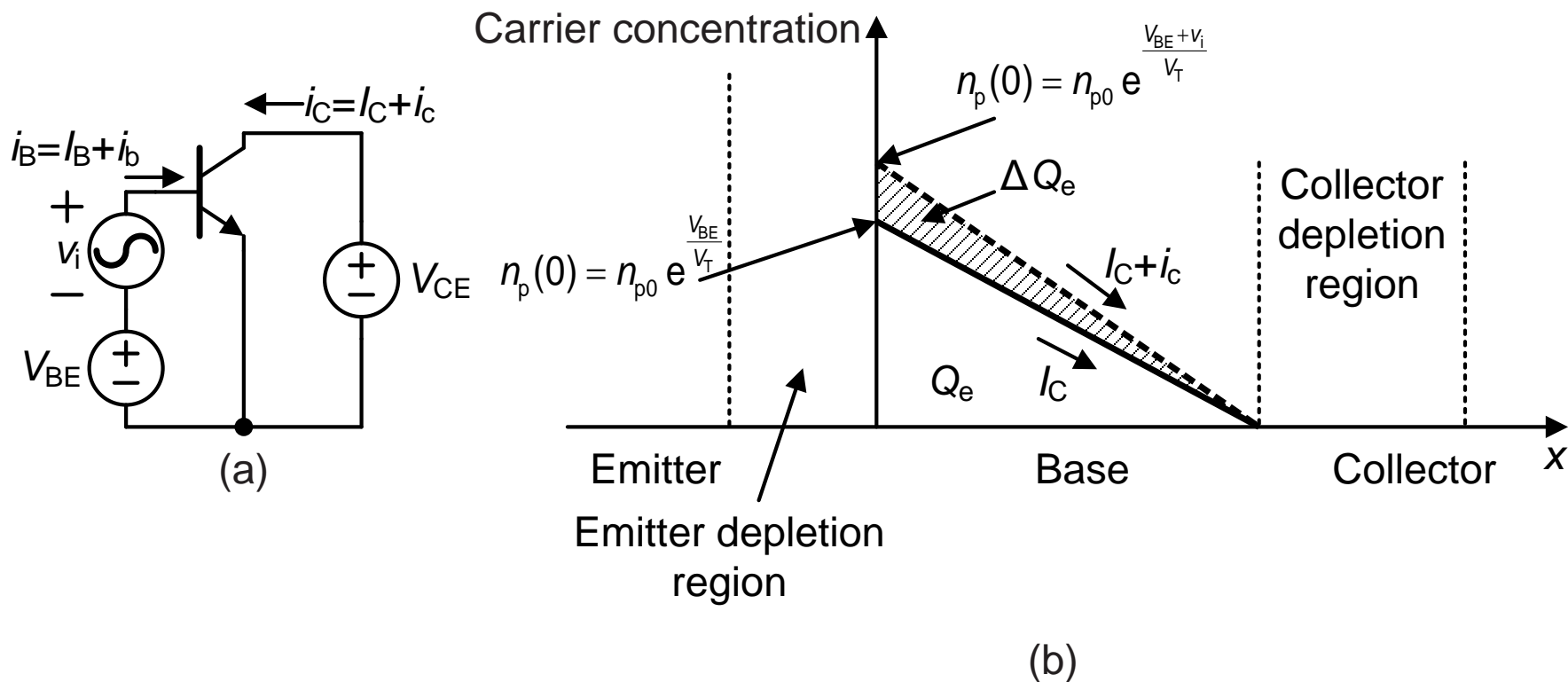
$$= \frac{I_{SH}^2}{I_S} \beta_{FM} \frac{1}{I_C}$$

$$I_B \approx \frac{I_S}{\beta_{FM}} e^{\frac{V_{BE}}{V_T}}$$

Region I II III

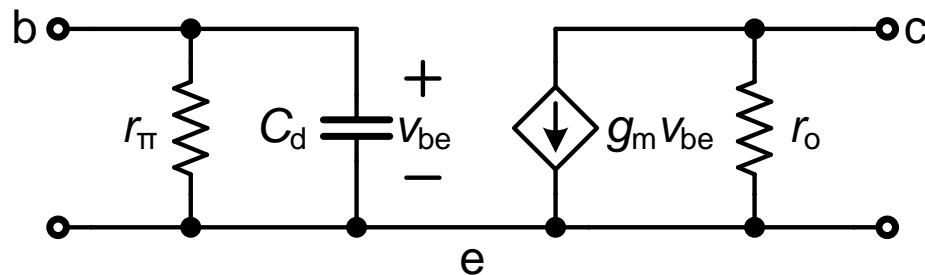
V_{BE}
(linear scale)

小信号模型



Effect of a small-signal input voltage applied to a bipolar transistor. (a) Circuit schematic. (b) Corresponding changes in carrier concentrations in the base when the device is in the forward-active region.

低频小信号模型：(1)



Basic bipolar transistor small-signal equivalent circuit.

跨导：
$$g_m = \frac{i_c}{v_{be}} = \frac{\partial I_C}{\partial V_{BE}} = \frac{I_{CS}}{V_T} e^{\frac{V_{BE}}{V_T}} = \frac{I_C}{V_T} \quad V_T = \frac{kT}{q}$$

小信号输入电阻：
$$r_{\pi} = \frac{\partial V_{BE}}{\partial I_B} = \left(\frac{\partial I_B}{\partial V_{BE}} \right)^{-1} = \left(\frac{\partial (I_{CS} e^{V_{BE}/V_T} / \beta)}{\partial V_{BE}} \right)^{-1}$$

$$= \frac{V_T}{I_B} = \beta \frac{V_T}{I_C} = \frac{\beta}{g_m}$$

低频小信号模型：(2)

基区中少数载流子存储电荷：

$$Q_e = \frac{1}{2} n_p(0) W_B q A = \frac{q A n_i^2 W_B}{2 N_B} e^{\frac{V_{BE}}{V_T}} \approx \frac{W_B^2}{2 D_n} I_C = \tau_b I_C$$

其中 τ_b 是基区渡越时间：

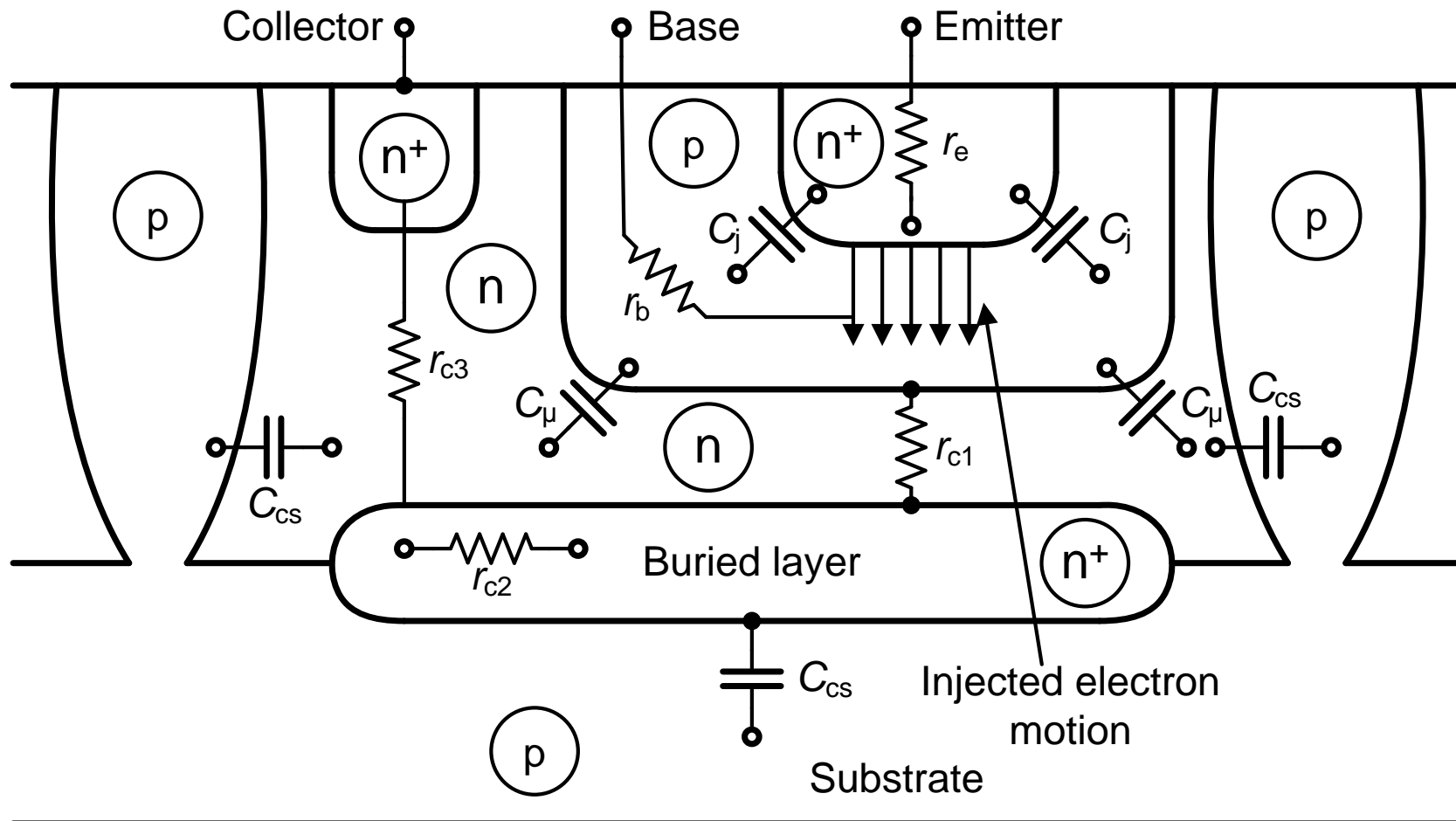
$$\tau_b = \frac{W_B^2}{2 D_n}$$

基区扩散电容： $C_d \approx \frac{dQ_e}{dV_{BE}} = \frac{d(\tau_b I_C)}{dV_{BE}} \approx \tau_b \frac{I_C}{V_T} = g_m \tau_b$

输出阻抗：

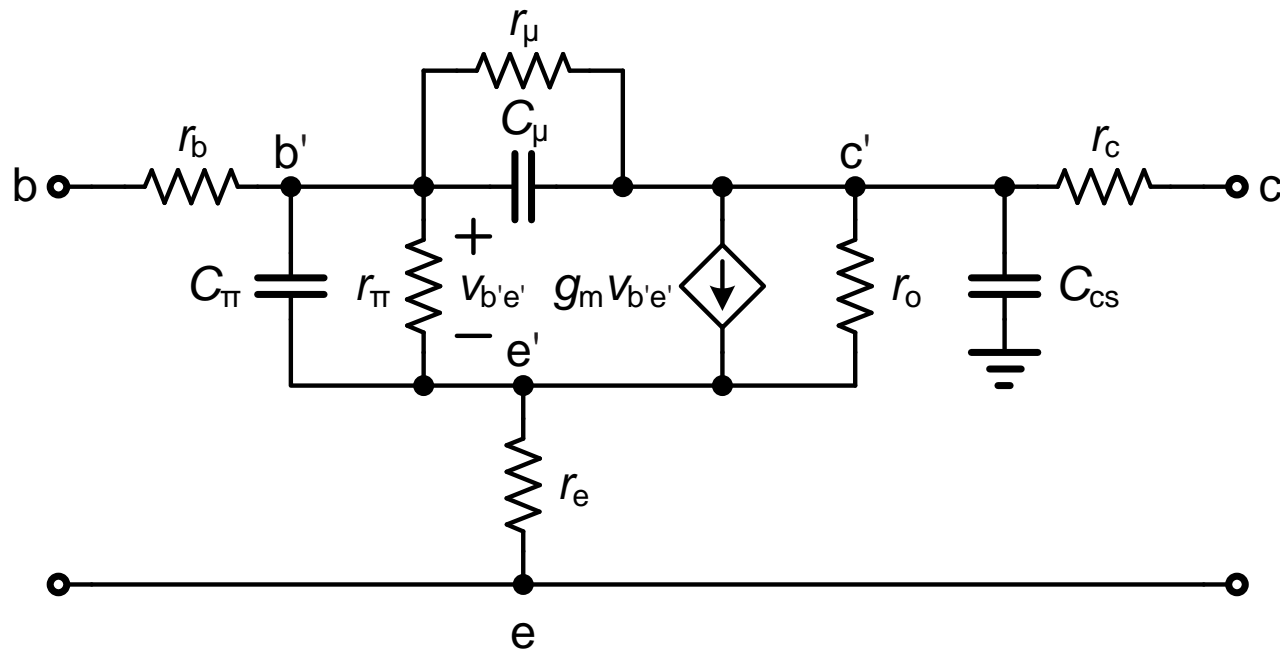
$$r_o = \frac{\partial V_{CE}}{\partial I_C} = \left(\frac{\partial I_C}{\partial V_{CE}} \right)^{-1} = \left(\frac{\partial (I_{CS} e^{V_{BE}/V_T} (1 + \frac{V_{CE}}{V_A}))}{\partial V_{CE}} \right)^{-1} \approx \frac{V_A}{I_C}$$

BJT晶体管的寄生参数



Integrated-circuit npn bipolar transistor structure showing parasitic elements.
(Not to scale.)

高频小信号模型：(1)



Complete bipolar transistor small-signal equivalent circuit.

集基电阻 r_{μ} : 假设 V_{BE} 恒定，基极电流 $I_B = 10 I_{B1}$

$$r_{\mu} = \frac{\partial V_{CE}}{\partial I_{B1}} = \frac{\partial V_{CE}}{\partial I_C} \frac{\partial I_C}{\partial I_{B1}} = 10 r_o \frac{\partial I_C}{\partial I_B} = 10 \beta_0 r_o$$

高频小信号模型：(2)

正向偏置的基极-发射极结电容：

其中 C_j 是基极-发射极结的耗尽电容

$$C_{\pi} = C_j + C_d$$

$$C_j = \frac{C_{jbe0}}{\left(1 - \frac{V_{BE}}{\phi_{0BE}}\right)^{1/2}}$$

基极-集电极结的耗尽电容：缓变结

集电极-衬底结的耗尽电容：

$$C_{\mu} = \frac{C_{jbc0}}{\left(1 + \frac{V_{CB}}{\phi_{0BC}}\right)^{1/3}}$$

$$C_{cs} = \frac{C_{jsc0}}{\left(1 + \frac{V_{CS}}{\phi_{0SC}}\right)^{1/3}}$$

寄生电阻： r_b ， r_e 和 r_c

例题5:

计算双极型晶体管小信号参数。假设 $I_C=1\text{ mA}$, $V_{CB}=3\text{ V}$, $V_{CS}=5\text{ V}$, $C_{jbe0}=10\text{ fF}$, $n_{be}=0.5$, $\Phi_{0BE}=0.9\text{ V}$, $C_{jbc0}=10\text{ fF}$, $n_{bc}=0.3$, $\Phi_{0BC}=0.5\text{ V}$, $C_{jsc0}=20\text{ fF}$, $n_{sc}=0.3$, $\Phi_{0SC}=0.65\text{ V}$, $\beta_0=100$, $\tau_b=10\text{ ps}$, $V_A=20\text{ V}$, $r_b=300\ \Omega$, $r_c=50\ \Omega$, $r_e=5\ \Omega$, $r_\mu=10\beta_0r_o$ 。

解:

$$g_m = \frac{I_C}{V_T} = \frac{1\text{ mA}}{26\text{ mV}} = 38\text{ mA/V} \quad r_\pi = \frac{\beta}{g_m} = \frac{100}{38\text{ mA/V}} = 2.6\text{ k}\Omega$$

$$r_o = \frac{V_A}{I_C} = \frac{20\text{ V}}{1\text{ mA}} = 20\text{ k}\Omega \quad r_\mu = 10\beta_0r_o = 10 \times 100 \times 20\text{ k}\Omega = 20\text{ M}\Omega$$

$$C_d = g_m\tau_b = 38\text{ mA/V} \times 10\text{ ps} = 0.38\text{ pF}$$

基极-发射极结正偏，耗尽电容很难计算，估算 $C_j=20\text{ fF}$ 。

$$C_\pi = C_j + C_d = 0.4\text{ pF} \quad C_\mu = 5.6\text{ fF} \quad C_{cs} = 10.5\text{ fF}$$

模拟评价指标

固有增益:

$$A_v = g_m r_o = \frac{I_C}{V_T} \frac{V_A}{I_C} = \frac{V_A}{V_T}$$

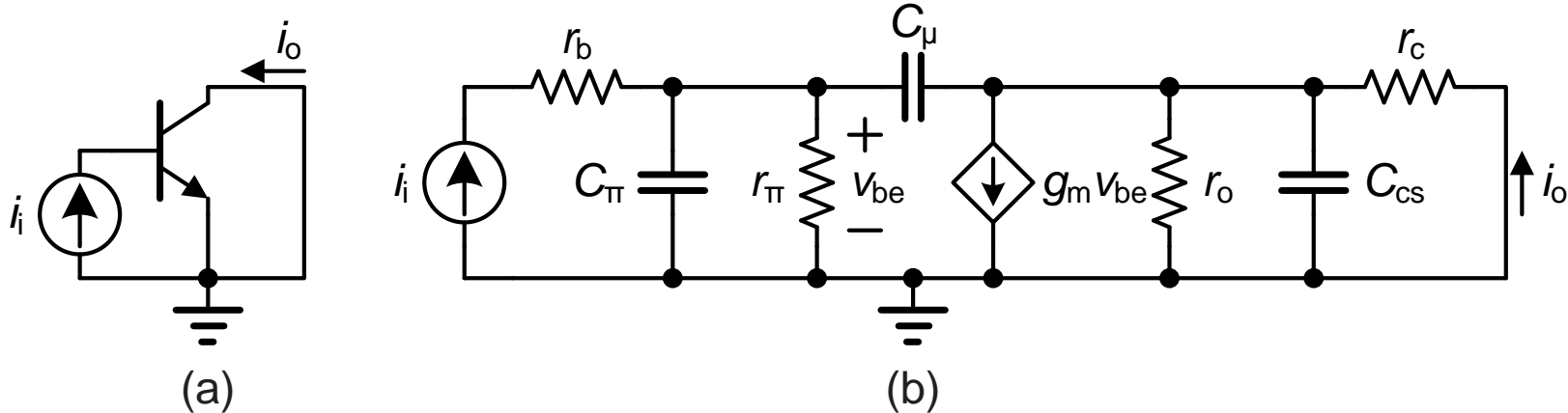
跨导电流比:

$$\frac{g_m}{I_C} = \frac{1}{V_T}$$

特征频率:

$$f_T = \frac{1}{2\pi} \frac{g_m}{C_{\pi} + C_{\mu}}$$

高频小信号电流增益



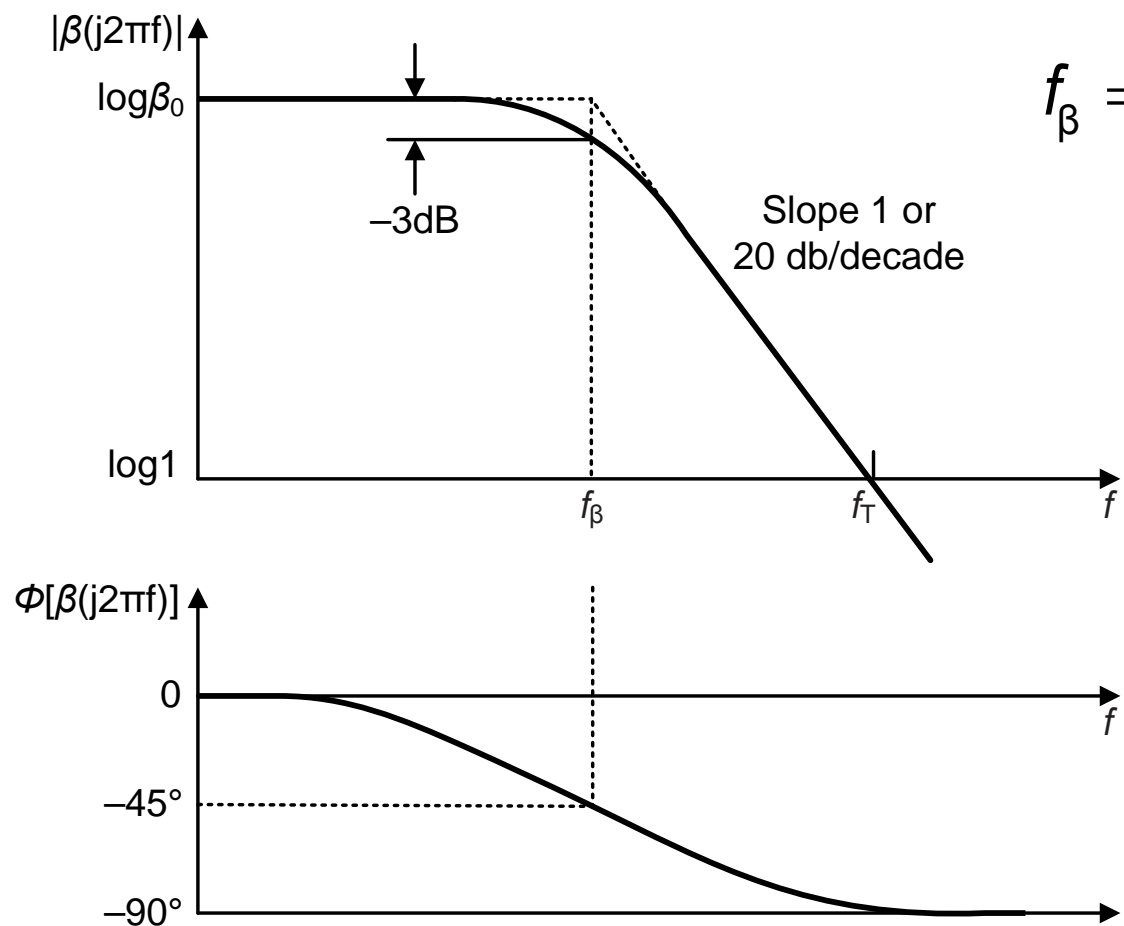
(a) Schematic of ac circuit for measurement of f_T . (b) Small-signal equivalent circuit for the calculation of f_T .

忽略 r_o 、 C_{cs} 、 r_c ，忽略通过 C_μ 的电流，

$$V_{be} \approx \frac{r_\pi}{1 + r_\pi(C_\pi + C_\mu)s} i_i \quad i_o \approx g_m V_{be} = i_i \frac{g_m r_\pi}{1 + r_\pi(C_\pi + C_\mu)s}$$

$$\beta(j2\pi f) = \frac{i_o}{i_i} = \frac{\beta_0}{1 + \beta_0 \frac{C_\pi + C_\mu}{g_m} j2\pi f} \approx \frac{g_m}{j2\pi f(C_\pi + C_\mu)}$$

特征频率



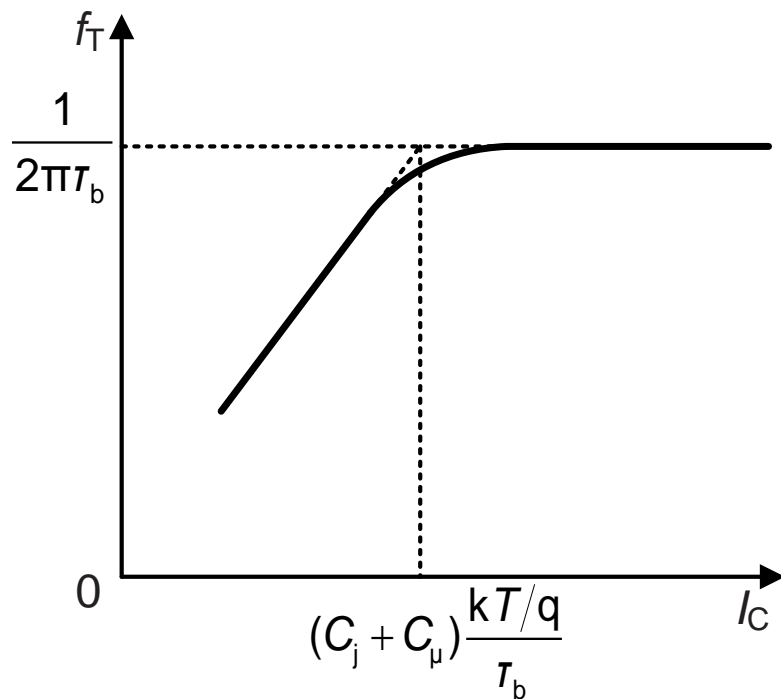
$$f_{\beta} = \frac{1}{2\pi\beta_0} \frac{g_m}{C_{\pi} + C_{\mu}} = \frac{f_T}{\beta_0}$$

$$f_T = \frac{1}{2\pi} \frac{g_m}{C_{\pi} + C_{\mu}}$$

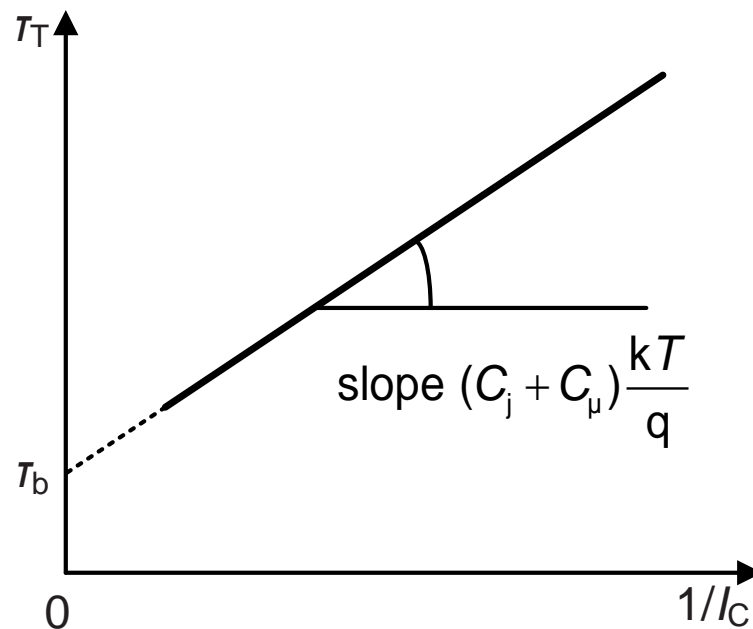
$$\beta(j2\pi f) = \frac{\beta_0}{1 + jf/f_{\beta}}$$

Bode diagrams of current driven CE bipolar transistor with shorted output.

f_T 与 I_{CE} 的关系：理论上



(a)

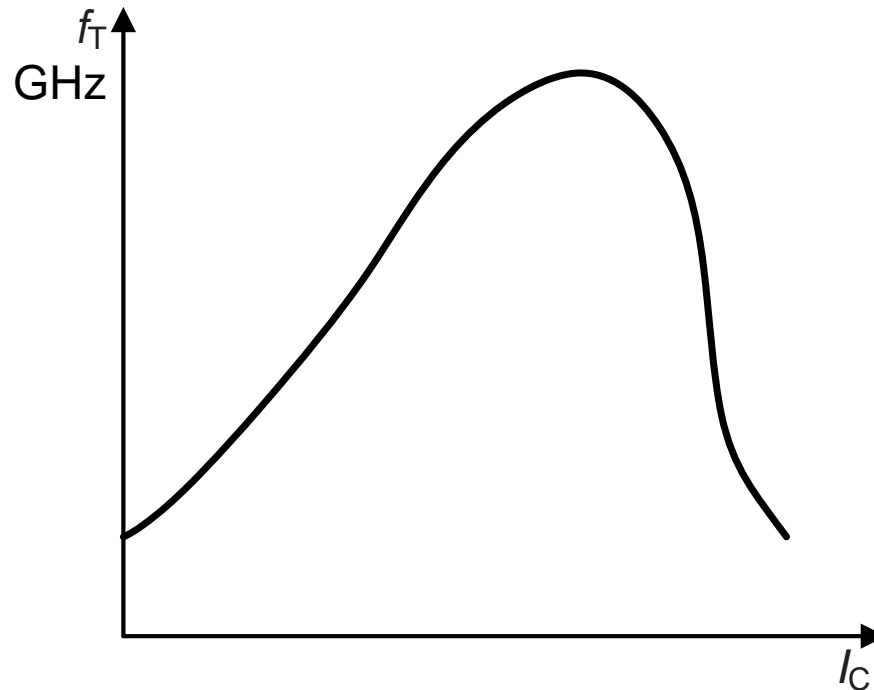


(b)

Unity-gain frequency f_T versus current I_C .

$$f_T = \frac{1}{2\pi T_b} \frac{I_C}{I_C + I_{CfT}} \quad I_{CfT} = (C_j + C_\mu) \frac{V_T}{T_b} \quad T_T = T_b + (C_j + C_\mu) \frac{V_T}{I_C}$$

f_T 与 I_{CE} 的关系：实际上



A sketch of transistor f_T versus collector current, I_C .

例题6:

某双极型晶体管在 $I_{C1}=0.25$ mA和 $I_{C2}=1$ mA两种工作情况下，在1 GHz频率点，输出短路的共射电流增益分别为8和9，电容 C_{μ} 的测试值为10 fF，假设 C_j 和 τ_b 是常数，计算它们的值。

解：在 $I_{C1}=0.25$ mA和 $I_{C2}=1$ mA两种工作情况下，特征频率分别为 $f_{T1}=8$ GHz, $f_{T2}=9$ GHz。

$$\begin{cases} \frac{1}{2\pi f_{T1}} = \tau_b + (C_j + C_{\mu}) \frac{kT/q}{I_{C1}} \\ \frac{1}{2\pi f_{T2}} = \tau_b + (C_j + C_{\mu}) \frac{kT/q}{I_{C2}} \end{cases} \quad \begin{cases} C_j = 18.2 \text{ fF} \\ \tau_b = 17 \text{ ps} \end{cases}$$

器件模型概要：放大区直流参数

$I_C = I_S e^{\frac{V_{BE}}{V_T}}$	$V_T \approx \frac{kT}{q} \approx 26 \text{ mV at } 300 \text{ K}$
For more accuracy, $I_C = I_S \left(1 + \frac{V_{CE}}{V_A} \right) e^{\frac{V_{BE}}{V_T}}$	
$I_S = \frac{qAD_n n_i^2}{Q_B}$	$I_B = \frac{I_C}{\beta}$
$I_E = - \left(I_C + \frac{I_C}{\beta} \right) = - \frac{I_C}{\alpha} = -(\beta + 1)I_B$	$\beta = \frac{I_C}{I_B} \approx \frac{D_n}{D_p} \frac{L_p}{W_B} \frac{N_D}{N_A} \approx 2.5 \frac{L_p}{W_B} \frac{N_D}{N_A}$
$\alpha = \frac{\beta}{1 + \beta} = \frac{1}{1 + \frac{1}{\beta}} = \frac{1}{1 + \frac{W_B^2}{2\tau_b D_n} + \frac{D_p}{D_n} \frac{W_B}{L_p} \frac{N_A}{N_D}} \approx \alpha_T \gamma$	
$\alpha_T = \frac{1}{1 + \frac{W_B^2}{2\tau_b D_n}}$	$\gamma = \frac{1}{1 + \frac{D_p}{D_n} \frac{W_B}{L_p} \frac{N_A}{N_D}}$

器件模型概要：放大区小信号参数

$r_{\pi} = \frac{V_T}{I_B} = \frac{\beta}{g_m}$	$r_o = \frac{V_A}{I_C}$
$g_m = \frac{I_C}{V_T}$	$g_m r_o = \frac{V_A}{V_T}$
$C_{\pi} = C_j + C_d$	
$C_j = \frac{C_{jbe0}}{\left(1 - \frac{V_{BE}}{\Phi_{0BE}}\right)^{1/2}}$	$C_d = g_m \tau_b$
$C_{\mu} = \frac{C_{jbc0}}{\left(1 + \frac{V_{CB}}{\Phi_{0BC}}\right)^{1/3}}$	$C_{cs} = \frac{C_{jsc0}}{\left(1 + \frac{V_{CS}}{\Phi_{0SC}}\right)^{1/3}}$

“单页” BJT型晶体管模型

$$I_C = I_S e^{\frac{V_{BE}}{V_T}} \left(1 + \frac{V_{CE}}{V_A} \right)$$

$$I_S \approx 10^{-15} \text{ A}$$

当 $k=300 \text{ K}$ 时, $V_T = kT/q = 26 \text{ mV}$

$$g_m = \frac{I_C}{V_T}$$

$$r_o = \frac{V_A}{I_C}$$

$$V_{Anpn} \approx 20 \text{ V}$$

$$V_{Apnp} \approx 10 \text{ V}$$

$$f_T = \frac{1}{2\pi} \frac{1}{T_b + \frac{C_j + C_\mu}{g_m}}$$

$$\text{或} \approx \frac{V_{scl}}{2\pi W_B}$$

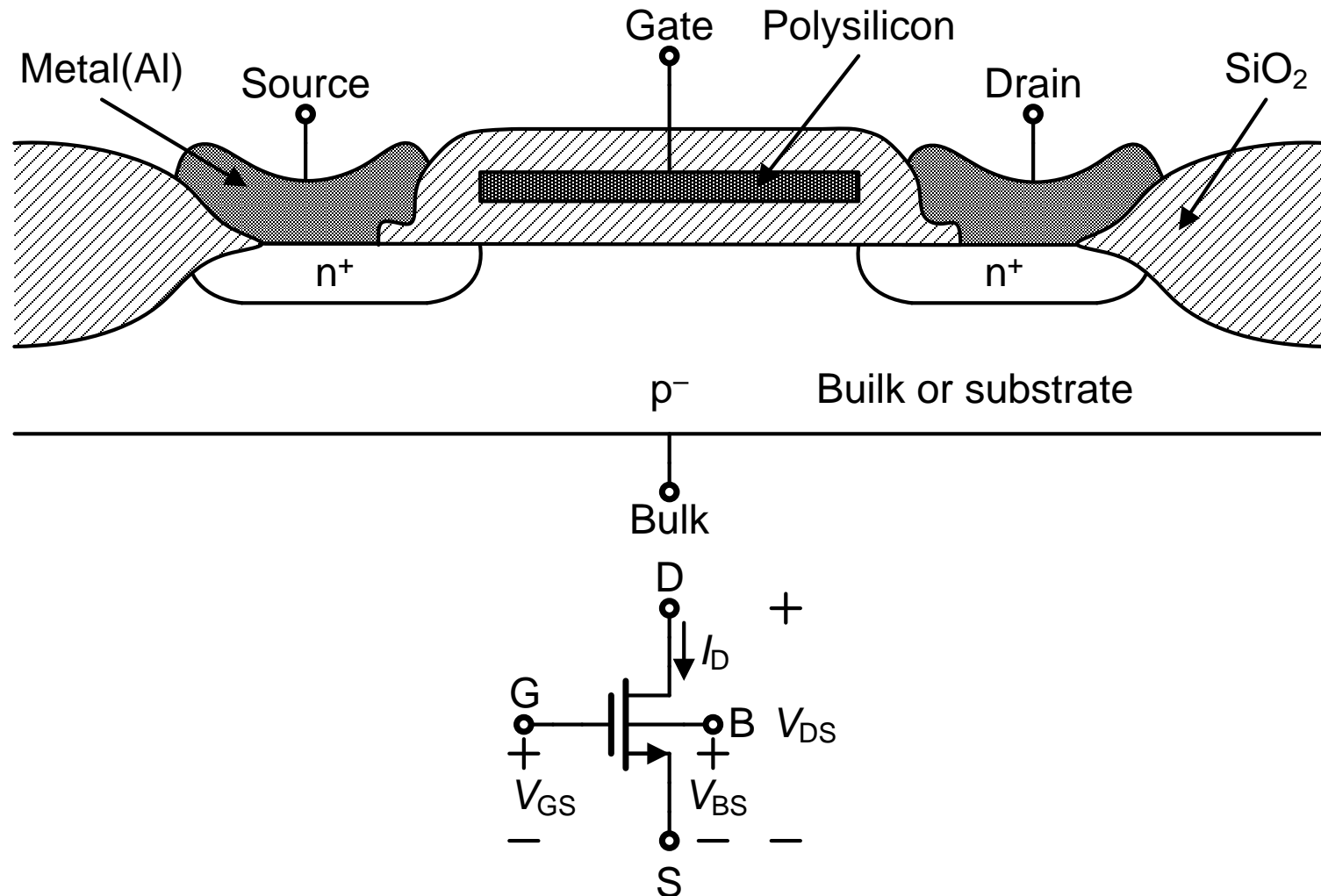
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 - MOS管
 - MOS电容
 - 阈值电压
 - 大信号工作原理
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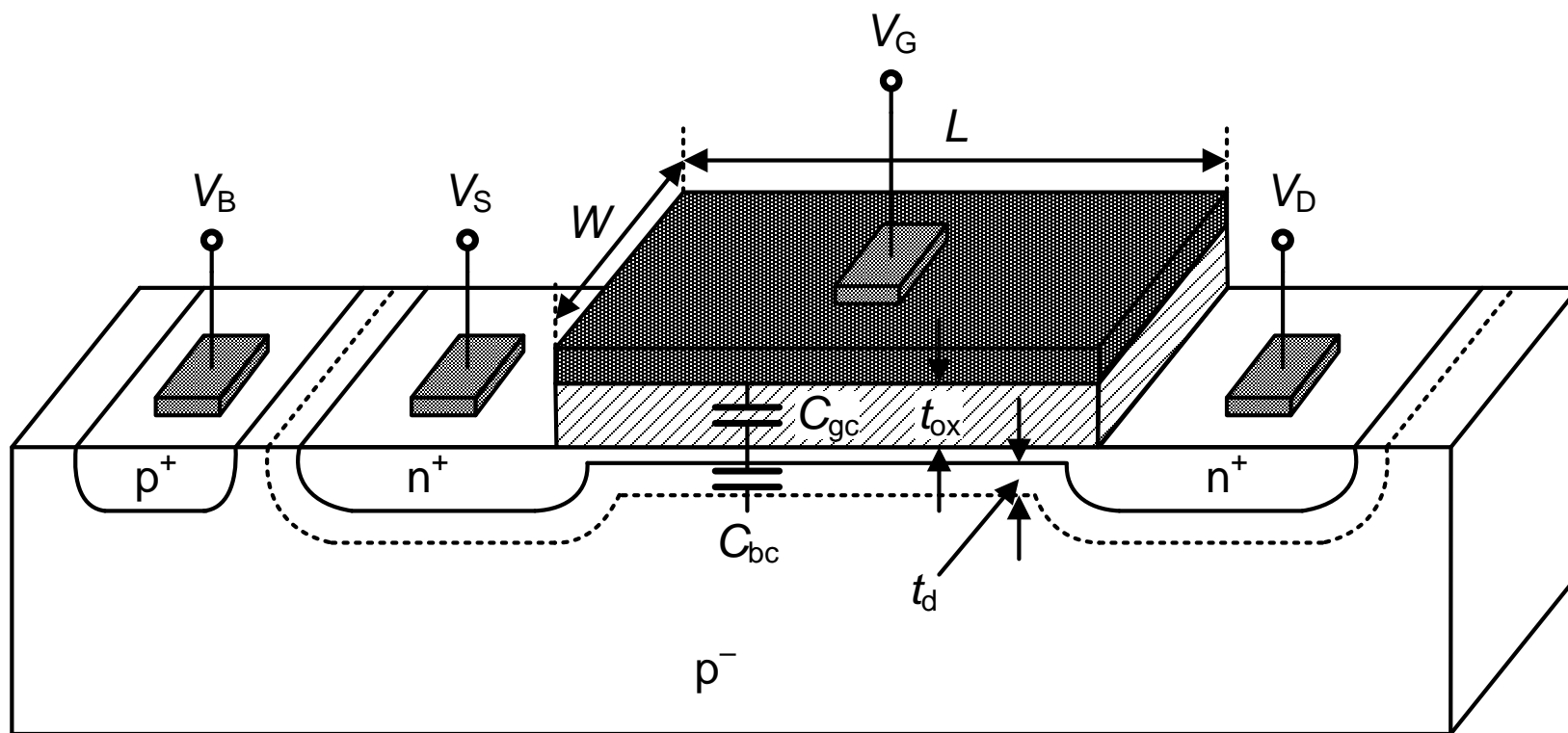
- 高频小信号模型
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- 器件模型概要
- MOS型与BJT型晶体管的比较

NMOS型晶体管的剖面图和符号

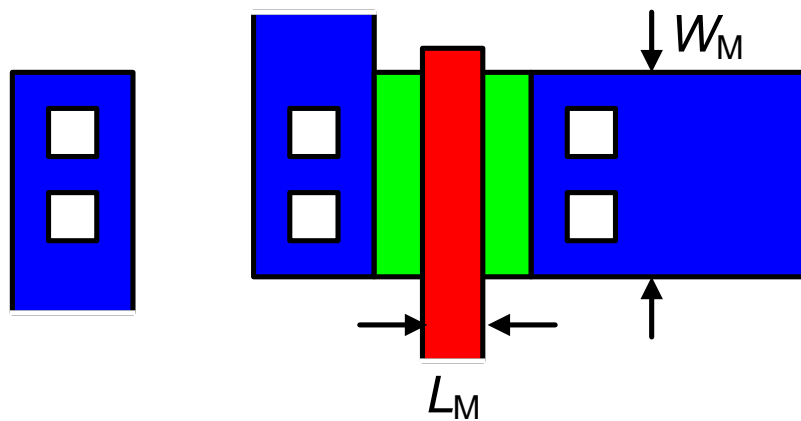
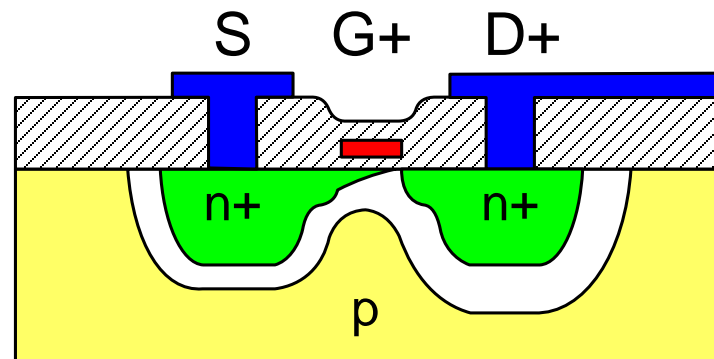
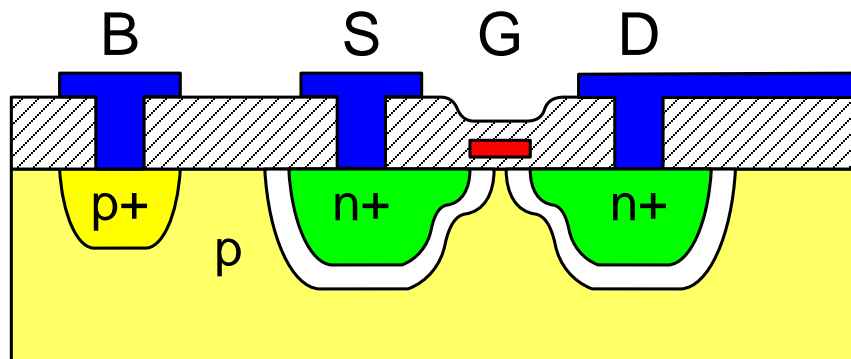


A cross section of a typical n-channel transistor.

MOS型晶体管的尺寸参数



MOS型晶体管的版图



MIS结构：电荷密度

耗尽层中的电荷体密度：

$$\rho = -qN_B$$

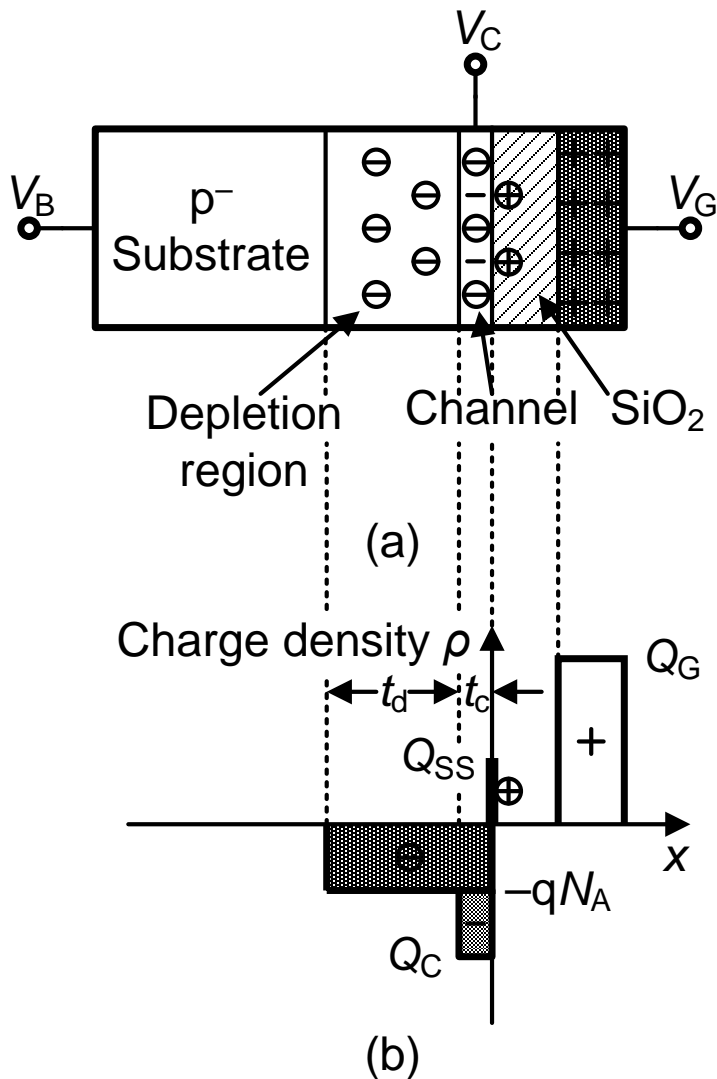
沟道中电荷面密度： Q_C

沟道和栅氧之间的表面缺陷造成的电荷面密度： Q_{SS}

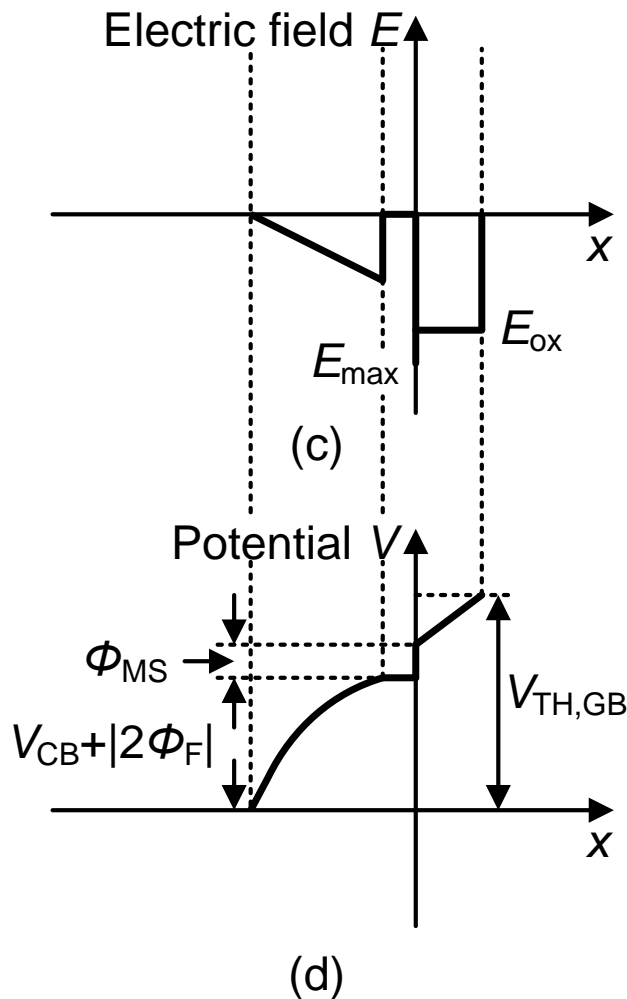
栅上电荷面密度： Q_G

电荷守恒：(面密度)

$$-qN_A t_d + Q_C + Q_{SS} + Q_G = 0$$



MIS结构：电场和静电势



在耗尽层中，由泊松方程：

$$\frac{d^2V(x)}{dx^2} = -\frac{\rho}{\epsilon_{si}} = \frac{qN_B}{\epsilon_{si}}$$

$$E(x) = -\frac{dV(x)}{dx} = -\left(\frac{qN_B}{\epsilon_{si}}x + C_1\right)$$

边界条件： $x = -t_d - t_c$ 时， $E(x) = 0$

$$E(x) = \frac{-qN_B}{\epsilon_{si}}(x + t_d + t_c)$$

MIS结构：静电势

$$E(x) = -\frac{qN_B}{\epsilon_{si}}(x + t_d + t_c) = -\frac{dV(x)}{dx}$$

$$V(x) = \frac{qN_B}{\epsilon_{si}} \left(\frac{x^2}{2} + (t_d + t_c)x \right) + C_2$$

耗尽层静电势差：

$$V(-t_c) - V(-t_d - t_c) = \frac{qN_B}{\epsilon_{si}} \frac{t_d^2}{2} = |\phi_S - \phi_F| + V_{CB}$$

其中 ϕ_S 是反型层的表面势。

当 $\phi_S = -\phi_F$ 时，衬底反型形成沟道。耗尽层的宽度：

$$t_d = \left[\frac{2\epsilon_{si} (|\phi_F| + V_{CB})}{qN_B} \right]^{1/2}$$

耗尽电容和栅氧电容

耗尽层中的电荷面密度： $Q_j = qN_B t_d$

耗尽电容： $C_{bc} = WL \frac{dQ_j}{dV_{CB}} = WL \frac{\epsilon_{si}}{t_d} = WLC_j$

其中 C_j 为单位面积的耗尽电容：

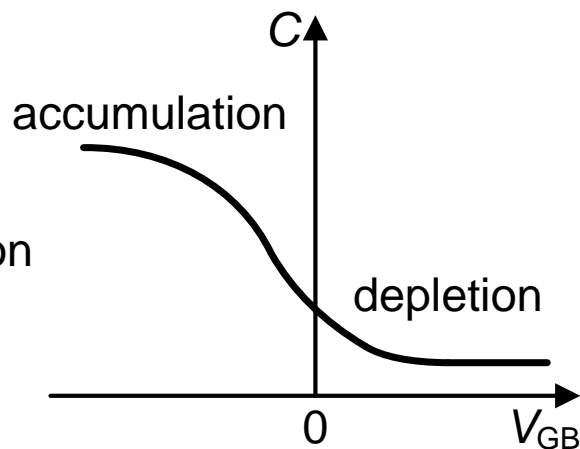
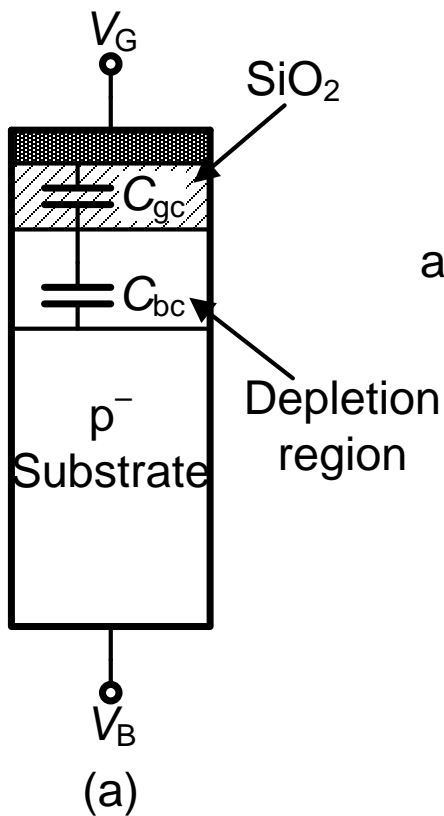
$$C_j = \frac{\epsilon_{si}}{t_d}$$

栅氧电容： $C_{gc} = WLC_{ox}$

其中 C_{ox} 为单位面积的栅氧电容：

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}}$$

MIS结构：电容



$$C_{gb} = \frac{1}{\frac{1}{C_{gc}} + \frac{1}{C_{bc}}} = \frac{C_{gc} C_{bc}}{C_{gc} + C_{bc}}$$

栅上的电荷面密度

耗尽区中的固定电荷面密度:

$$Q_j = -qN_B t_d = -\sqrt{2qN_B \epsilon_{si} (|2\Phi_F| + V_{CB})}$$

如果 V_C 浮空或者耗尽层偏压 $V_{CB}=0$ ，耗尽区中的固定电荷面密度:

$$Q_{j0} = -qN_B t_d = -\sqrt{2qN_B \epsilon_{si} (|2\Phi_F|)}$$

当反型沟道层刚形成时，根据电荷守恒，栅上的电荷面密度:

$$Q_G = -Q_j - Q_{SS}$$

V_{GB} 的阈值电压

$$\begin{aligned}
 V_{TH,GB} &= V_{CB} + |2\phi_F| + \phi_{MS} + \frac{Q_G}{C_{ox}} = V_{CB} + |2\phi_F| + \phi_{MS} + \frac{-Q_j - Q_{SS}}{C_{ox}} \\
 &= V_{CB} + |2\phi_F| + \phi_{MS} - \frac{Q_{j0}}{C_{ox}} - \frac{Q_{SS}}{C_{ox}} - \frac{Q_j - Q_{j0}}{C_{ox}} \\
 &= V_{CB} + V_{TH0} + Y(\sqrt{|2\phi_F| + V_{CB}} - \sqrt{|2\phi_F|})
 \end{aligned}$$

$$V_{TH0} = |2\phi_F| + \phi_{MS} - \frac{Q_{j0}}{C_{ox}} - \frac{Q_{SS}}{C_{ox}}$$

体效应系数:

$$Y = \frac{\sqrt{2qN_B\epsilon_{si}}}{C_{ox}} = \frac{C_{bc}}{C_{gc}} 2\sqrt{|2\phi_F| + V_{CB}}$$

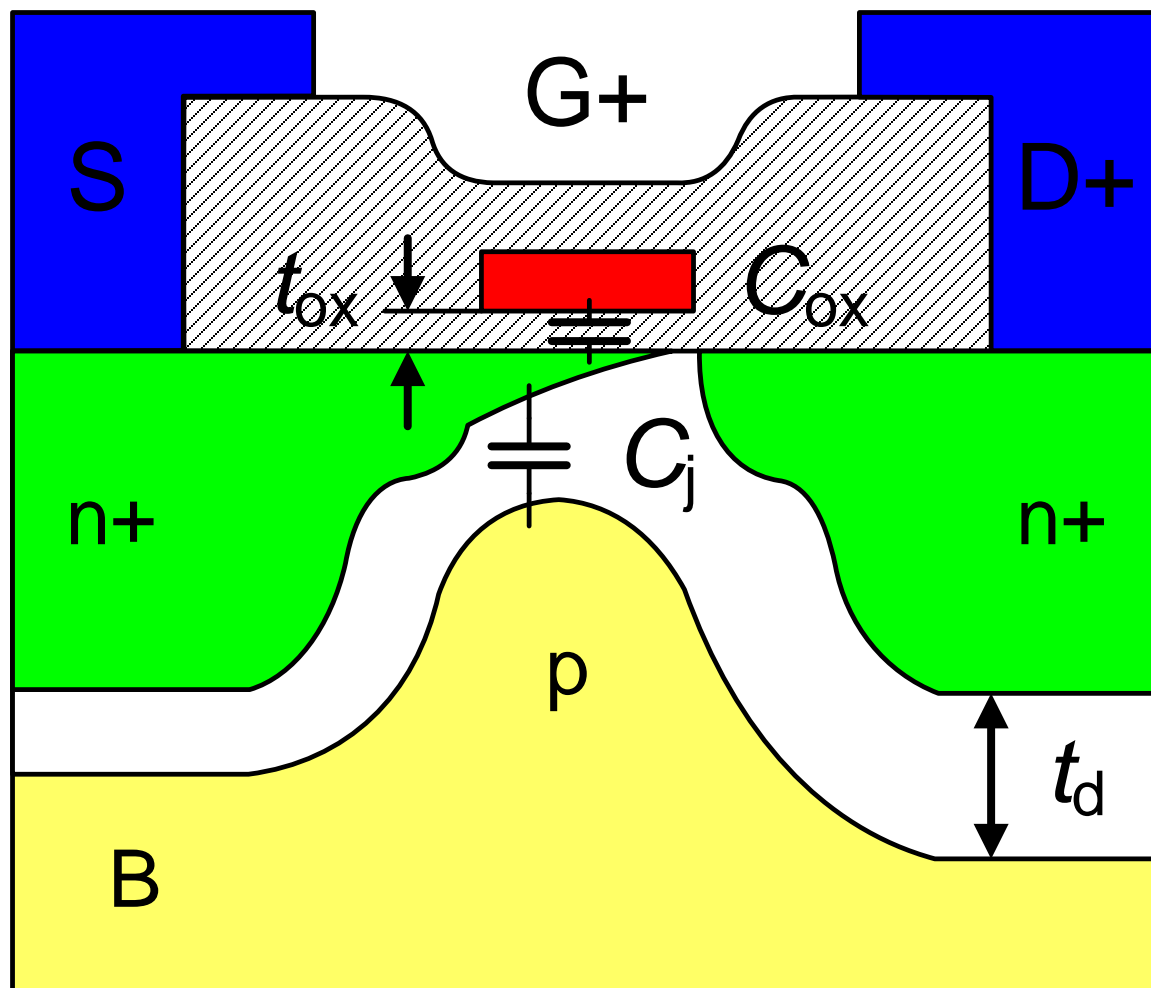
V_{GC} 的阈值电压

$$\begin{aligned}
 V_{TH,GC} &= V_{TH,GB} - V_{CB} = |2\phi_F| + \phi_{MS} - \frac{Q_{j0}}{C_{ox}} - \frac{Q_{SS}}{C_{ox}} - \frac{Q_j - Q_{j0}}{C_{ox}} \\
 &= V_{TH0} + Y(\sqrt{|2\phi_F| + V_{CB}} - \sqrt{|2\phi_F|})
 \end{aligned}$$

耗尽电容与栅氧电容之比:

$$\frac{C_{bc}}{C_{gc}} = \frac{C_j}{C_{ox}} = \frac{Y}{2\sqrt{|2\phi_F| + V_{CB}}} = n - 1$$

MOST版图： C_{ox} 和 C_j



$$C_j = \frac{\epsilon_{si}}{t_d}$$

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}}$$

$$\frac{C_j}{C_{ox}} = n-1$$

MOST版图： C_{ox} 和 C_j 的值

$$C_j = \frac{\epsilon_{si}}{t_d} \quad t_d = \left[\frac{2\epsilon_{si} (|2\phi_F| + V_{DB})}{qN_B} \right]^{1/2}$$

$$\epsilon_{si} = 1 \text{ pF/cm}$$

$$\epsilon_{ox} = 0.34 \text{ pF/cm}$$

$$N_B = 4 \times 10^{17} \text{ cm}^{-3}$$

$$|2\phi_F| = 0.6 \text{ V}$$

$$q = 1.6 \times 10^{-19} \text{ C}$$

例如： $L = 0.35 \mu\text{m}$ $W/L = 8$

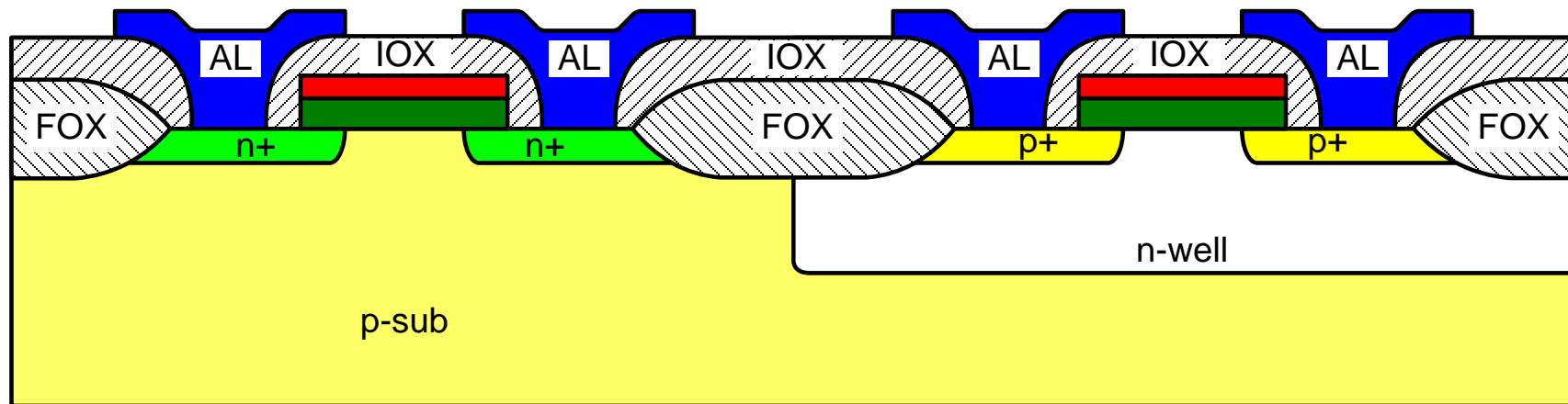
$$V_{DB} = 3.3 \text{ V}$$

$$t_d = 0.11 \mu\text{m} \quad \Rightarrow \quad C_j \approx 1 \times 10^{-7} \text{ F/cm}^2 = 1 \text{ fF}/\mu\text{m}^2$$

$$t_{ox} = \frac{L_{\min}}{50} \Rightarrow t_{ox} = 7 \text{ nm} \Rightarrow C_{ox} = 5 \times 10^{-7} \text{ F/cm}^2 = 5 \text{ fF}/\mu\text{m}^2$$

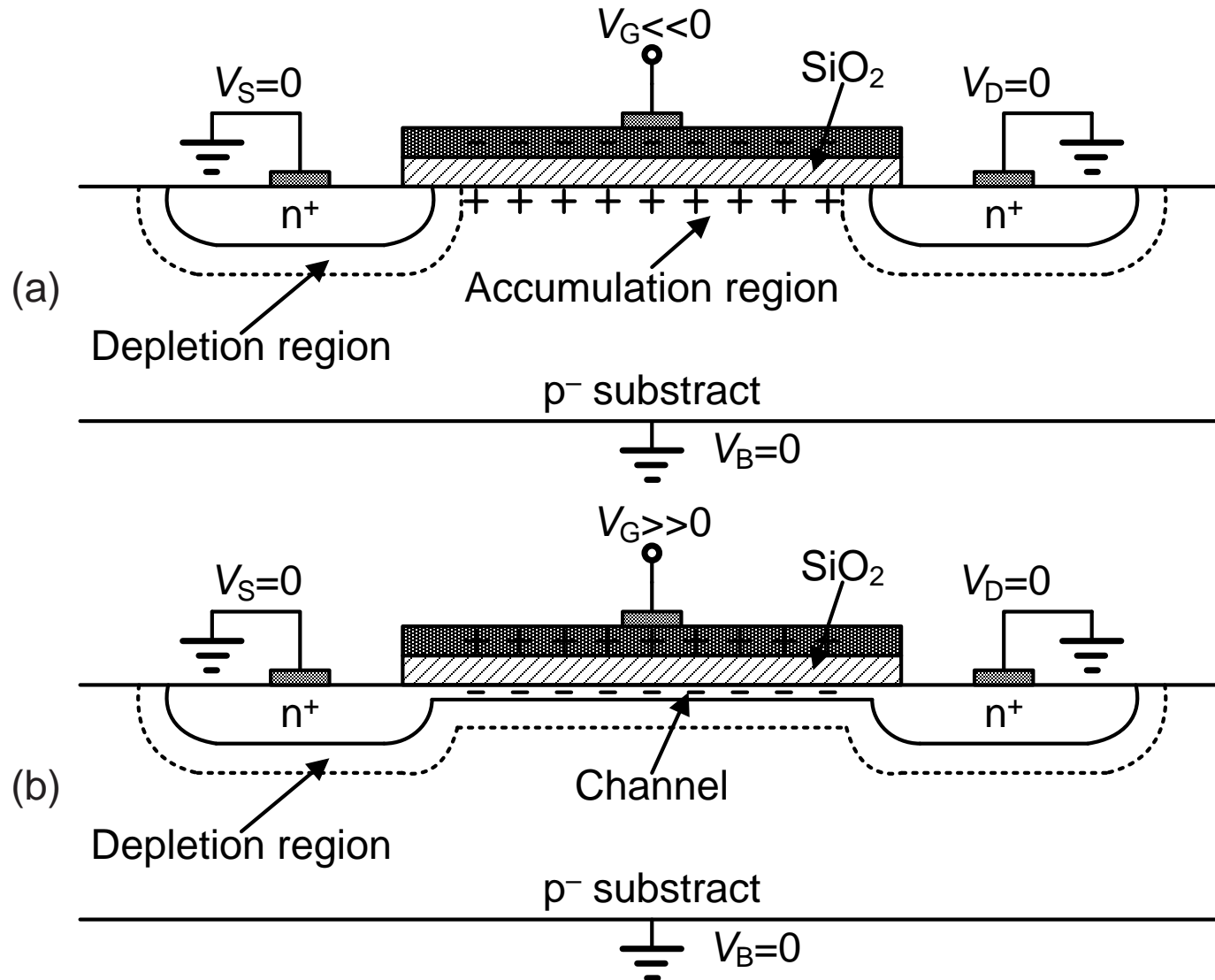
$$\frac{C_j}{C_{ox}} = n-1 \approx 0.2$$

N阱CMOS工艺



$$N_{n\text{-well}} \gg N_{p\text{-sub}}, \quad n_{p\text{mos}} > n_{n\text{mos}}!$$

大信号工作原理：沟道的形成



方块电阻：(1)

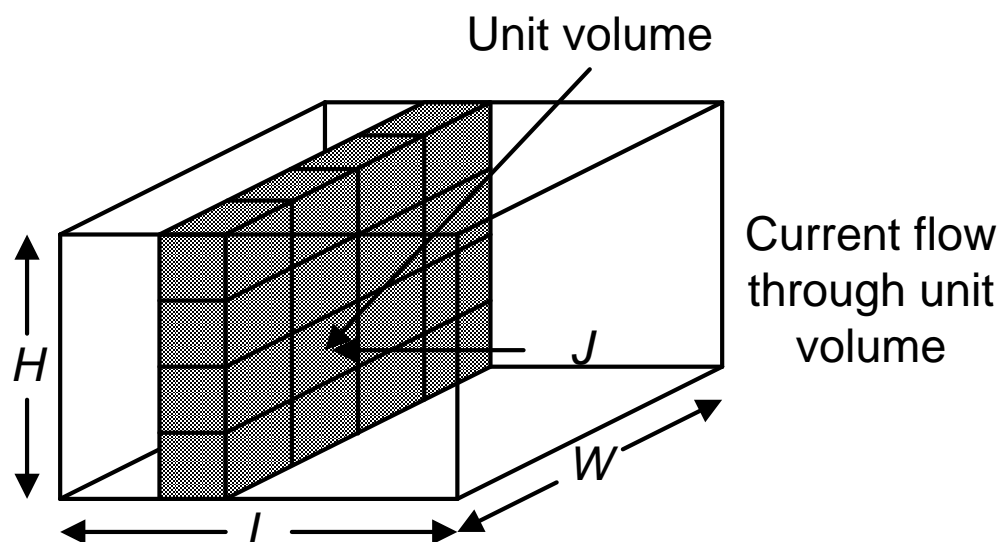
n型半导体的电流密度： $J = \sigma E$ $\sigma = -qn_n\mu_n$

n_n 是单位体积中电子载流子的浓度， μ_n 为电子迁移率。

沟道中的电流： $I = JWH = -qn_n\mu_n WHE$

其中 W 为沟道宽度，

H 为沟道的厚度。



Current flowing through a unit volume.

方块电阻：(2)

沟道中的电场强度： $E = -\frac{dV}{dx}$ $qn_n\mu_n WHdV = Idx$

沟道中的电流：

$$I = qn_n\mu_n WH \frac{dV}{dx} \int_0^L Idx = \int_0^V qn_n\mu_n WHdV \quad I = \frac{qn_n\mu_n WH}{L} V$$

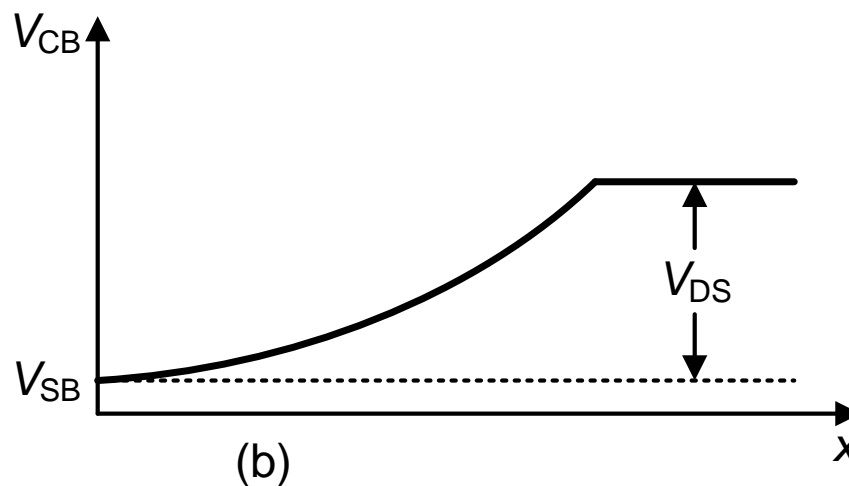
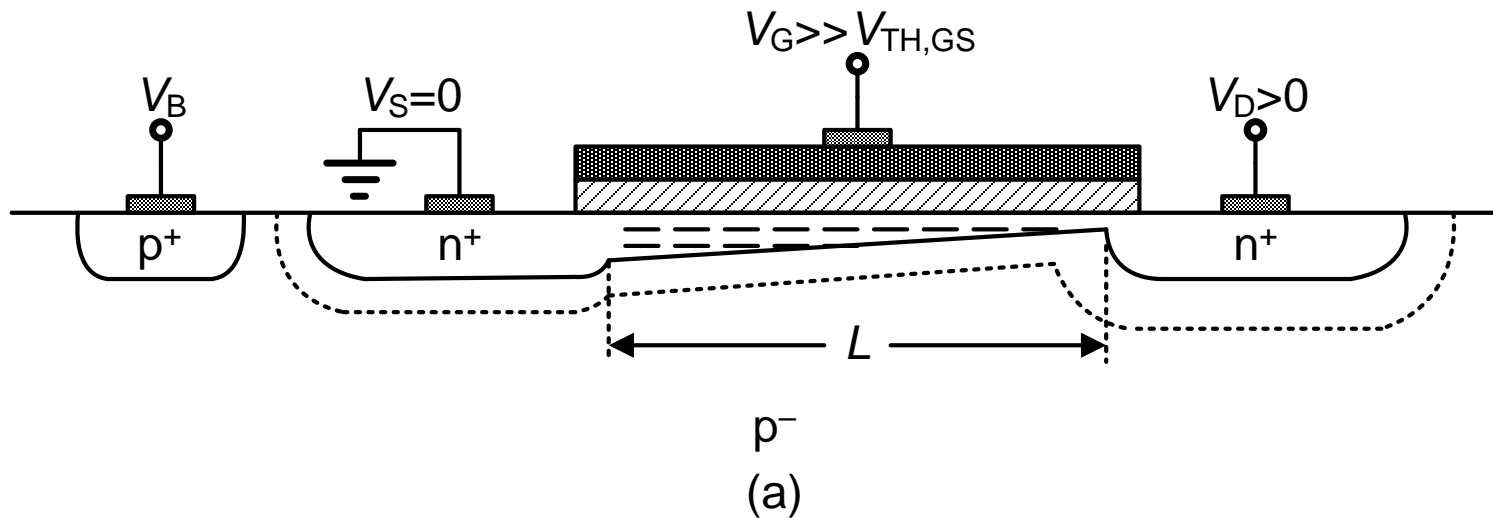
沟道总电阻：

$$R = \frac{V}{I} = \frac{L}{qn_n\mu_n WH} = R_{\square} \frac{L}{W}$$

其中方块电阻：

$$R_{\square} = \frac{1}{qn_n\mu_n H} = \frac{1}{\sigma H}$$

大信号工作原理：线性区



I-V关系式：(1)

在MOS管中，沟道电荷密度 $n_n(x)$ 不是常数，单位面积的电荷密度：

$$Q_n(x) = qn_n(x)H = C_{ox} \{V_{GC}(x) - V_{TH,GC}[V_{CB}(x)]\}$$

$$I_D = W\mu_n Q_n(x) \frac{dV_{CS}(x)}{dx}$$

$$\int_0^L I_D dx = \int_0^{V_{DS}} W\mu_n C_{ox} \{V_{GC}(x) - V_{TH,GC}[V_{CB}(x)]\} dV_{CS}(x)$$

$$V_{GC}(x) = V_{GS} - V_{CS}(x) \quad V_{CB}(x) = V_{CS}(x) + V_{SB}$$

$$V_{TH,GC}[V_{CB}(x)] = V_{TH0} + \gamma(\sqrt{|2\Phi_F| + V_{CB}(x)} - \sqrt{|2\Phi_F|})$$

I-V关系式：(2)

$$\begin{aligned}
 V_{\text{TH,GC}}[V_{\text{CB}}(x)] &= V_{\text{TH,GS}} + \gamma(\sqrt{|2\Phi_{\text{F}}| + V_{\text{CB}}(x)} - \sqrt{|2\Phi_{\text{F}}| + V_{\text{SB}}}) \\
 &= V_{\text{TH,GS}} + \gamma \frac{V_{\text{CB}}(x) - V_{\text{SB}}}{\sqrt{|2\Phi_{\text{F}}| + V_{\text{CB}}(x)} + \sqrt{|2\Phi_{\text{F}}| + V_{\text{SB}}}} \\
 &\approx V_{\text{TH,GS}} + \gamma \frac{V_{\text{CS}}(x)}{2\sqrt{|2\Phi_{\text{F}}| + V_{\text{SB}}}} = V_{\text{TH,GS}} + (n-1)V_{\text{CS}}(x)
 \end{aligned}$$

$$\int_0^L I_{\text{D}} dx = \int_0^{V_{\text{DS}}} \mu_{\text{n}} W C_{\text{ox}} \{V_{\text{GS}} - V_{\text{TH,GS}} - nV_{\text{CS}}(x)\} dV_{\text{CS}}(x)$$

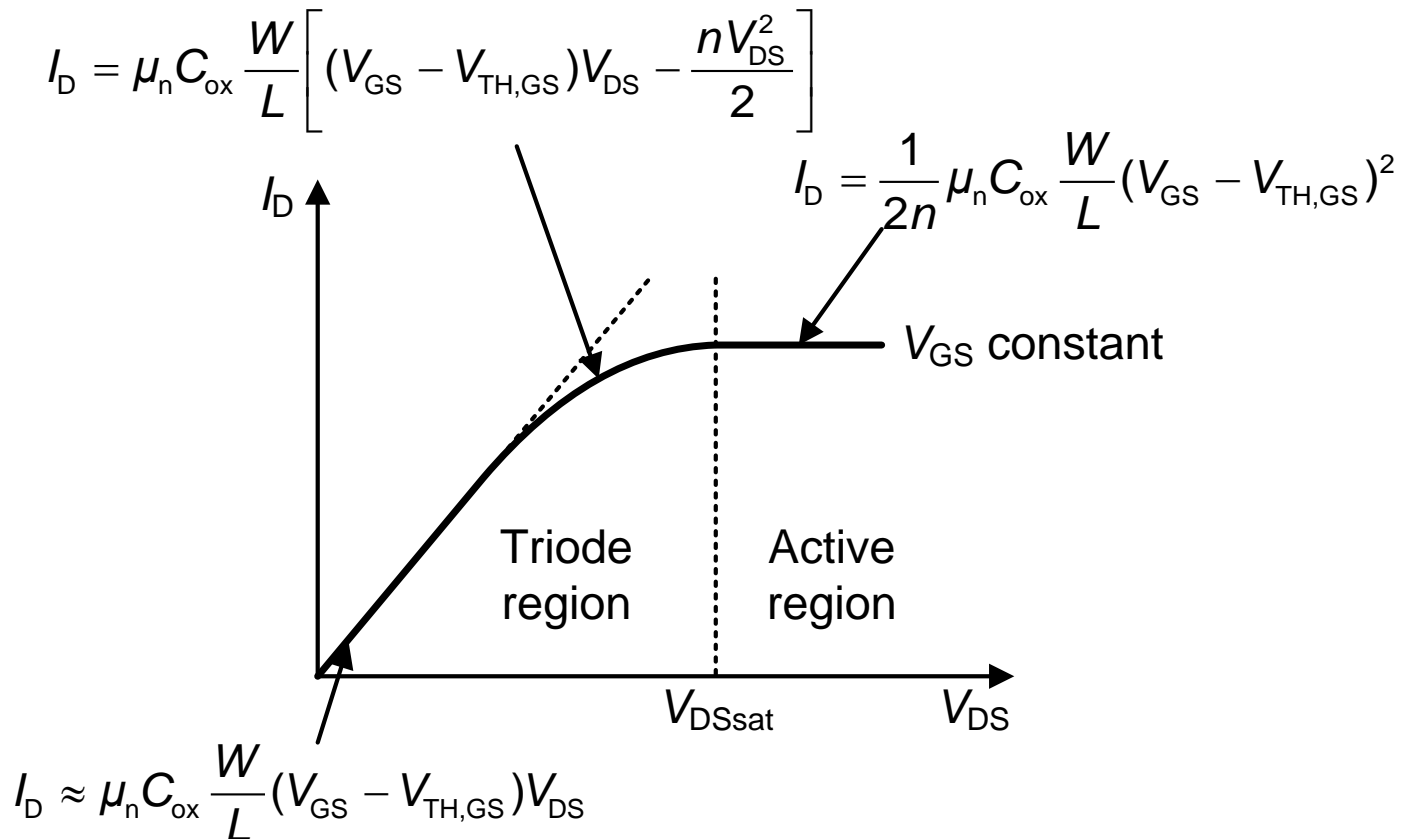
$$I_{\text{D}} = \mu_{\text{n}} C_{\text{ox}} \frac{W}{L} \left[(V_{\text{GS}} - V_{\text{TH,GS}}) V_{\text{DS}} - \frac{nV_{\text{DS}}^2}{2} \right]$$

$$V_{\text{TH,GS}} = V_{\text{TH0}} + \gamma(\sqrt{|2\Phi_{\text{F}}| + V_{\text{SB}}} - \sqrt{|2\Phi_{\text{F}}|})$$

$$n = \frac{\gamma}{2\sqrt{|2\Phi_{\text{F}}| + V_{\text{SB}}}} + 1$$

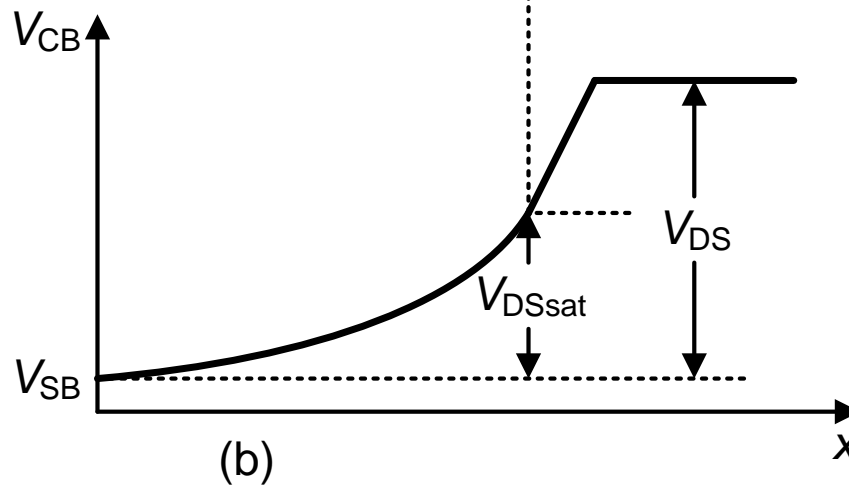
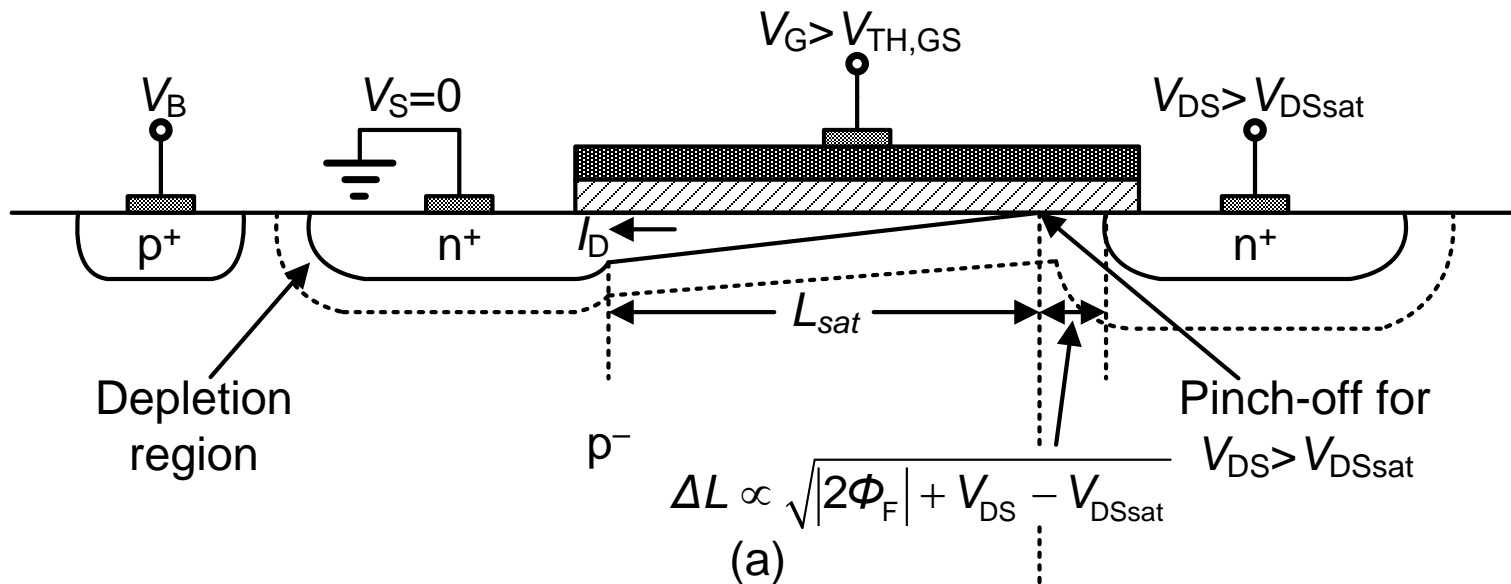
$n = 1.2 \sim 1.5$

I-V关系式：(3)



The I_D versus V_{DS} curve for an ideal MOS transistor. For $V_{DS} > V_{DSsat}$, I_D is approximately constant.

大信号工作原理：饱和区



饱和条件和I-V关系式

饱和条件:

$$V_{GC}(x) - V_{TH,GC}[V_{CB}(x)] = V_{GS} - V_{TH,GS} - nV_{CS}(x) = 0$$

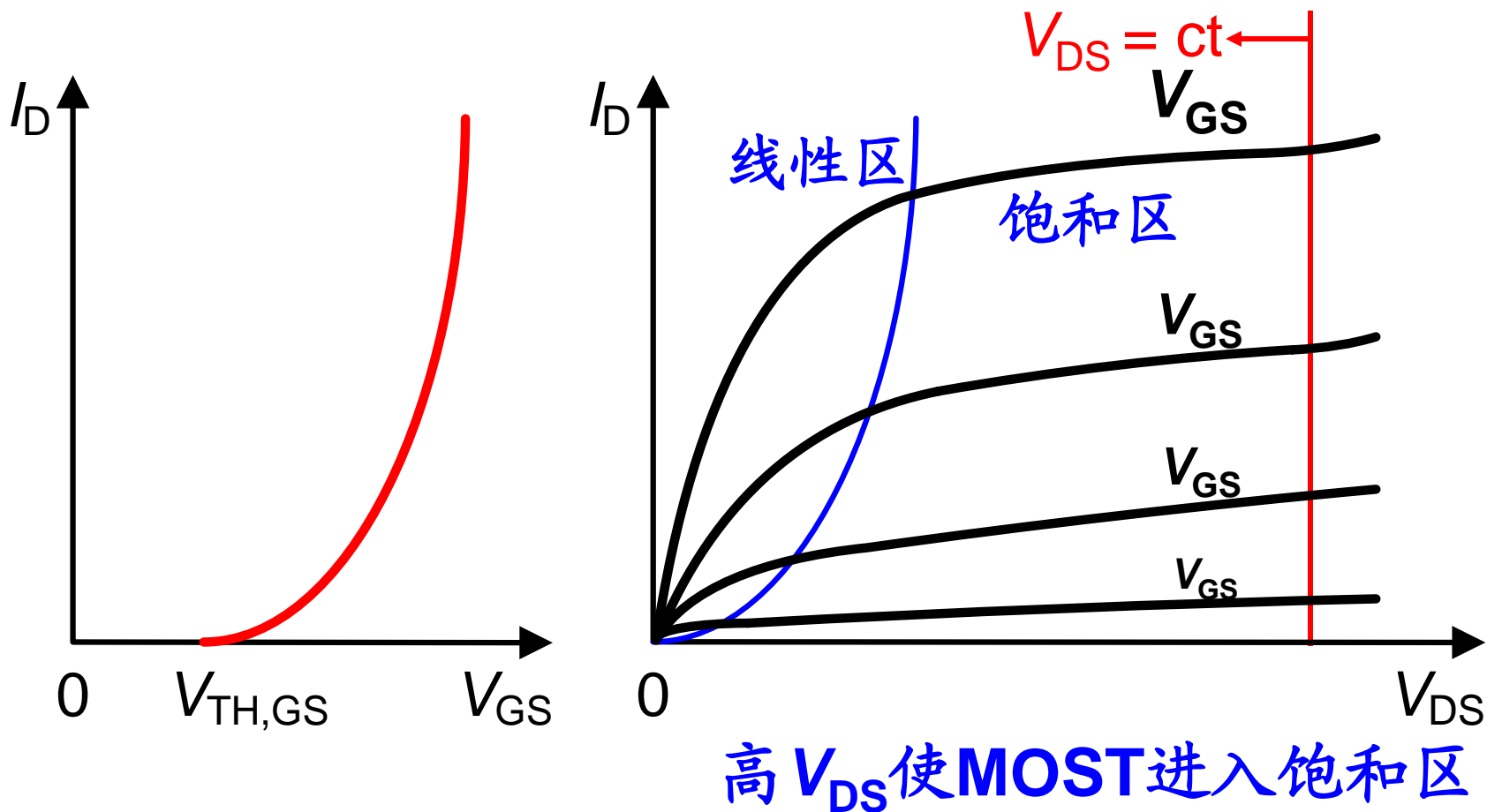
$$V_{CS} = \frac{V_{GS} - V_{TH,GS}}{n}$$

$$V_{DSsat} = \frac{V_{GS} - V_{TH,GS}}{n} = V_{eff}$$

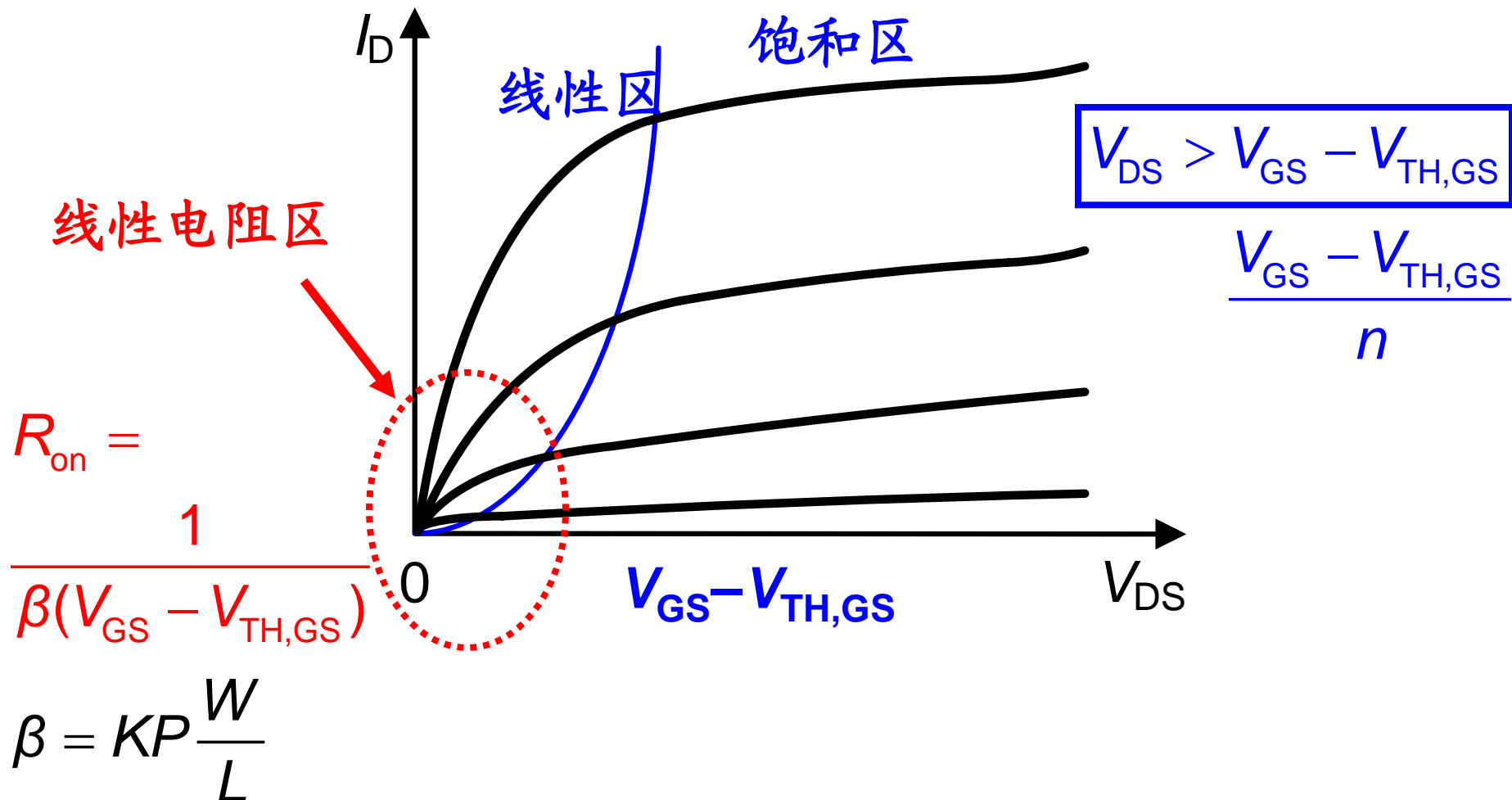
I-V关系式:

$$I_D = \frac{1}{2n} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH,GS})^2$$

MOST的 I_D 与 V_{GS} 和 V_{DS} 的关系



MOST的 V_{DS} 与 I_D 的关系



沟道长度调制效应：(1)

饱和时的沟道长度： $L_{\text{sat}} = L - \Delta L$

$$\Delta L = \left[\frac{2\epsilon_{\text{si}} (|2\Phi_{\text{F}}| + V_{\text{DS}} - V_{\text{DSsat}})}{qN_{\text{B}}} \right]^{1/2} \quad I_{\text{D}} = \frac{1}{2n} \mu_{\text{n}} C_{\text{ox}} \frac{W}{L} (V_{\text{GS}} - V_{\text{TH,GS}})^2$$

$$\frac{\partial I_{\text{D}}}{\partial V_{\text{DS}}} = \frac{\partial I_{\text{D}}}{\partial L} \frac{\partial L}{\partial V_{\text{DS}}} = -\frac{1}{2n} \mu_{\text{n}} C_{\text{ox}} \frac{W}{L^2} (V_{\text{GS}} - V_{\text{TH,GS}})^2 \frac{\partial L}{\partial V_{\text{DS}}} = \frac{I_{\text{D}}}{L} \frac{\partial L}{\partial V_{\text{DS}}}$$

定义厄利电压 V_{A} 为： V_{E} 近似为常数

$$V_{\text{A}} = \frac{I_{\text{D}}}{\partial I_{\text{D}} / \partial V_{\text{DS}}} = L \left(\frac{\partial L}{\partial V_{\text{DS}}} \right)^{-1} = \left[\frac{qN_{\text{B}} (|2\Phi_{\text{F}}| + V_{\text{DS}} - V_{\text{DSsat}})}{\epsilon_{\text{si}}} \right]^{1/2} L$$

$$= V_{\text{E}} L$$

沟道长度调制效应：(2)

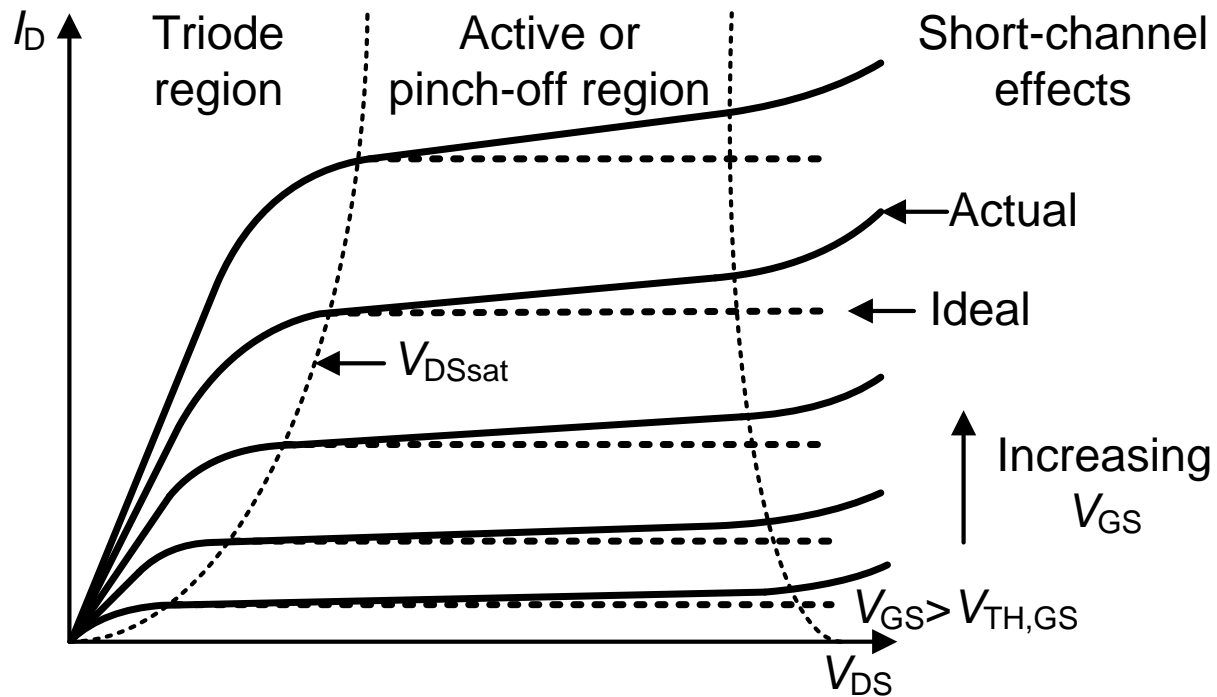
沟道长度调制系数：

$$\lambda = \frac{1}{V_A} = \frac{1}{V_E L}$$

沟道饱和电流：

$$I_D = \frac{1}{2n} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH,GS})^2 [1 + \lambda(V_{DS} - V_{DSsat})]$$

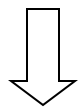
沟道长度调制效应：(3)



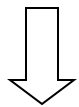
I_D versus V_{DS} for different values of V_{GS} .

MOST的参数 β 、 KP 、 C_{ox} 等

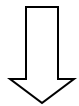
$$\beta = KP \frac{W}{L}$$



$$KP = \mu C_{ox}$$



$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}}$$



$$t_{ox} = \frac{L_{min}}{50}$$

$$KP_p \approx 125 \mu A/V^2$$

$$KP_n \approx 300 \mu A/V^2$$

$$C_{ox} \approx 5 \times 10^{-7} \text{ F/cm}^2$$

$$\epsilon_{si} = 1 \text{ pF/cm}$$

$$\epsilon_{ox} = 0.34 \text{ pF/cm}$$

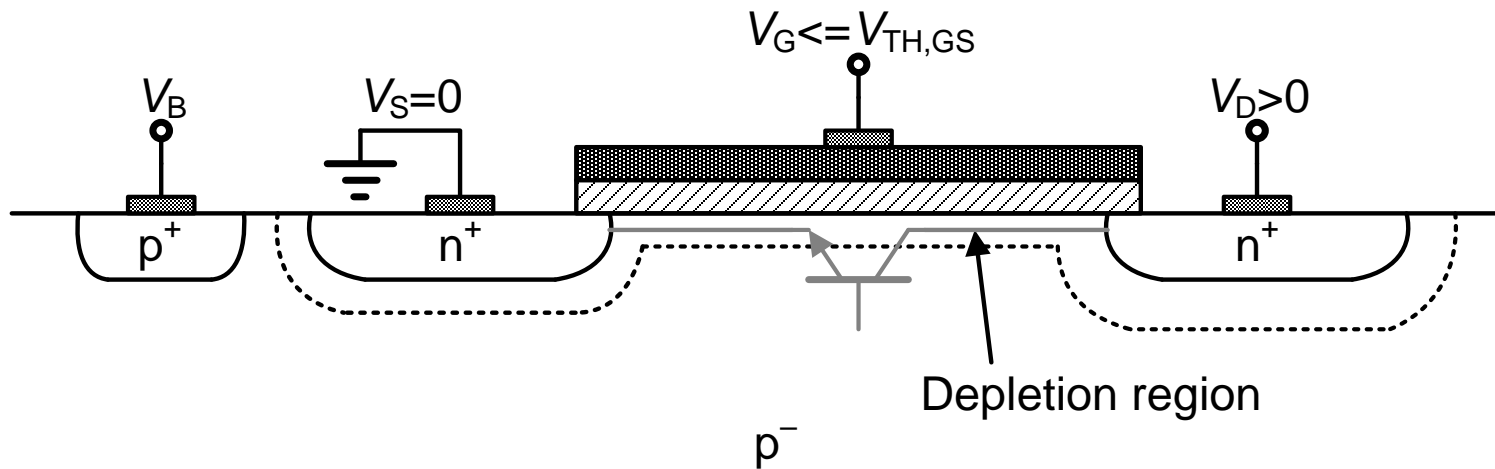
$$t_{ox} = 7 \text{ nm}$$

$$L = 0.35 \mu m$$

$$\mu_p = 250 \text{ cm}^2/Vs$$

$$\mu_n = 600 \text{ cm}^2/Vs$$

大信号工作原理：弱反型(亚阈值)区



The depletion region of subthreshold operation

p 型衬底中源端和漏端的少数载流子浓度:

$$n_p(0) = n_{p0} e^{\frac{\phi_S}{V_T}} \quad n_p(L) = n_{p0} e^{\frac{\phi_S - V_{DS}}{V_T}}$$

其中， n_{p0} 是衬底中的平衡载流子浓度， ϕ_S 是表面势。

I-V关系式：(1)

电子扩散产生的电流：

$$I_D = qAD_n \frac{n_p(0) - n_p(L)}{L} = \frac{W}{L} q t_d D_n n_{p0} e^{\frac{\phi_s}{V_T}} \left(1 - e^{-\frac{V_{DS}}{V_T}}\right)$$

其中 D_n 是电子的扩散系数， A 是电流流过区域的截面积， $A = W \times t_d$ ， W 为 MOS 管宽度， t_d 为耗尽区深度。

在弱反型区，表面势正比于栅源电压：

$$\frac{d\phi_s}{dV_{GS}} = \frac{C_{ox}}{C_j + C_{ox}} = \frac{1}{n} \quad \phi_s = \frac{V_{GS}}{n} + k_1 = \frac{V_{GS} - V_{TH,GS}}{n} + k_2$$

$$k_2 = k_1 + \frac{V_{TH,GS}}{n}$$

I-V关系式：(2)

漏极电流：

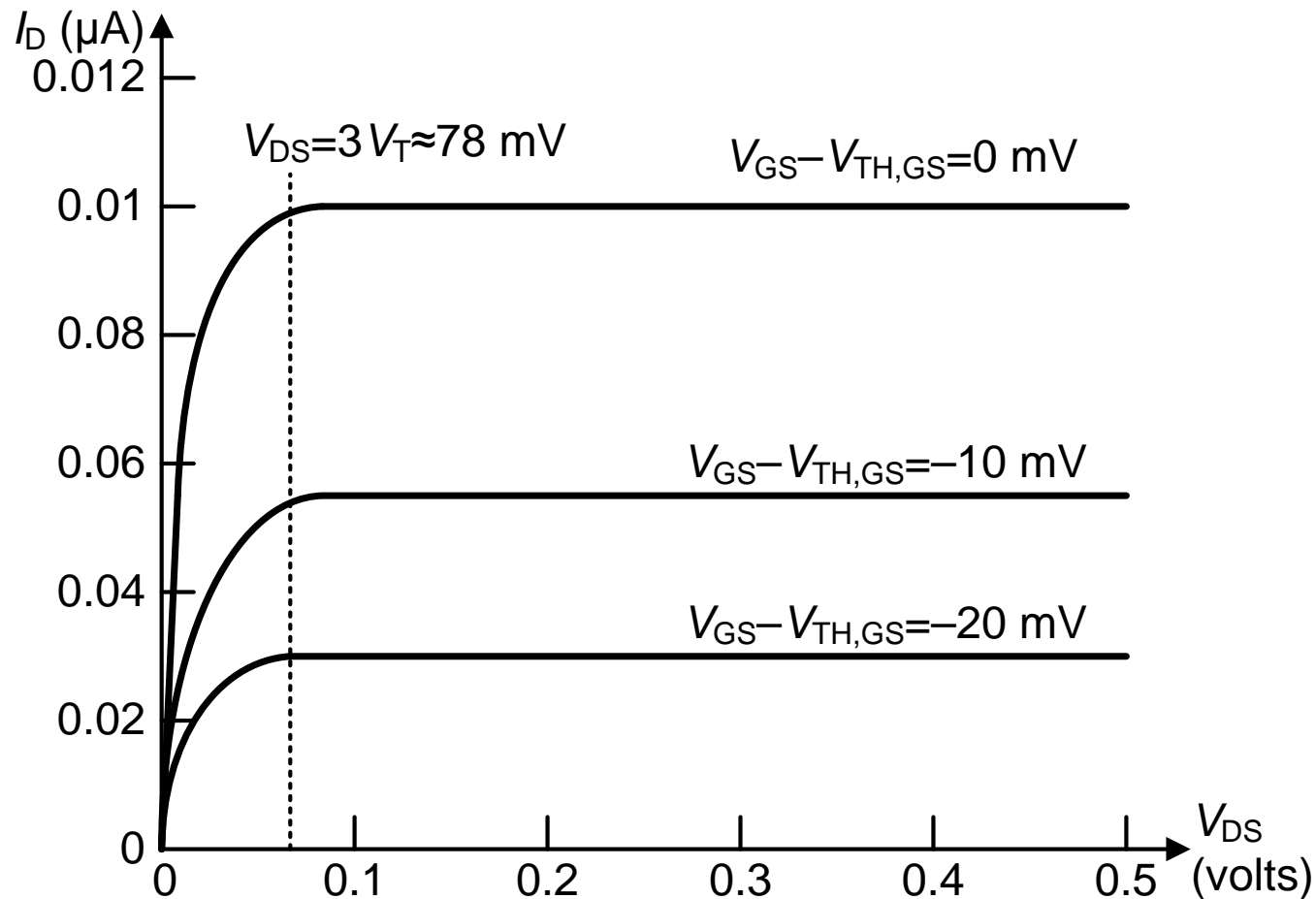
$$I_D = \frac{W}{L} t_d q D_n n_{p0} e^{\frac{k_2}{V_T}} e^{\frac{V_{GS} - V_{TH,GS}}{nV_T}} \left(1 - e^{-\frac{V_{DS}}{V_T}}\right)$$

$$I_D = \frac{W}{L} I_t e^{\frac{V_{GS} - V_{TH,GS}}{nV_T}} \left(1 - e^{-\frac{V_{DS}}{V_T}}\right)$$

其中，

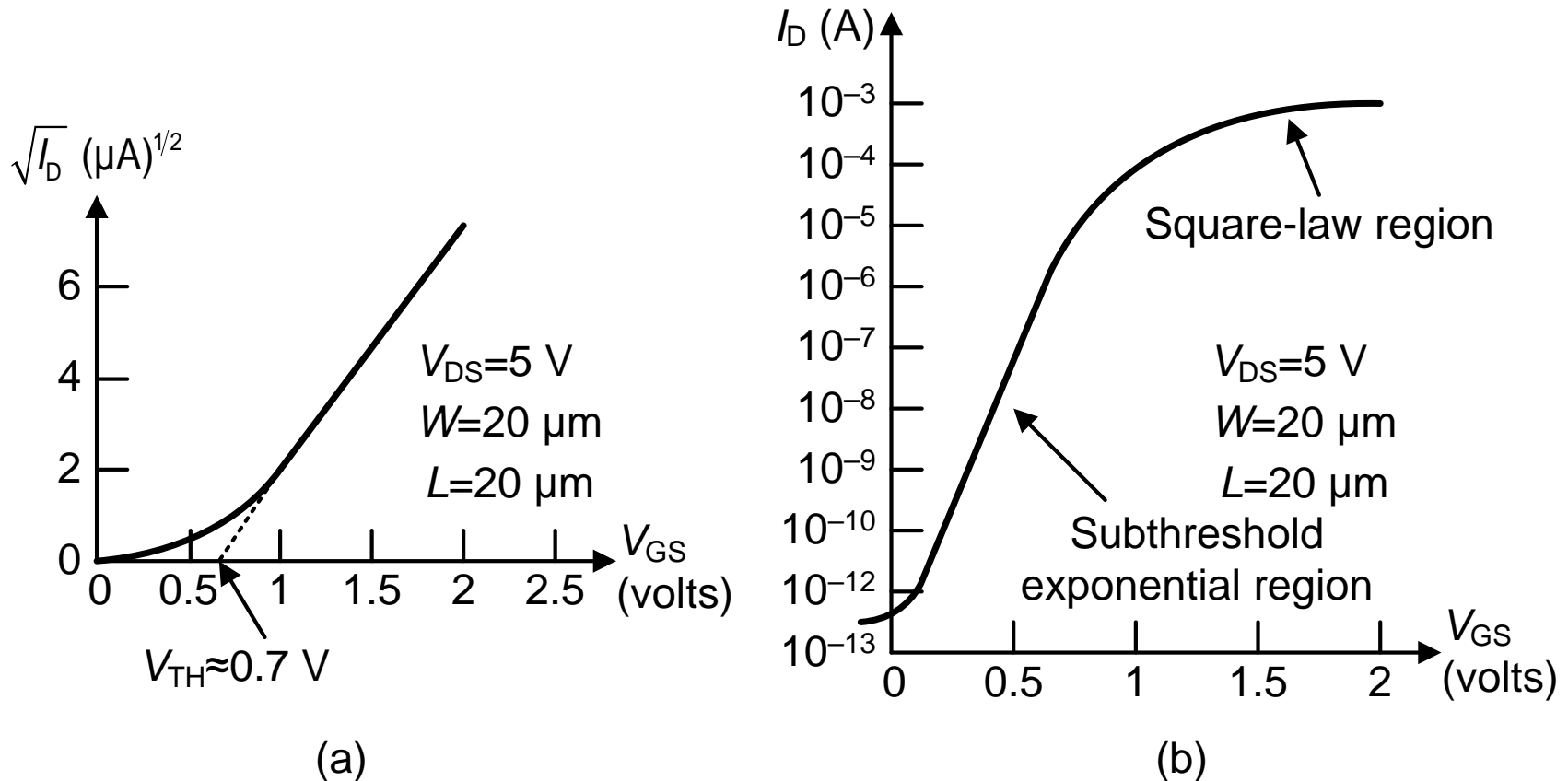
$$I_t = t_d q D_n n_{p0} e^{\frac{k_2}{V_T}}$$

亚阈值区的典型 I - V 曲线



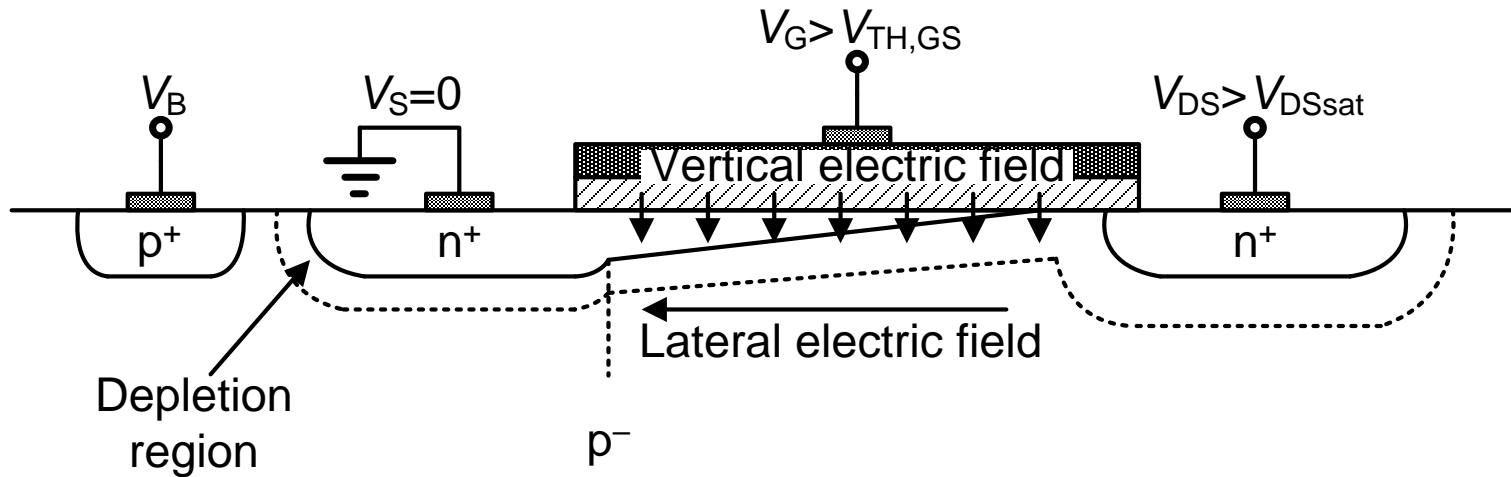
Drain current versus drain-source voltage in weak inversion.

亚阈值区和饱和区的典型 I - V 曲线



Drain current versus gate-source voltage in weak inversion with a
(a) square root (b) logarithmic scale.

大信号工作原理：速度饱和区



An NMOS device in active mode (saturation) identifying the lateral and vertical electric field components.

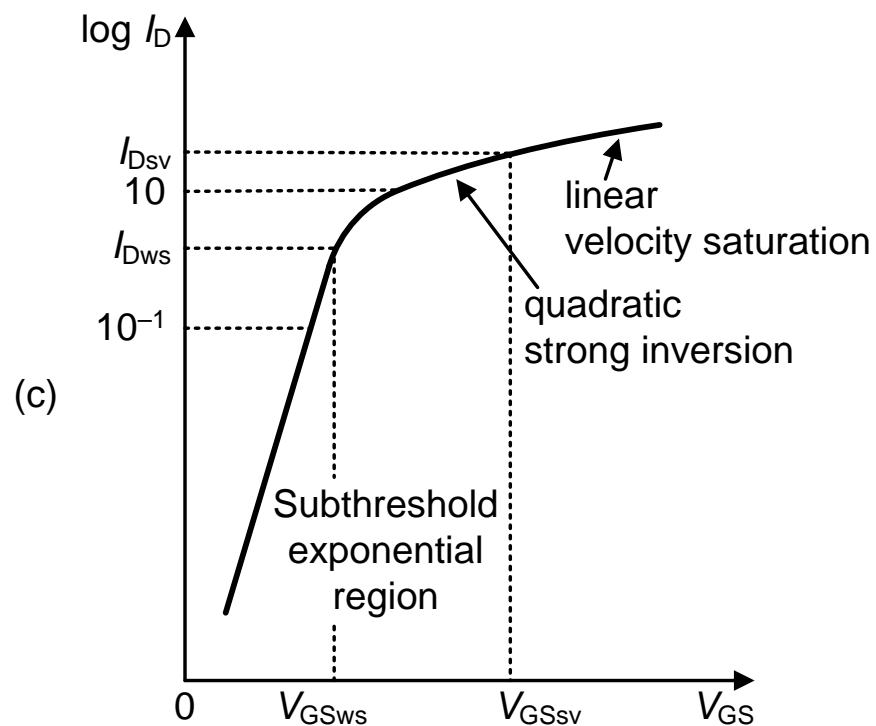
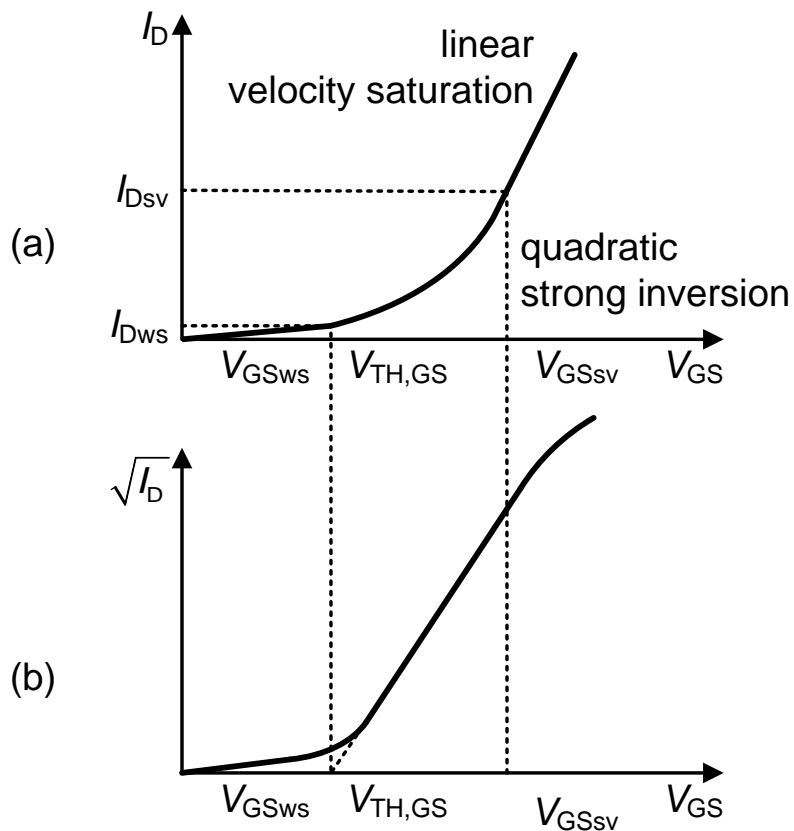
在临界电场 E_{crit} 下的速度定义为散射极限速度 v_{scl} :

$$v_{scl} = \mu_n E_{crit}$$

速度饱和时的电流:

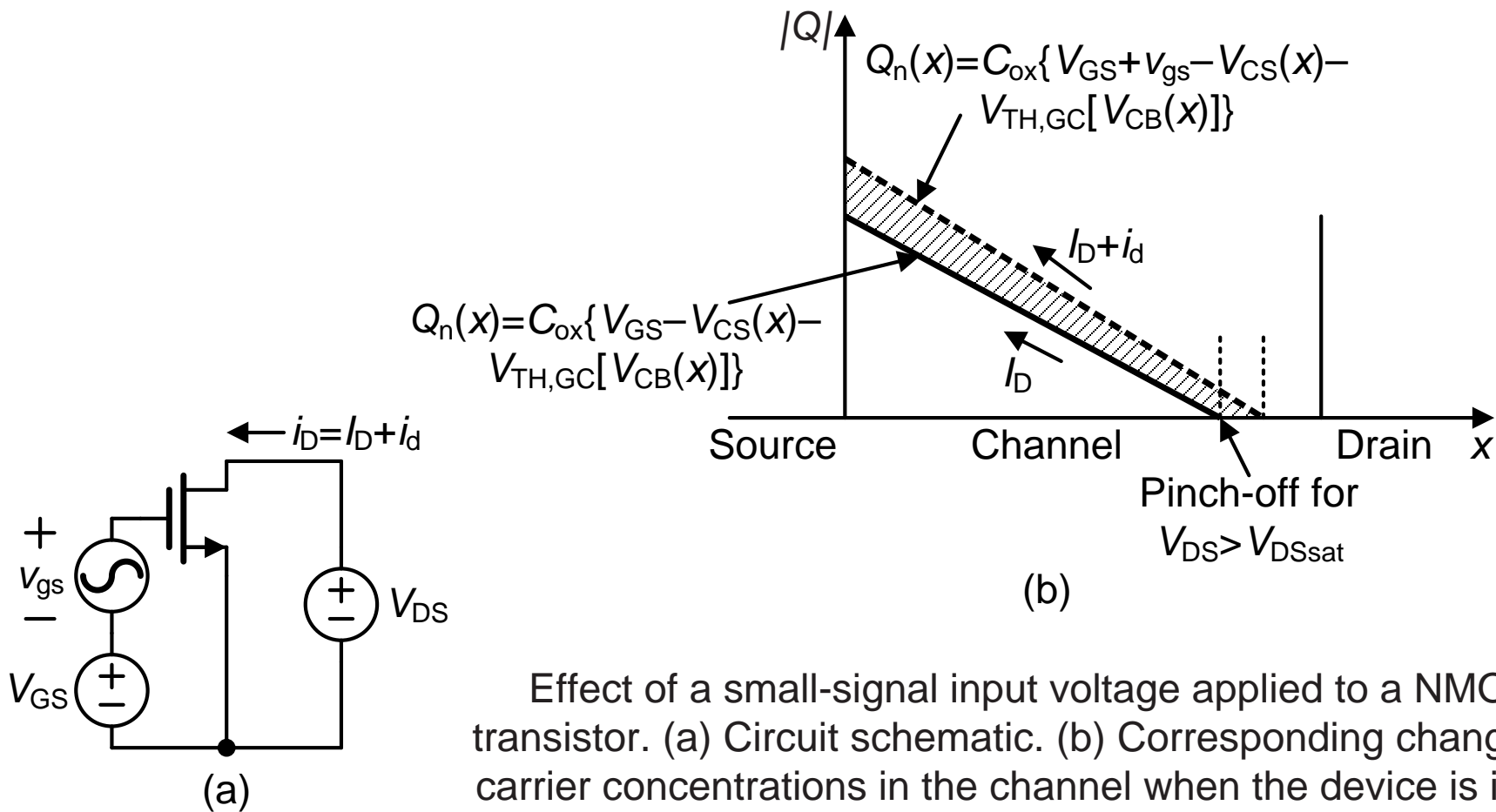
$$I_D = WC_{ox} (V_{GS} - V_{TH,GS}) v_{scl}$$

三个工作区域的I-V曲线



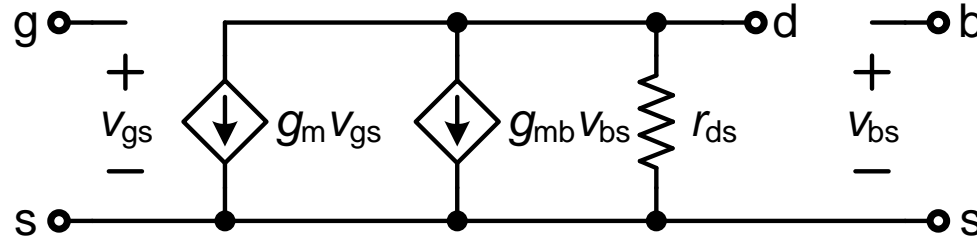
$I_D/V_{GS}=0$ characteristic with a (a) linear, (b) square root, and (c) logarithmic current scale.

小信号模型



Effect of a small-signal input voltage applied to a NMOS transistor. (a) Circuit schematic. (b) Corresponding changes in carrier concentrations in the channel when the device is in the active region.

低频小信号模型：栅跨导(1)



The low-frequency, small-signal model for an active MOS transistor.

栅跨导: $g_m = \frac{\partial I_D}{\partial V_{GS}}$

线性区栅跨导 $g_{m,tri}$:

$$g_{m,tri} = \mu_n C_{ox} \frac{W}{L} V_{DS}$$

饱和区栅跨导 $g_{m,si}$:

$$g_{m,si} = \frac{1}{n} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH,GS}) [1 + \lambda (V_{DS} - V_{DSsat})]$$

低频小信号模型：栅跨导(2)

若 $\lambda(V_{DS} - V_{DSsat}) \ll 1$

$$g_{m,si} = \frac{1}{n} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH,GS}) = \sqrt{\frac{2}{n} \mu_n C_{ox} \frac{W}{L} I_D} = \frac{2I_D}{V_{GS} - V_{TH,GS}}$$

弱反型区栅跨导 $g_{m,wi}$:

$$g_{m,wi} = \frac{W}{L} \frac{I_t}{nV_T} e^{\frac{V_{GS} - V_{TH,GS}}{nV_T}} (1 - e^{-\frac{V_{DS}}{V_T}}) = \frac{I_D}{nV_T} = \frac{I_D}{V_T} \frac{C_{ox}}{C_j + C_{ox}}$$

速度饱和区栅跨导 $g_{m,vs}$:

$$g_{m,vs} = WC_{ox} v_{scl}$$

体跨导：(1)

$$g_{mb} = \frac{\partial I_D}{\partial V_{BS}} = \frac{\partial I_D}{\partial V_{TH,GS}} \frac{\partial V_{TH,GS}}{\partial V_{BS}} = - \frac{\partial I_D}{\partial V_{GS}} \frac{\partial V_{TH,GS}}{\partial V_{BS}} = g_m (n-1)$$

$$\frac{\partial V_{TH,GS}}{\partial V_{BS}} = - \frac{V}{2\sqrt{|2\phi_F| + V_{SB}}} = -(n-1)$$

线性区体跨导 $g_{mb,tri}$:

$$g_{mb,tri} = -\mu_n C_{ox} \frac{W}{L} V_{DS} \frac{\partial V_{TH,GS}}{\partial V_{BS}} = (n-1) \mu_n C_{ox} \frac{W}{L} V_{DS} = (n-1) g_{m,tri}$$

饱和区体跨导 $g_{mb,si}$

$$g_{mb,si} = -\frac{1}{n} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH,GS}) [1 + \lambda(V_{DS} - V_{DSsat})] \frac{\partial V_{TH,GS}}{\partial V_{BS}}$$

$$= (n-1) g_{m,si}$$

体跨导：(2)

弱反型区体跨导 $g_{mb,wi}$:

$$g_{mb,wi} = -\frac{1}{nV_T} \frac{W}{L} I_t e^{\frac{V_{GS}-V_{TH,GS}}{nV_T}} \left(1 - e^{-\frac{V_{DS}}{V_T}}\right) \frac{\partial V_{TH,GS}}{\partial V_{BS}} = \frac{(n-1)I_D}{nV_T}$$

$$= (n-1)g_{m,wi}$$

速度饱和区体跨导 $g_{mb,vs}$

$$g_{mb,vs} = -WC_{ox} v_{scl} \frac{\partial V_{TH,GS}}{\partial V_{BS}} = (n-1)g_{m,vs}$$

输出阻抗

$$r_{ds} = \frac{\partial V_{DS}}{\partial I_D} = \left(\frac{\partial I_D}{\partial V_{DS}} \right)^{-1}$$

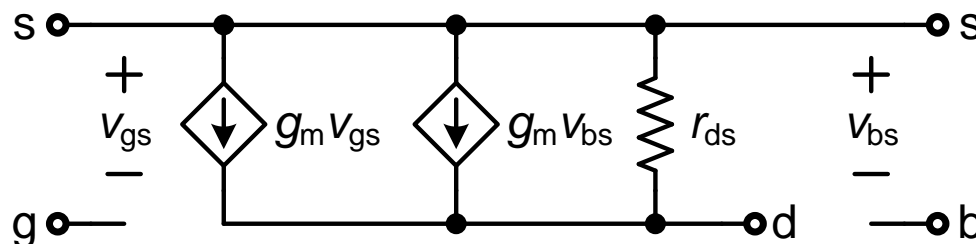
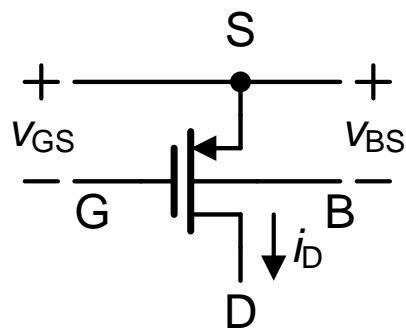
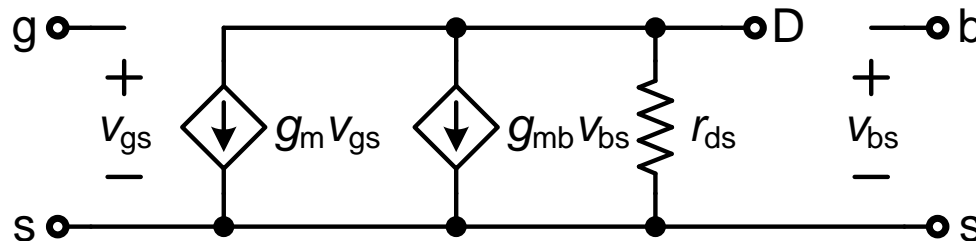
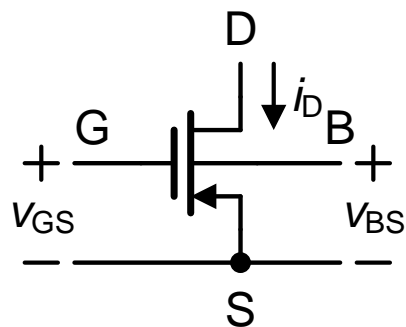
线性区输出阻抗 $r_{ds,tri}$:
$$r_{ds,tri} = \frac{1}{\mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH,GS} - nV_{DS})}$$

饱和区输出阻抗 $r_{ds,si}$:
$$r_{ds,si} \approx \frac{V_A}{I_D} = \frac{1}{\lambda I_D} = \frac{V_E L}{I_D}$$

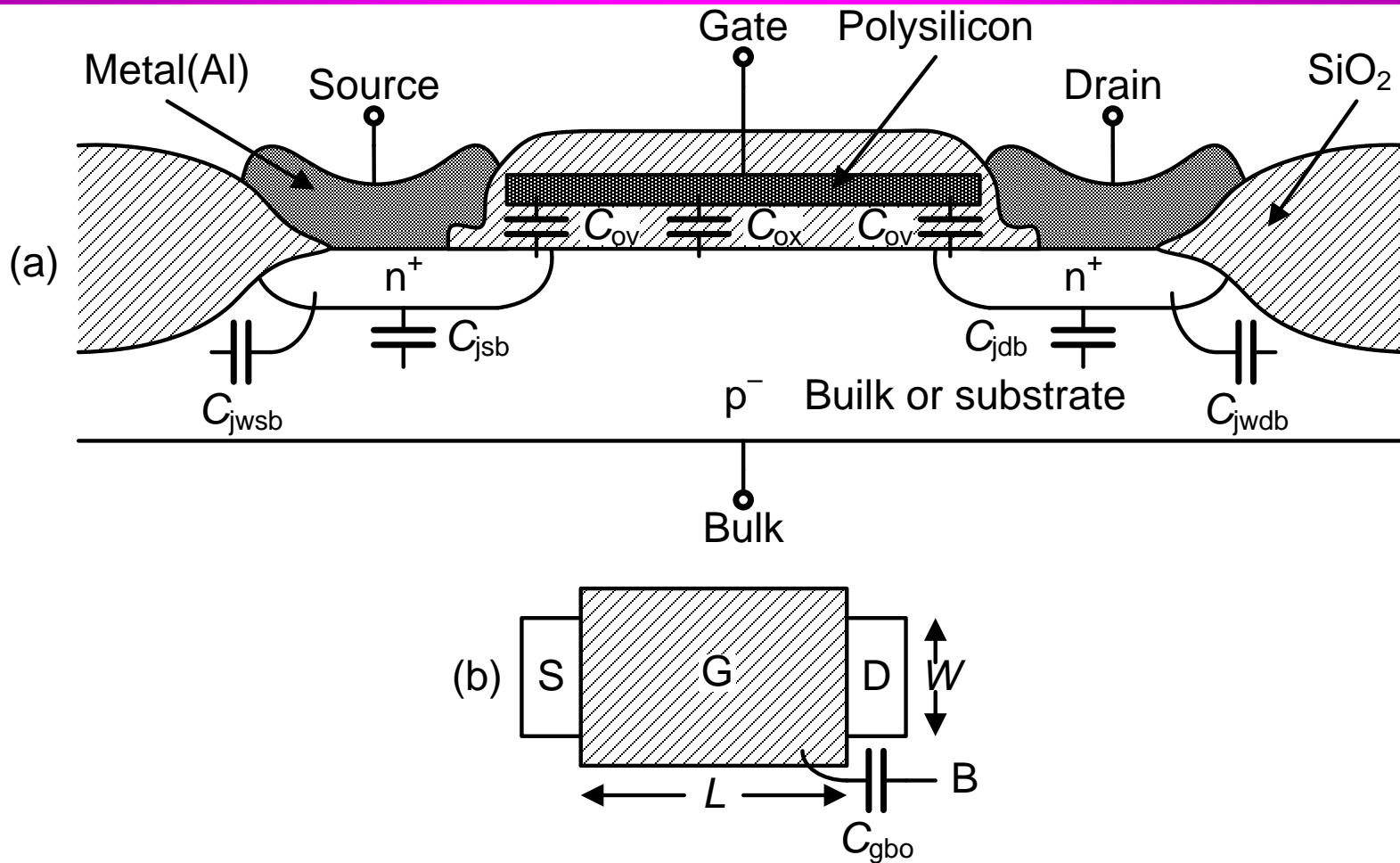
弱反型区输出阻抗 $r_{ds,wi}$:
$$r_{ds,wi} = \frac{V_T}{\frac{W}{L} I_t e^{\frac{V_{GS} - V_{TH,GS}}{nV_T}} e^{-\frac{V_{DS}}{V_T}}} = \frac{V_T}{I_D} (e^{\frac{V_{DS}}{V_T}} - 1)$$

速度饱和区输出阻抗 $r_{ds,vs}$:
$$\frac{\partial I_D}{\partial V_{DS}} = 0 \quad r_{ds,vs} \rightarrow \infty$$

PMOST的小信号模型

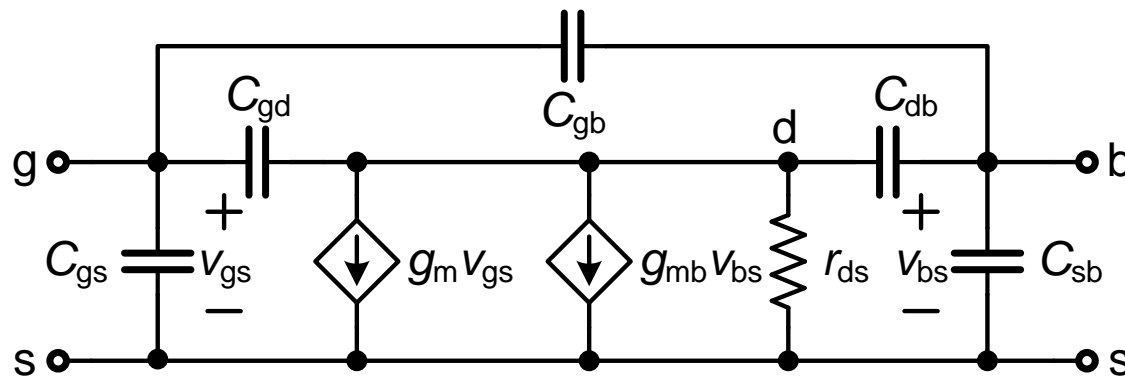


高频小信号模型: (1)



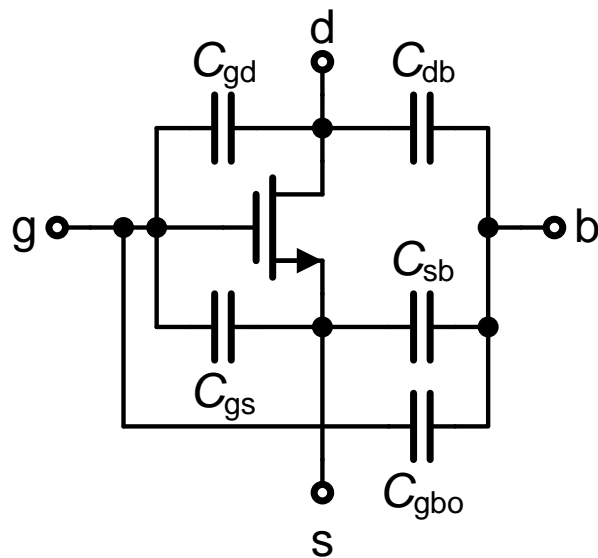
(a) A cross section of an n-channel MOS transistor showing the small-signal capacitances. (b) Top view of an NMOS

高频小信号模型：(2)



The high-frequency, small-signal model for a MOS transistor.

栅寄生电容 C_{gs} 和 C_{gd} : (1)



Terminal capacitance in a NMOS

线性区:

$$C_{gs} = C_{gd} = \frac{C_{ox} WL}{2} + C_{ov}$$

其中 C_{ov} 为栅与源(漏)的交叠电容,

$$C_{ov} = WL_{ov} C_{ox}$$

弱反型区:

$$C_{gs} = C_{gd} = C_{ov} = WL_{ov} C_{ox}$$

交叠电容:
$$C_{gbo} = 2W_{ov} LC_{ox}$$

栅寄生电容 C_{gs} 和 C_{gd} : (2)

饱和区和速度饱和区，沟道中的总电荷和沟道电流：

$$Q_T = WC_{ox} \int_0^L \{V_{GS} - V_{TH,GS} - nV_{CS}(x)\} dx$$

$$I_D = W\mu_n C_{ox} [V_{GS} - V_{TH,GS} - nV_{CS}(x)] \frac{dV_{CS}(x)}{dx}$$

$$Q_T = \frac{W^2 C_{ox}^2 \mu_n}{I_D} \int_0^{\frac{V_{GS} - V_{TH,GS}}{n}} \{V_{GS} - V_{TH,GS} - nV_{CS}(x)\}^2 dV_{CS}(x)$$

$$= \frac{2}{3} WLC_{ox} (V_{GS} - V_{TH,GS})$$

$$C'_{gs} = \frac{\partial Q_T}{\partial V_{GS}} = \frac{2}{3} WLC_{ox}$$

$$C_{gs} = C'_{gs} + C_{ov} = \frac{2}{3} C_{ox} WL + C_{ov}$$

$$C_{gd} = C_{ov}$$

源/漏寄生结电容

$$C_{jsbt} = A_S C_{jsb} + P_S C_{jwsb}$$

$$C_{jdbt} = A_D C_{jdb} + P_D C_{jwdb}$$

其中 A_S 和 A_D 分别为源和漏的底部面积， P_S 和 P_D 分别为源和漏的侧壁周长。

源衬和漏衬的面结电容:

$$C_{jsb} = \frac{C_j}{\sqrt{1 + \frac{V_{sb}}{\Phi_0}}} \quad C_{jdb} = \frac{C_j}{\sqrt{1 + \frac{V_{db}}{\Phi_0}}}$$

源衬和漏衬的边墙结电容:

其中 $m=1/3\sim 1/2$

$$C_{jwsb} = \frac{C_{jw}}{\left(1 + \frac{V_{sb}}{\Phi_0}\right)^m} \quad C_{jwdb} = \frac{C_{jw}}{\left(1 + \frac{V_{db}}{\Phi_0}\right)^m}$$

背栅寄生电容 C_{bs} 和 C_{bd} : (1)

线性区:

$$C_{sb} = \frac{1}{2}C_{bc} + C_{jsbt} \quad C_{db} = \frac{1}{2}C_{bc} + C_{jdbt}$$

饱和区和速度饱和区:

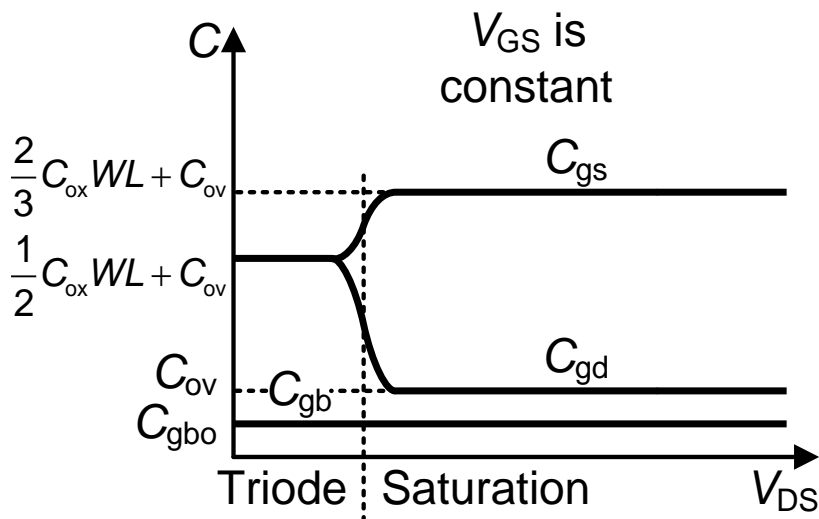
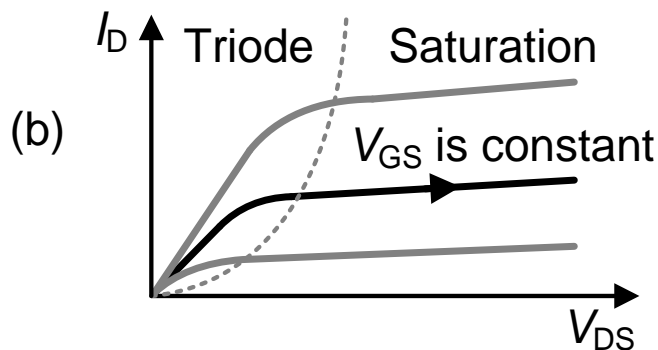
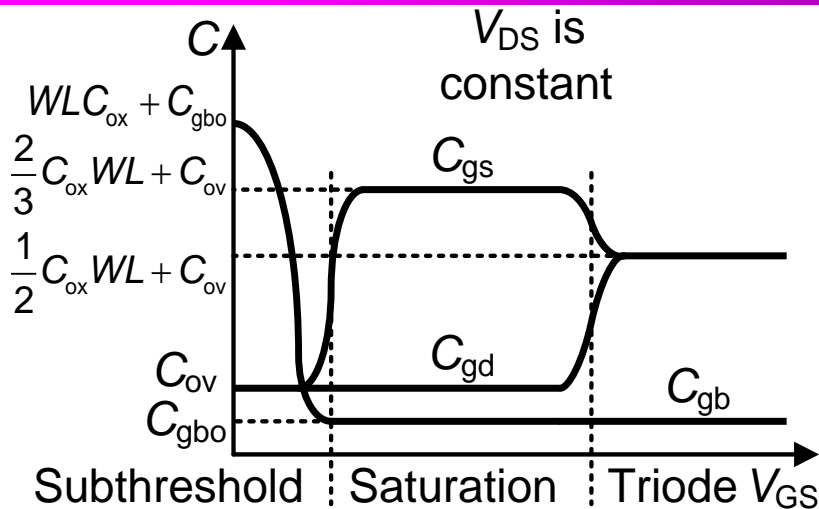
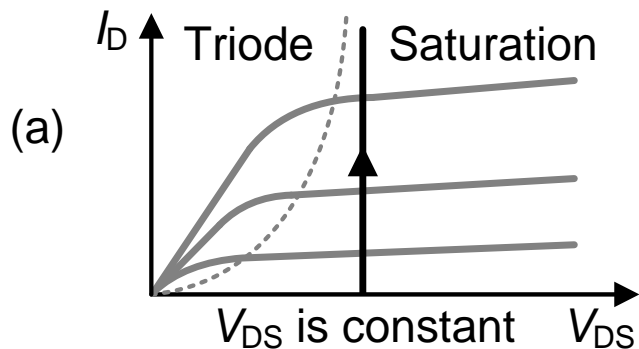
$$C_{sb} = \frac{2}{3}C_{bc} + C_{jsbt} \quad C_{db} = C_{jdbt}$$

弱反型区:

$$C_{sb} = C_{jsbt} \quad C_{db} = C_{jdbt}$$

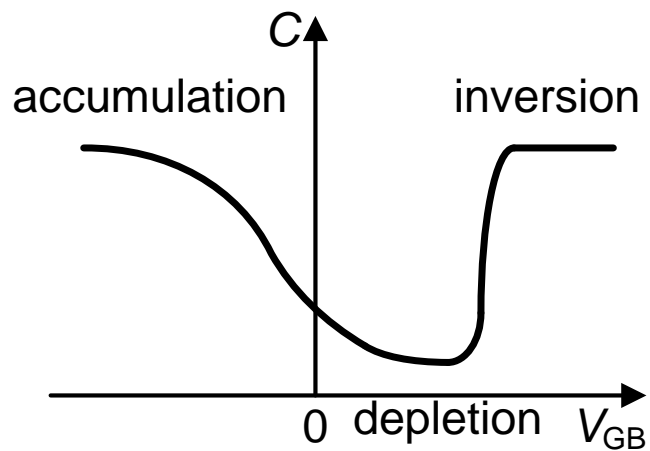
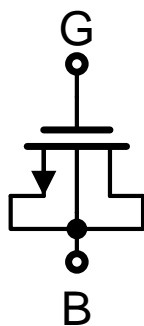
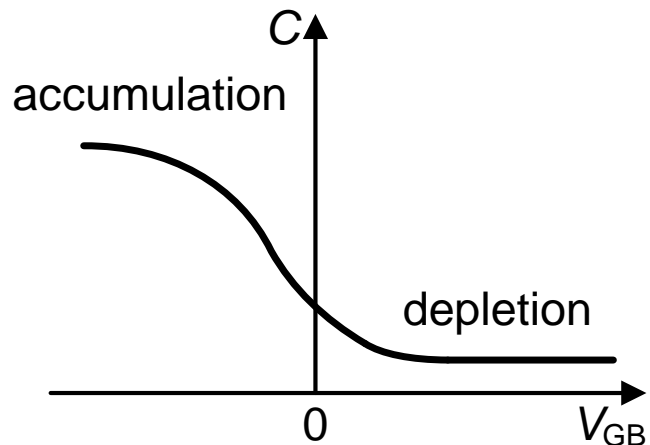
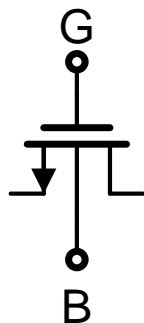
$$C_{gb} = \frac{C_j C_{ox}}{C_j + C_{ox}} + C_{gbo}$$

寄生电容与 V_{GS} 和 V_{DS} 的关系



Voltage dependence of C_{gs} and C_{gd} as a function of V_{GS} and V_{DS} .

NMOS管可变电容



NMOS varactor

模拟评价指标：固有增益

$$A_v = g_m r_{ds}$$

线性区：

$$A_v = \frac{V_{DS}}{V_{GS} - V_{TH,GS} - nV_{DS}}$$

饱和区：

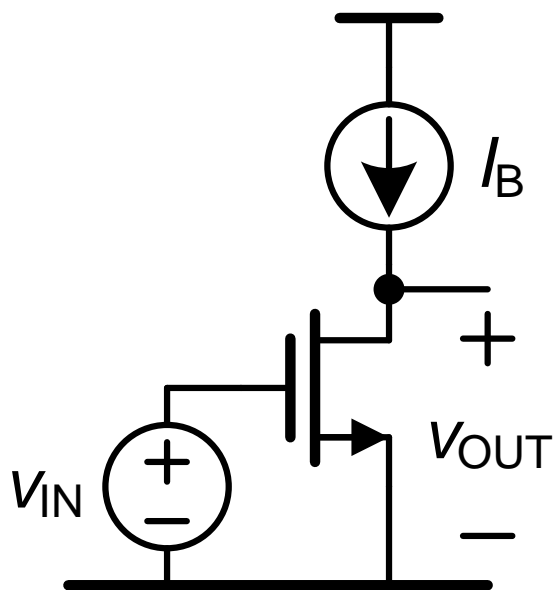
$$A_v = \frac{2I_D}{V_{GS} - V_{TH,GS}} \frac{V_E L}{I_D} = \frac{2V_E L}{(V_{GS} - V_{TH,GS})}$$

弱反型区：

$$A_v = \frac{I_D}{nV_T} \frac{V_T}{I_D} (e^{\frac{V_{DS}}{V_T}} - 1) = \frac{e^{\frac{V_{DS}}{V_T}} - 1}{n}$$

速度饱和区： $A_v \rightarrow \infty$!?

单MOS管增益 A_V



$$\begin{aligned}
 A_V &= g_m r_{ds} \\
 &= \frac{2I_D}{V_{GS} - V_{TH,GS}} \cdot \frac{V_E L}{I_D} \\
 &= \frac{2V_E L}{V_{GS} - V_{TH,GS}}
 \end{aligned}$$

如果 $V_{GS} - V_{TH,GS} = 0.2 \text{ V}$ 、 $V_E L \approx 10 \text{ V}$ ，则 $A_V \approx 100$ 。

高增益设计

	高增益	高速
$V_{GS} - V_{TH,GS}$	低(0.2 V)	
L	大	

$V_{GS} - V_{TH,GS}$ 决定 g_m/I_D 值，能效比!

例题7：单管放大器

用三个单管串联的结构，实现总增益为10,000的三级放大器。 $V_{GS} - V_{TH,GS} = 0.2 \text{ V}$ 。

使用先进的65 nm CMOS工艺($V_{En} = 4 \text{ V}/\mu\text{m}$)，求最小栅长。

模拟评价指标：跨导电流比 g_m/I_D

线性区：

$$\frac{g_m}{I_D} = \frac{1}{V_{GS} - V_{TH,GS} - \frac{n}{2} V_{DS}}$$

饱和区：

$$\frac{g_m}{I_D} = \frac{2}{V_{GS} - V_{TH,GS}}$$

弱反型区：

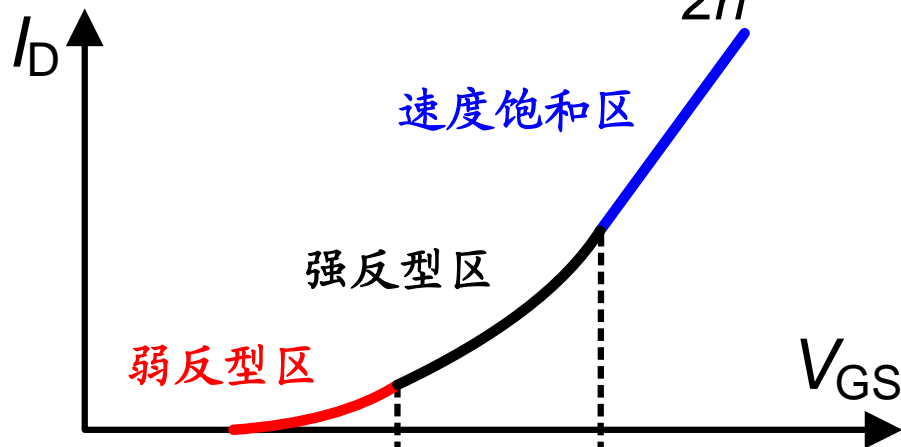
$$\frac{g_m}{I_D} = \frac{1}{nV_T}$$

速度饱和区：

$$\frac{g_m}{I_D} = \frac{1}{V_{GS} - V_{TH,GS}}$$

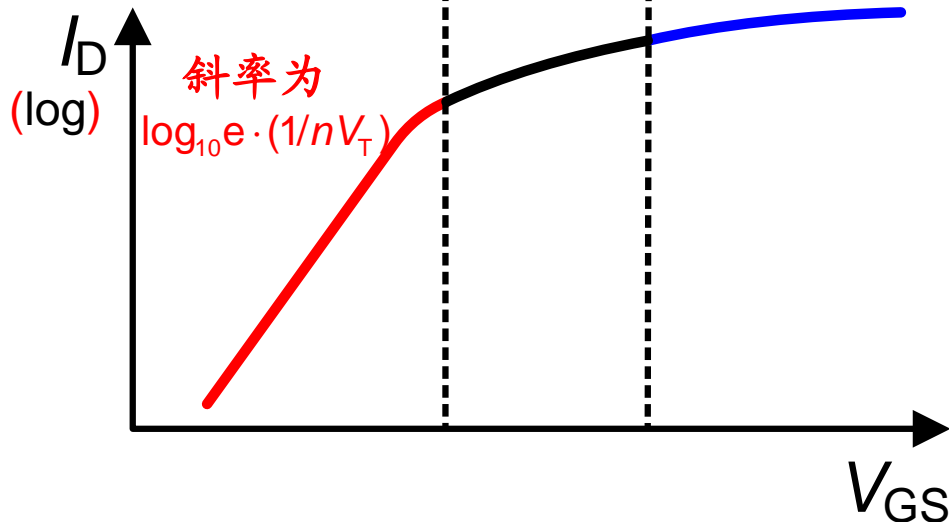
I_D 与 V_{GS} 的关系: 尺寸 W/L 固定

$$I_{D,si} = \frac{1}{2n} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH,GS})^2 [1 + \lambda(V_{DS} - V_{DSsat})]$$



$$I_{D,wi} = I_t \frac{W}{L} e^{\frac{V_{GS} - V_{TH,GS}}{nV_T}} \left(1 - e^{-\frac{V_{DS}}{V_T}}\right)$$

$$I_{D,vs} = C_{ox} W (V_{GS} - V_{TH,GS}) v_{scl}$$



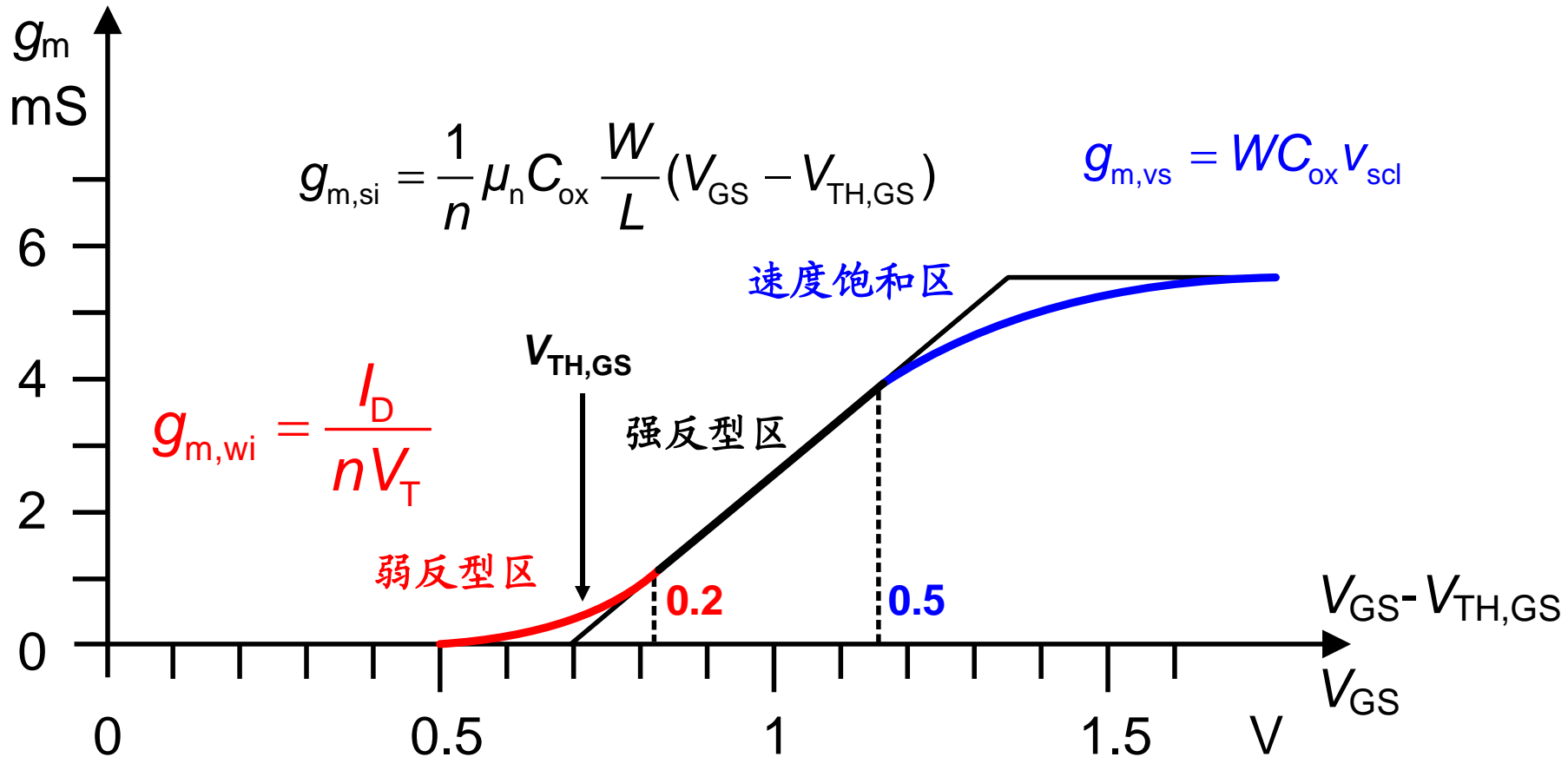
$$k = 1.38 \times 10^{-23} \text{ J/K}$$

$$q = 1.6 \times 10^{-19} \text{ C}$$

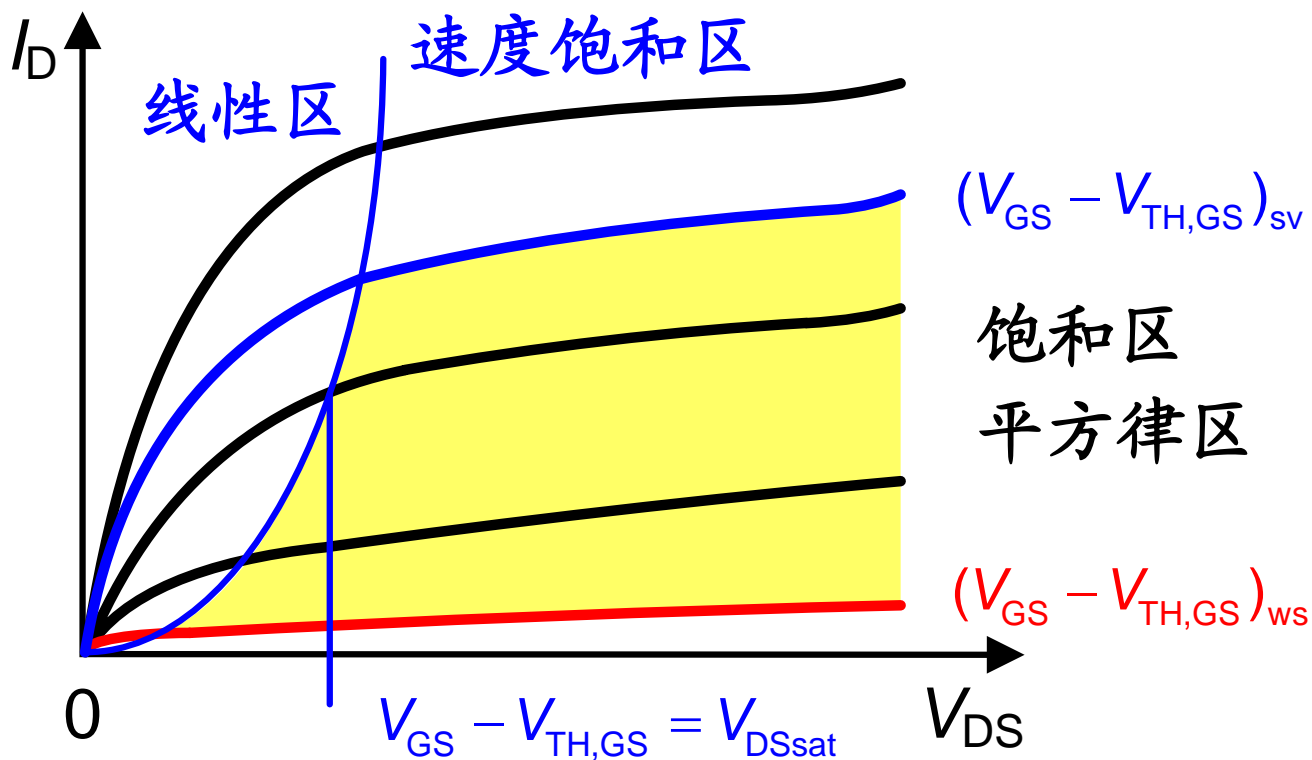
$$V_T = kT/q = 26 \text{ mV} @ T = 300 \text{ K}$$

$$v_{scl} \approx 10^7 \text{ cm/s}$$

跨导 g_m 与 V_{GS} 的关系：尺寸 W/L 固定



饱和区和速度饱和区



wi与si转换点电压 $V_{GST,ws}$

$$I_{D,wi} = I_t \frac{W}{L} e^{\frac{V_{GS} - V_{TH,GS}}{nV_T}} \left(1 - e^{-\frac{V_{DS}}{V_T}} \right)$$

$$g_{m,wi} = \frac{I_{D,wi}}{nV_T}$$

$$\frac{g_{m,wi}}{I_{D,wi}} = \frac{1}{nV_T}$$

$$I_{D,si} = \frac{1}{2n} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH,GS})^2$$

$$g_{m,si} = \frac{2I_{D,si}}{V_{GS} - V_{TH,GS}}$$

$$\frac{g_{m,si}}{I_{D,si}} = \frac{2}{V_{GS} - V_{TH,GS}}$$

$$(V_{GS} - V_{TH,GS})_{ws} = 2nV_T$$

转换点电压 $V_{\text{GST,ws}}$: 与 L 无关

$$(V_{\text{GS}} - V_{\text{TH,GS}})_{\text{ws}} = 2nV_{\text{T}}$$

$$I_{\text{Dws}} = \frac{1}{2n} \mu_{\text{n}} C_{\text{ox}} \frac{W}{L} (2nV_{\text{T}})^2$$

$$(V_{\text{GS}} - V_{\text{TH,GS}})_{\text{ws}} = 2nV_{\text{T}} \approx 70 \text{ mV}$$

$$\frac{1}{2n} \mu_{\text{n}} C_{\text{ox}} \approx 100 \mu\text{A/V}^2$$

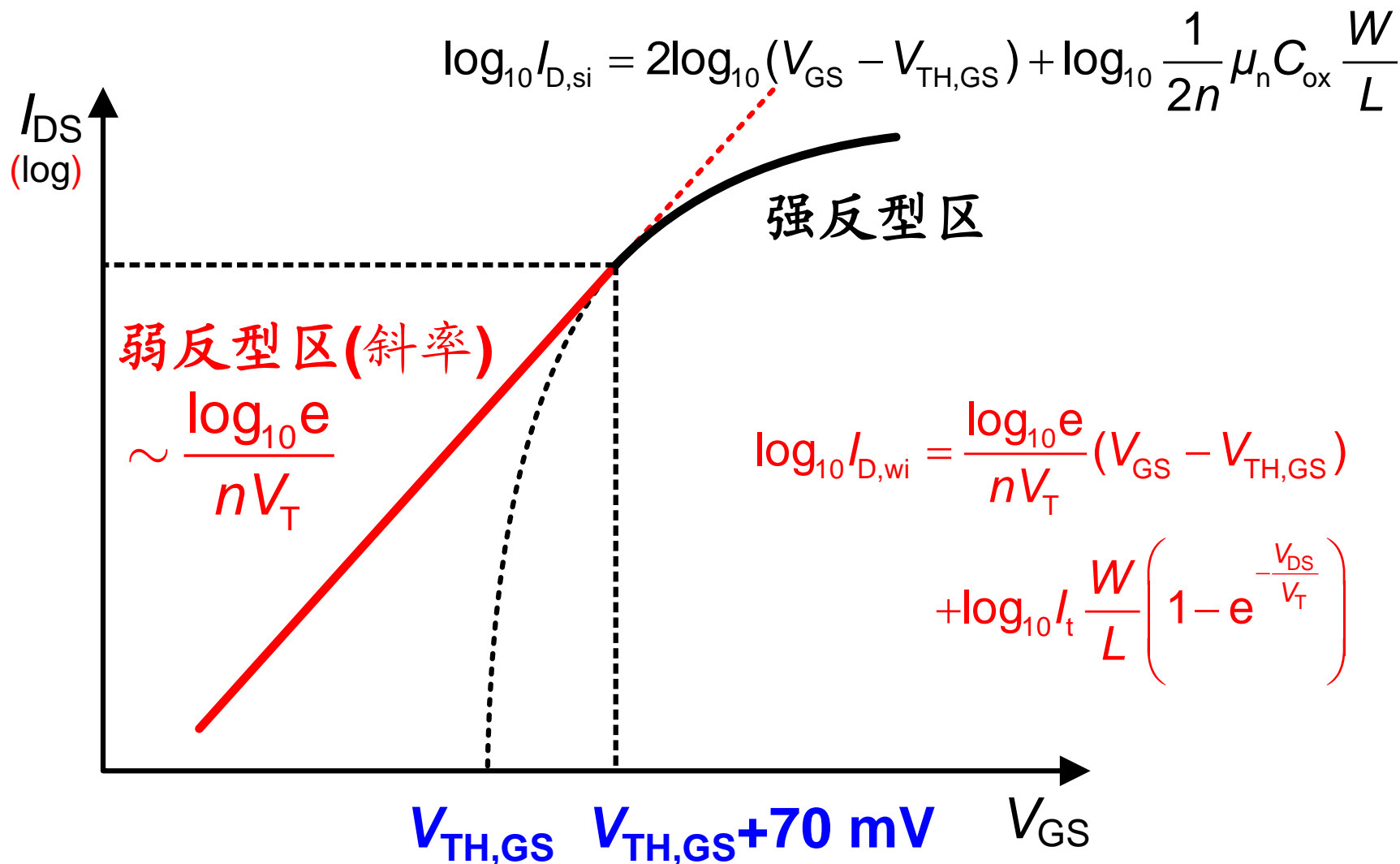
$$\frac{1}{2n} \mu_{\text{p}} C_{\text{ox}} \approx 40 \mu\text{A/V}^2$$

与沟道长度 L 无关，
很长时间内仍然遵循这一规律！

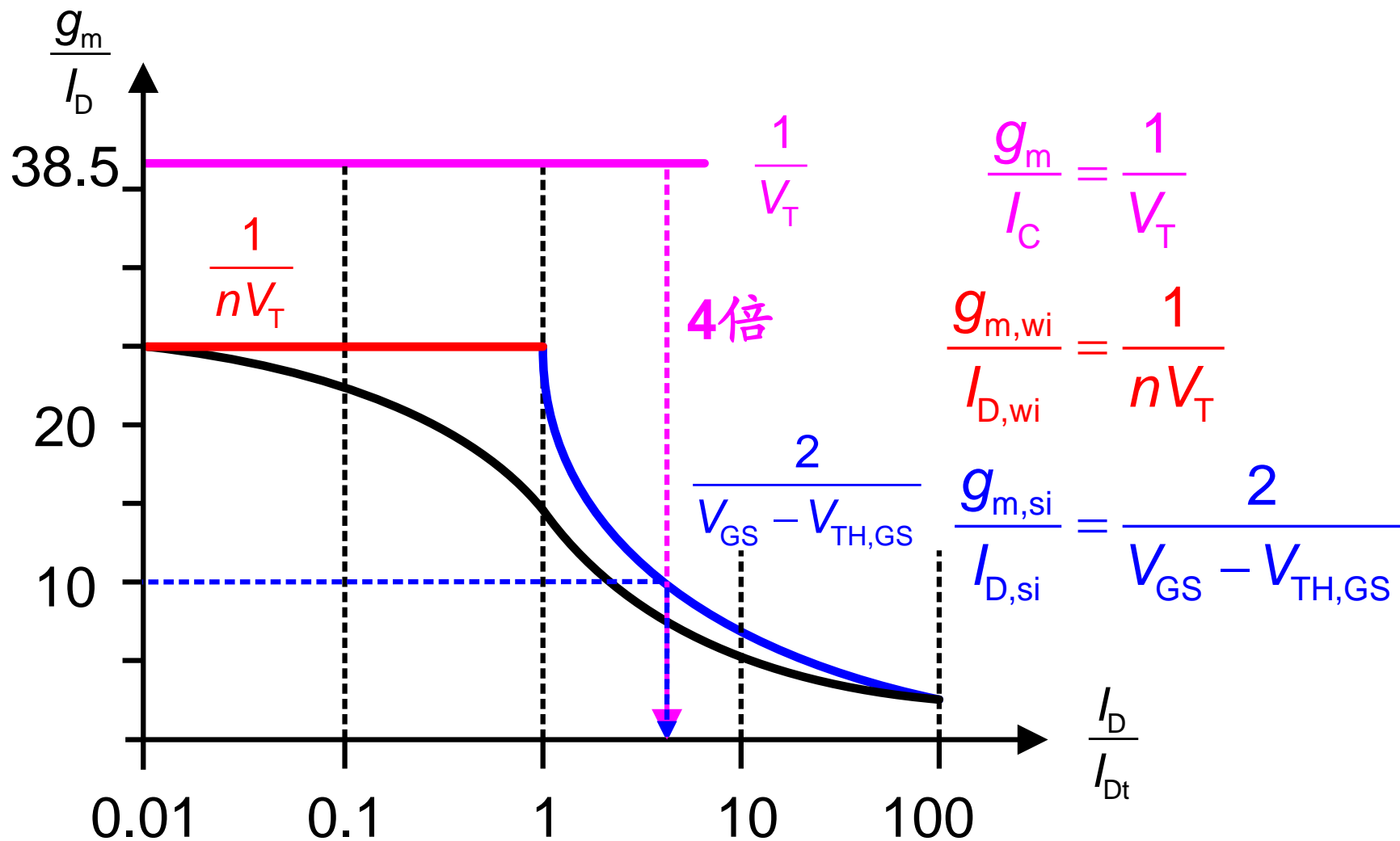
例如，当 $\frac{W}{L} = 10$ 时，NMOS 的 $I_{\text{D,ws}} \approx 5 \mu\text{A}$ ；

PMOS 的 $I_{\text{D,ws}} \approx 2 \mu\text{A}$ 。

wi与si的转换点



wi与si转换点的能效比 g_m/I_D



wi与si转换点电流 $I_{D,ws}$

$$I_{D,ws} = K' \frac{W}{L} V_{GST,ws}^2$$

$$i = \frac{I_D}{I_{D,ws}} = [\ln(1 + e^v)]^2 \quad \text{反型系数}$$

$$v = \ln(e^{\sqrt{i}} - 1)$$

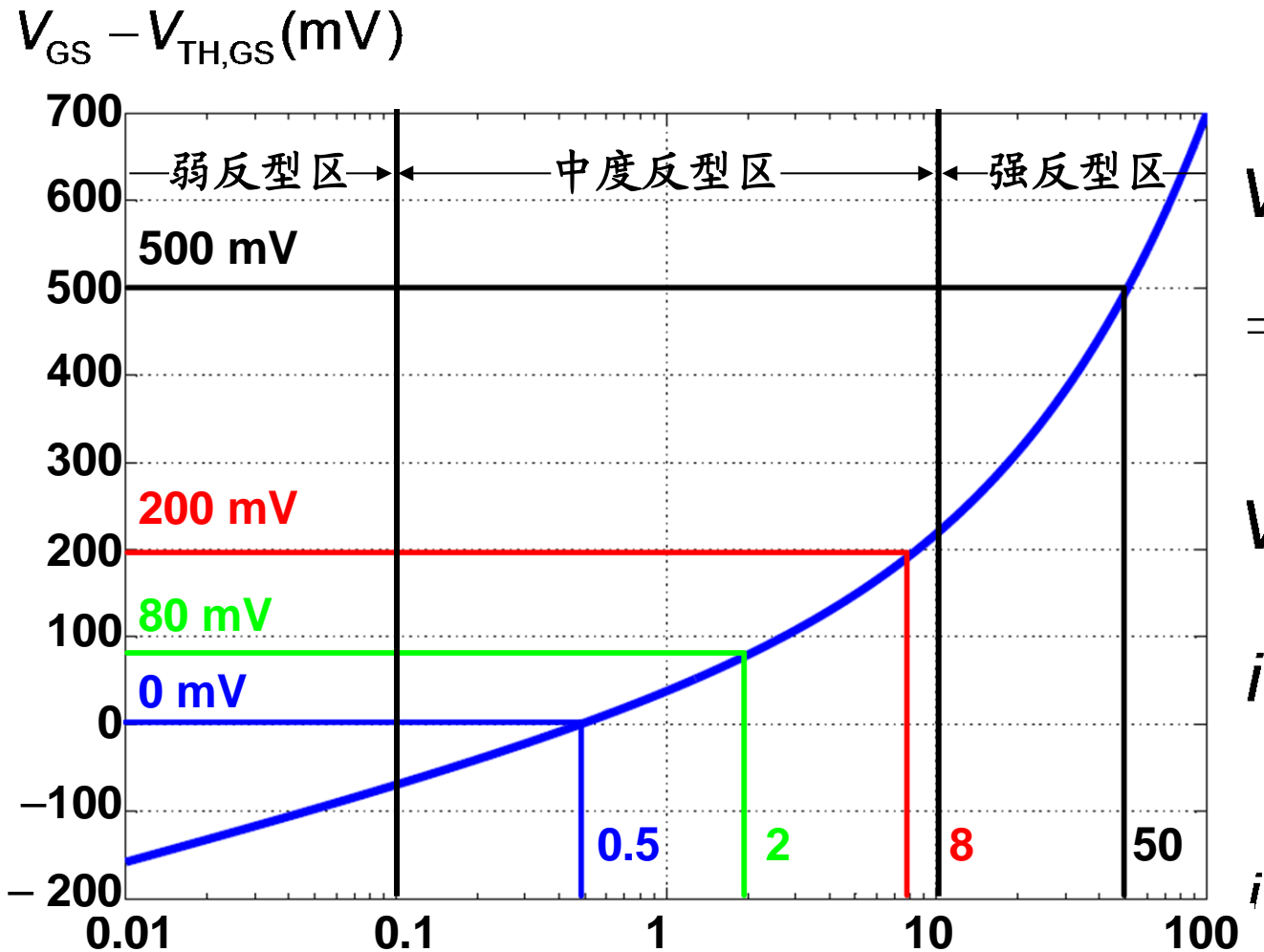
$$V_{GS} - V_{TH,GS} = V_{GST,ws} \ln(e^{\sqrt{i}} - 1) \quad V_{GST,ws} = 2nV_T \approx 70 \text{ mV}$$

$$i = 1 \quad v = \ln(e^{\sqrt{1}} - 1) = 0.54 \quad V_{GS} - V_{TH,GS} \approx 38 \text{ mV}$$

$$v = 1 \quad i = [\ln(1 + e^1)]^2 = 1.72$$

$$v = 0 \quad i = [\ln(1 + e^0)]^2 = 0.48$$

$V_{GS} - V_{TH,GS}$ 与反型系数 i 的关系



$$V_{GS} - V_{TH,GS} = V_{GST,ws} \ln(e^{\sqrt{i}} - 1)$$

$$V_{GST,ws} = 2nV_T$$

$$i = \frac{I_D}{I_{D,ws}}$$

wi与si之间的跨导 g_m ：归一化GM

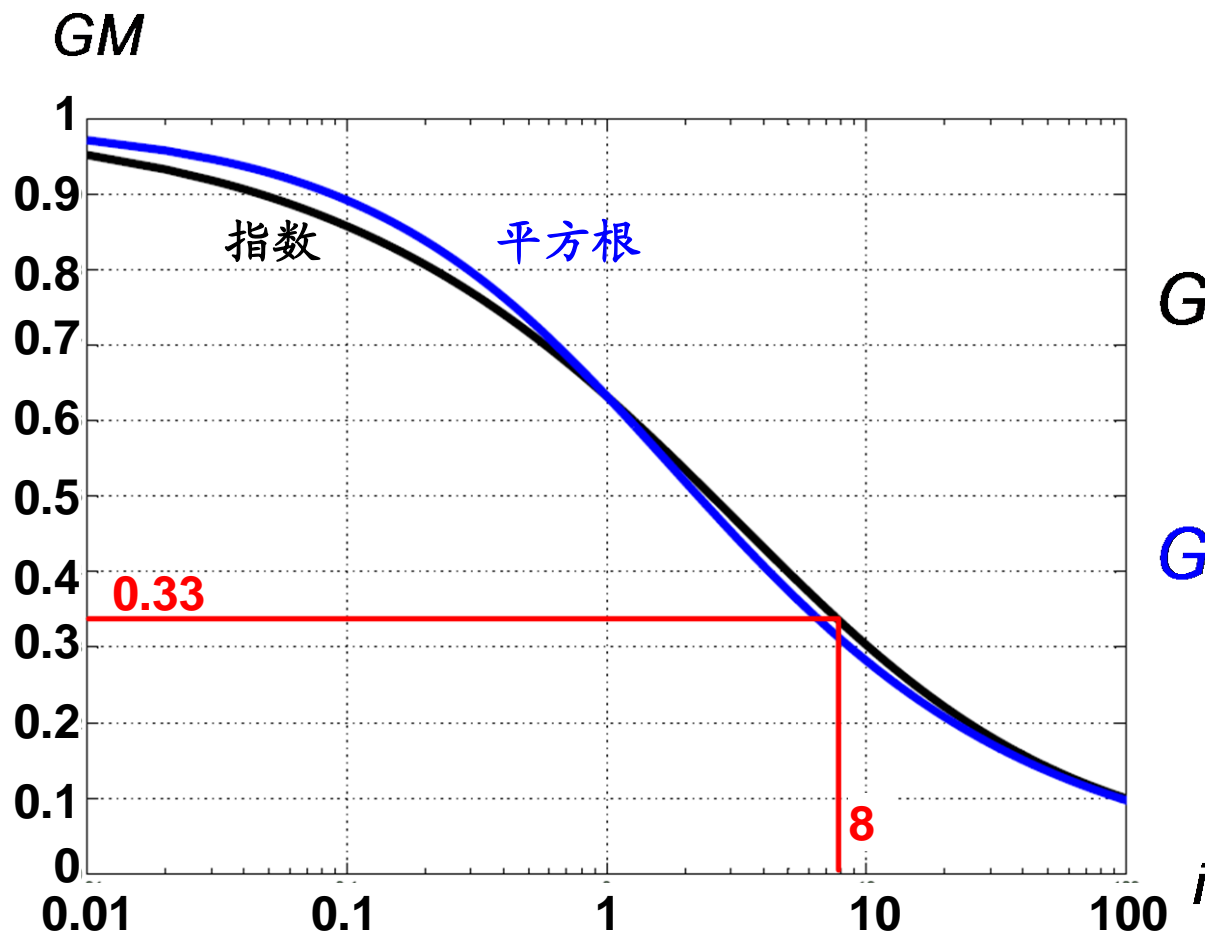
$$i = \frac{I_D}{I_{D,ws}} = [\ln(1 + e^v)]^2 \quad g_m \approx \dots$$

$$GM = \frac{\frac{g_m}{I_D}}{\frac{1}{nV_T}} = \frac{g_m}{I_{DS}} nV_T$$

$$(1) GM = \frac{1 - e^{-\sqrt{i}}}{\sqrt{i}} \quad \text{大 } i : GM = \frac{1}{\sqrt{i}} \quad \text{小 } i : GM = 1 - \frac{\sqrt{i}}{2}$$

$$(2) GM = \frac{1}{\sqrt{1 + 0.5\sqrt{i} + i}} \quad \text{大 } i : GM = \frac{1}{\sqrt{i}} \quad \text{小 } i : GM = 1 - \frac{\sqrt{i}}{4}$$

归一化跨导 GM 与反型系数 i 的关系



$$GM = \frac{g_m}{I_D} nV_T$$

$$GM = \frac{1 - e^{-\sqrt{i}}}{\sqrt{i}}$$

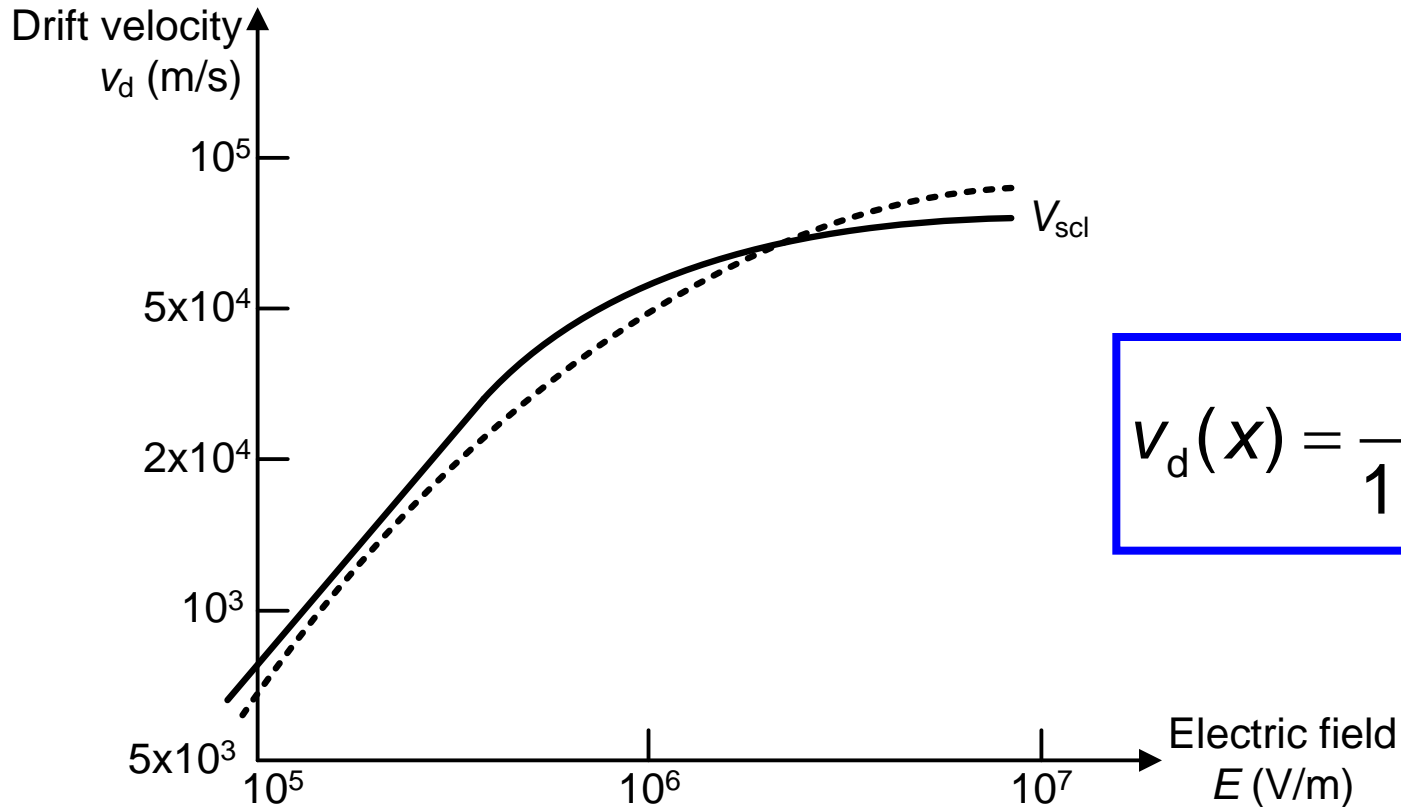
(指数)

$$GM = \frac{1}{\sqrt{1 + 0.5\sqrt{i} + i}}$$

(平方根)

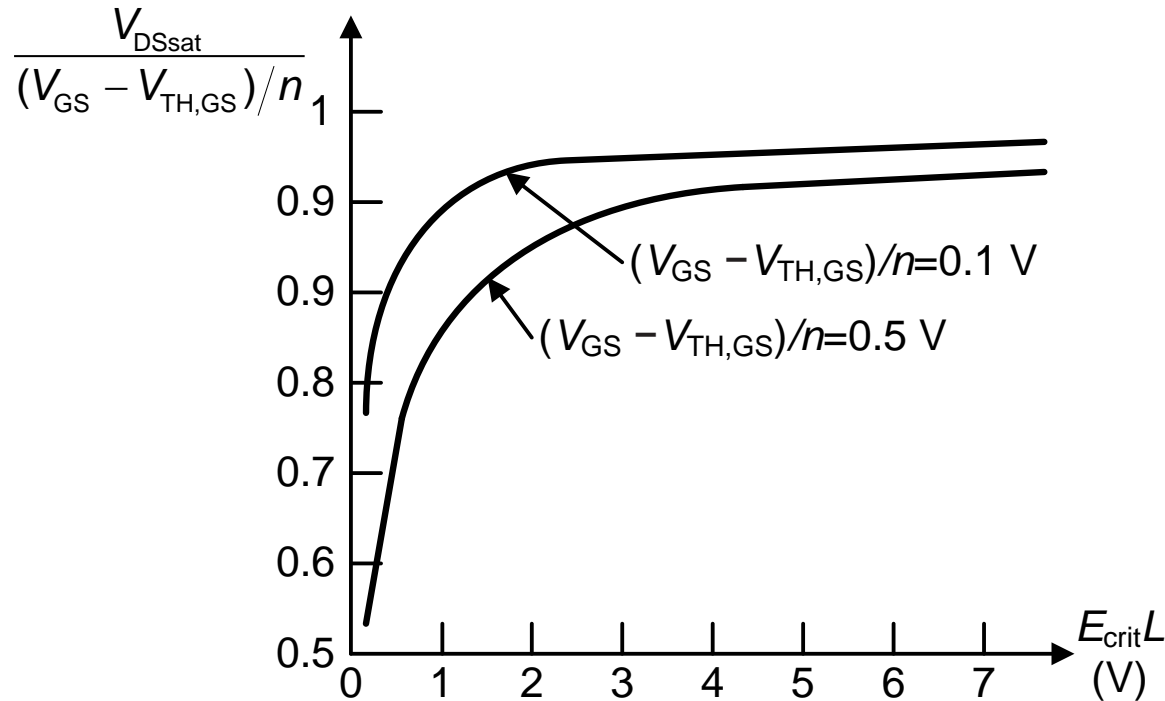
$$i = \frac{I_D}{I_{D,ws}}$$

电子漂移速度与横向电场的关系



Typical measured electron drift velocity v_d versus horizontal electric field E in an MOS surface channel (solid plot). Also shown (dashed plot) is the analytical approximation with $E_{\text{crit}} = 1.5 \times 10^6$ V/m and $\mu_n = 0.07$ m²/Vs.

漏源饱和电压 V_{DSsat}



Ratio of the minimum drain-source voltage required for operation in the active region to the overdrive versus the product of the critical field and the channel length. When $E_{crit} \rightarrow \infty$, velocity saturation is not a factor, and $V_{DSsat} \rightarrow (V_{GS} - V_{TH,GS})/n$, as expected. When velocity saturation is significant, $V_{DSsat} < (V_{GS} - V_{TH,GS})/n$.

I-V关系式：(1)

单位面积的电荷密度： $Q_n(x) = C_{ox} \{V_{GS} - V_{TH,GS} - nV_{CS}(x)\}$

$$I_D = WQ_n(x)v_d(x) \quad v_d(x) = \frac{\mu_n E(x)}{1 + E(x)/E_{crit}} \quad E(x) = -\frac{dV_{CS}(x)}{dx}$$

$$I_D \left(1 + \frac{1}{E_{crit}} \frac{dV_{CS}(x)}{dx} \right) = W\mu_n C_{ox} \{V_{GS} - V_{TH,GS} - nV_{CS}(x)\} \frac{dV_{CS}(x)}{dx}$$

$$\int_0^L I_D \left(1 + \frac{1}{E_{crit}} \frac{dV_{CS}(x)}{dx} \right) dx = \int_0^{V_{DS}} W\mu_n C_{ox} \{V_{GS} - V_{TH,GS} - nV_{CS}(x)\} dV_{CS}(x)$$

$$I_D = \frac{\mu_n C_{ox}}{1 + \frac{V_{DS}}{E_{crit} L}} \frac{W}{L} \left[(V_{GS} - V_{TH,GS}) V_{DS} - \frac{nV_{DS}^2}{2} \right]$$

饱和条件(1)

饱和条件:

$$\frac{\partial I_D}{\partial V_{DS}} = \mu_n C_{ox} \left[\frac{\left(1 + \frac{V_{DS}}{E_{crit} L}\right) (V_{GS} - V_{TH,GS} - \frac{nV_{DS}}{2}) - \frac{(V_{GS} - V_{TH,GS})V_{DS} - \frac{nV_{DS}^2}{2}}{E_{crit} L}}{\left(1 + \frac{V_{DS}}{E_{crit} L}\right)^2} \right] = 0$$

$$\frac{nV_{DS}^2}{E_{crit} L} + 2nV_{DS} - 2(V_{GS} - V_{TH,GS}) = 0$$

$$V_{DSsat} = E_{crit} L \left(\sqrt{1 + \frac{2(V_{GS} - V_{TH,GS})}{nE_{crit} L}} - 1 \right)$$

饱和条件(2)

$$x = \frac{V_{GS} - V_{TH,GS}}{nE_{crit}L} \quad \sqrt{1+2x} = 1 + x - \frac{x^2}{2} + \dots$$

$$V_{DSsat} = \frac{V_{GS} - V_{TH,GS}}{n} \left(1 - \frac{V_{GS} - V_{TH,GS}}{2nE_{crit}L} + \dots \right)$$

$$\frac{2(V_{GS} - V_{TH,GS})}{n} = E_{crit}L \left[\left(\frac{V_{DSsat}}{E_{crit}L} + 1 \right)^2 - 1 \right]$$

$$I_D = \frac{\mu_n C_{ox}}{2n} \frac{W}{L} (nV_{DSsat})^2$$

I-V关系式(2)

$$\begin{aligned}
 I_D &= \frac{\mu_n C_{ox}}{2n} \frac{W}{L} (V_{GS} - V_{TH,GS})^2 \left(1 - \frac{V_{GS} - V_{TH,GS}}{2nE_{crit}L} + \dots \right)^2 \\
 &= \frac{\mu_n C_{ox}}{2n} \frac{W}{L} (V_{GS} - V_{TH,GS})^2 \left(1 - \frac{V_{GS} - V_{TH,GS}}{nE_{crit}L} + \dots \right)
 \end{aligned}$$

$$I_D \approx \frac{\mu_n C_{ox}}{2n \left(1 + \frac{V_{GS} - V_{TH,GS}}{nE_{crit}L} \right)} \frac{W}{L} (V_{GS} - V_{TH,GS})^2$$

速度饱和区: R_{SX}

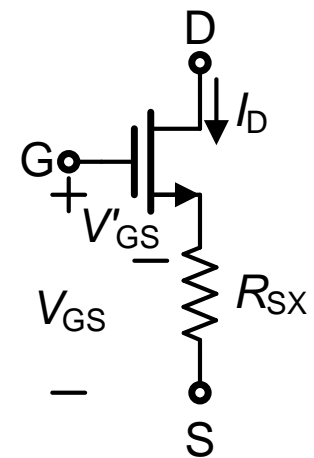
$$I_D = \frac{1}{2n} \mu_n C_{ox} \frac{W}{L} (V'_{GS} - V_{TH,GS})^2 \quad V_{GS} = V'_{GS} + I_D R_{SX}$$

$$I_D = \frac{1}{2n} \mu_n C_{ox} \frac{W}{L} [(V_{GS} - V_{TH,GS})^2 - 2(V_{GS} - V_{TH,GS}) I_D R_{SX} + (I_D R_{SX})^2]$$

$$= \frac{\mu_n C_{ox}}{2n \left[1 + \mu_n C_{ox} \frac{W}{L} R_{SX} (V_{GS} - V_{TH,GS}) \right]} \frac{W}{L} (V_{GS} - V_{TH,GS})^2$$

$$\mu_n C_{ox} \frac{W}{L} R_{SX} = \frac{1}{n E_{crit} L}$$

$$R_{SX} = \frac{1}{n \mu_n C_{ox} W E_{crit}}$$



si与vs转换点电压 $V_{GST,sv}$

$$I_{D,si} = \frac{\mu_n C_{ox}}{2n} \frac{W}{L} (V_{GS} - V_{TH,GS})^2$$

$$I_{D,vs} = WC_{ox} v_{scl} (V_{GS} - V_{TH,GS})$$

$$g_{m,si} = 2 \frac{\mu_n C_{ox}}{2n} \frac{W}{L} (V_{GS} - V_{TH,GS})$$

$$g_{m,vs} = WC_{ox} v_{scl}$$

$$I_{D,si} = I_{D,vs} \quad \text{or} \quad \frac{g_{m,si}}{I_{D,si}} = \frac{g_{m,vs}}{I_{D,vs}}$$

$$(V_{GS} - V_{TH,GS})_{sv} = 2nL \frac{v_{scl}}{\mu_n} \approx 5L$$

$$I_{D,sv} = \frac{2nWLC_{ox} v_{scl}^2}{\mu_n}$$

$$v_{scl} = 10^7 \text{ cm/s}$$

$$n = 1.4$$

当 $L = 0.13 \mu\text{m}$ 时, $(V_{GS} - V_{TH,GS})_{sv} \approx 0.65 \text{ V}$ $\mu_n = 500 \text{ cm}^2/\text{Vs}$

si与vs转换点电流 $I_{D,sv}$

$$I_{D,sv} \approx \frac{\mu_n C_{ox}}{2n} \frac{W}{L} \left(2nL \frac{V_{scl}}{\mu_n}\right)^2 \approx 100n\epsilon_{ox} W \frac{V_{scl}^2}{\mu_n}$$

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}} \quad t_{ox} = \frac{L_{min}}{50}$$

$$\frac{I_{D,sv}}{W} \approx 10 \text{ A/cm}$$

$$\epsilon_{ox} = 0.34 \text{ pF/cm}$$

$$V_{sat} = 10^7 \text{ cm/s}$$

$$n = 1.4$$

$$\mu_n = 500 \text{ cm}^2/\text{Vs}$$

当 $W = 1 \mu\text{m}$, $L_{min} = 0.13 \mu\text{m}$ 时, $I_{D,sv} \approx 1 \text{ mA}$ 。

si与vs转换点电压 $V_{GST,sv}$

$$I_{D,si} = \frac{\mu_n C_{ox} W}{2n L} (V_{GS} - V_{TH,GS})^2 \quad I_{D,vs} = WC_{ox} v_{scl} (V_{GS} - V_{TH,GS})$$

$$g_{m,si} = 2 \frac{\mu_n C_{ox} W}{2n L} (V_{GS} - V_{TH,GS}) \quad g_{m,vs} = WC_{ox} v_{scl}$$

$$g_{m,si} = g_{m,vs}$$

$$(V_{GS} - V_{TH,GS})_{sv} = nL \frac{v_{scl}}{\mu_n} \approx 2.5L$$

$$I_{D,sv} = \frac{nWLC_{ox} v_{scl}^2}{2\mu_n}$$

$$v_{scl} = 10^7 \text{ cm/s}$$

$$n = 1.4$$

正比于沟道长度L!!!

当 $L = 0.13 \mu\text{m}$ 时, $(V_{GS} - V_{TH,GS})_{sv} \approx 0.325 \text{ V}$ $\mu_n = 500 \text{ cm}^2/\text{Vs}$

si与vs转换点跨导 g_m

$$g_{m,vs} = WC_{ox} v_{scl} = 50\epsilon_{ox} v_{scl} \frac{W}{L_{min}} = 17 \times 10^{-5} W/L_{min} \text{ (S)}|_{cm}$$

$$g_{m,si} = 2K'_n \frac{W}{L_{min}} (V_{GS} - V_{TH,GS})$$

$$= \frac{50\mu_n \epsilon_{ox}}{n} \frac{W}{L_{min}^2} V_{GST} = 6 \times 10^{-9} V_{GST} W/L_{min}^2 \text{ (S)}|_{cm}$$

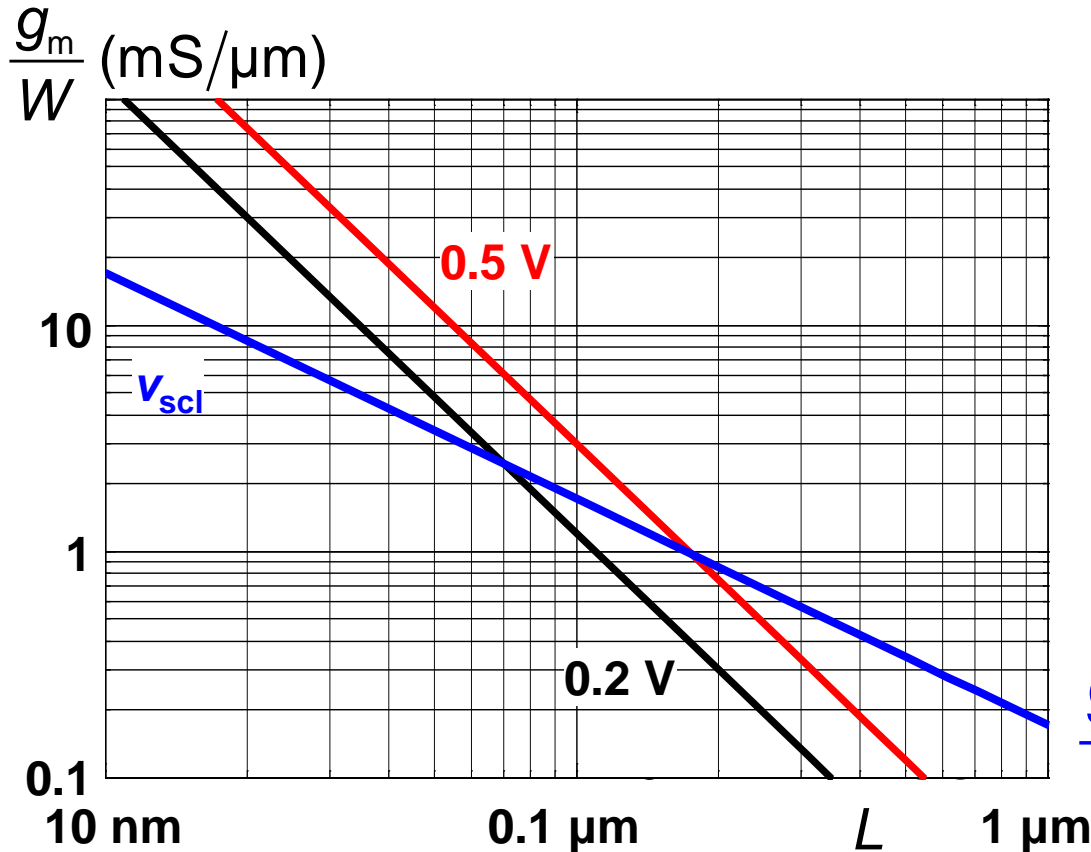
$$\frac{1}{g_m} = \frac{1}{g_{m,vs}} + \frac{1}{g_{m,si}}$$

$$g_m \approx \frac{W}{L_{min}} \frac{17 \times 10^{-5}}{1 + 2.8 \times 10^4 L_{min} / V_{GST}}$$

L_{min} 的单位为cm

$$g_{m,vs} = g_{m,si} \quad L_{min} = \frac{\mu_n V_{GST,sv}}{n v_{scl}} = 0.4 V_{GST,sv} (\mu m)$$

速度饱和区? 饱和区?



$$V_{GS} - V_{TH,GS} \approx 0.2 \text{ V}$$

$$\frac{g_{m,si}}{W} = \frac{2K'_n (0.5 \text{ V})}{L_{min}} (V_{GS} - V_{TH,GS})$$

$$\frac{g_{m,si}}{W} \approx \frac{0.06 V_{GST}}{L_{min}^2}$$

L 的单位为 μm

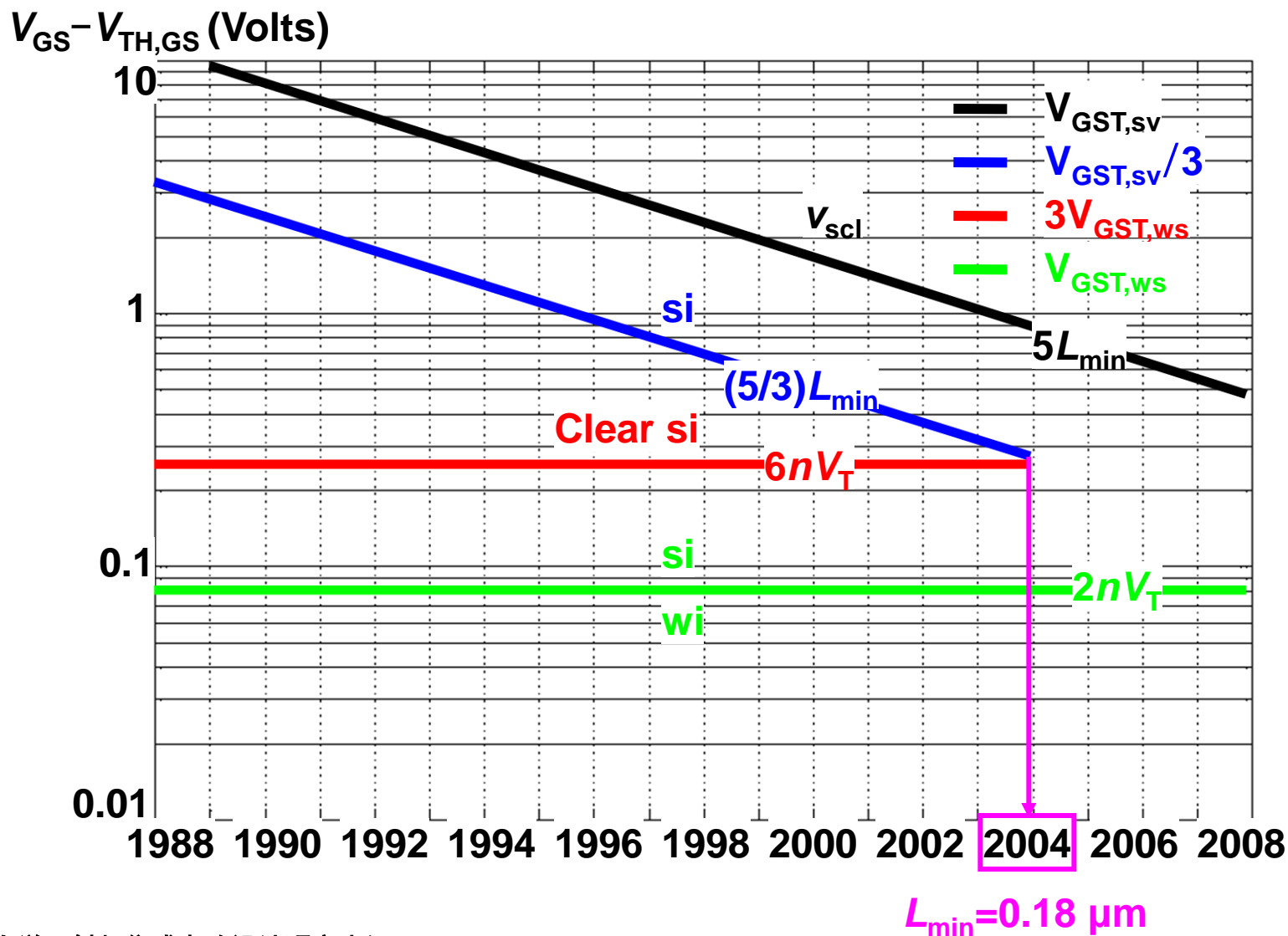
$$\frac{g_{m,vs}}{W} = C_{ox} V_{scl}$$

$$\frac{g_{m,vs}}{W} \approx \frac{0.17}{L_{min}} \quad L \text{ 的单位为 } \mu\text{m}$$

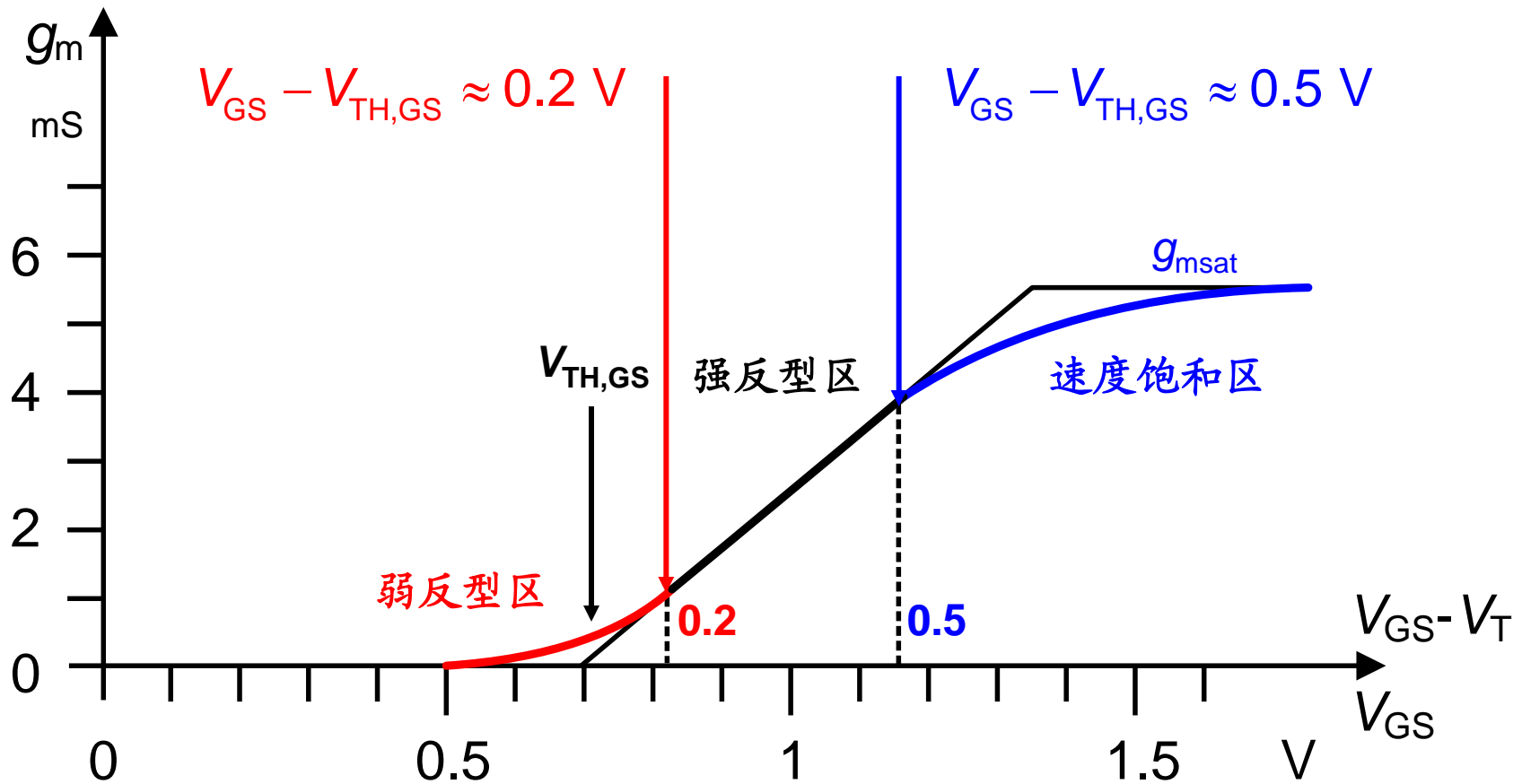
当 $V_{GST,sv} = 0.2 \text{ V}$, $L_{min} < 65 \text{ nm}$;

或 $V_{GST,sv} = 0.5 \text{ V}$, $L_{min} < 0.18 \mu\text{m}$ 时, 晶体管进入速度饱和区

平方率饱和区 V_{GST} 的有效范围

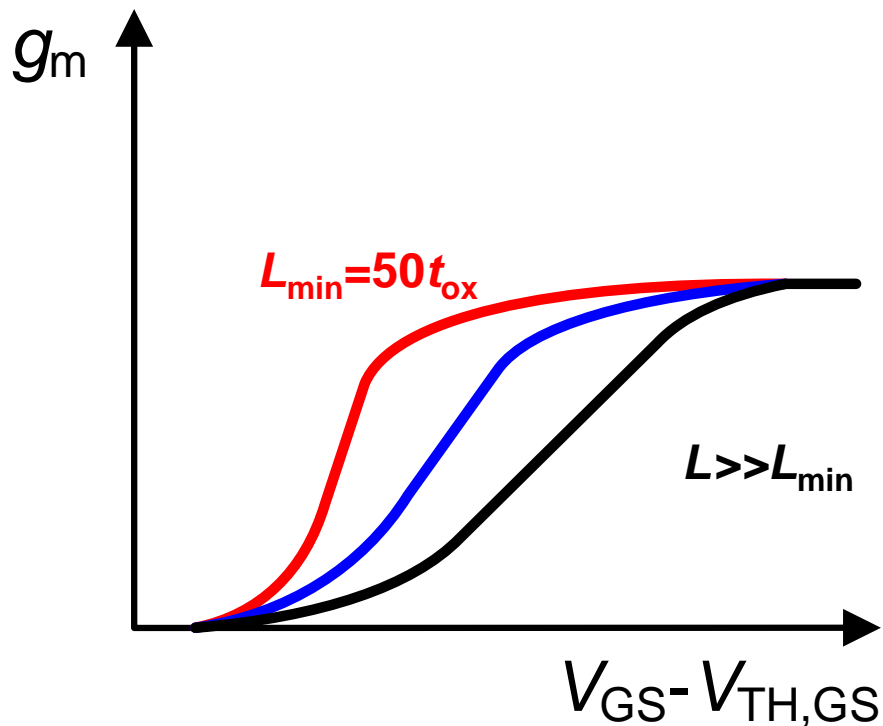


在饱和区MOST的工作范围

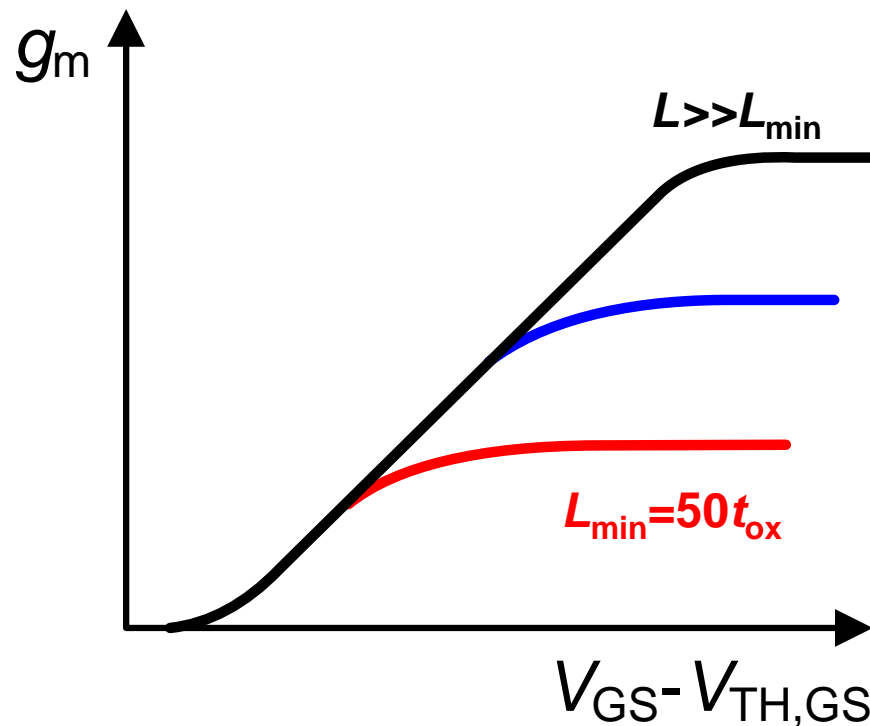


练习2: 相同工艺下，不同L值

相同 t_{ox} 值!



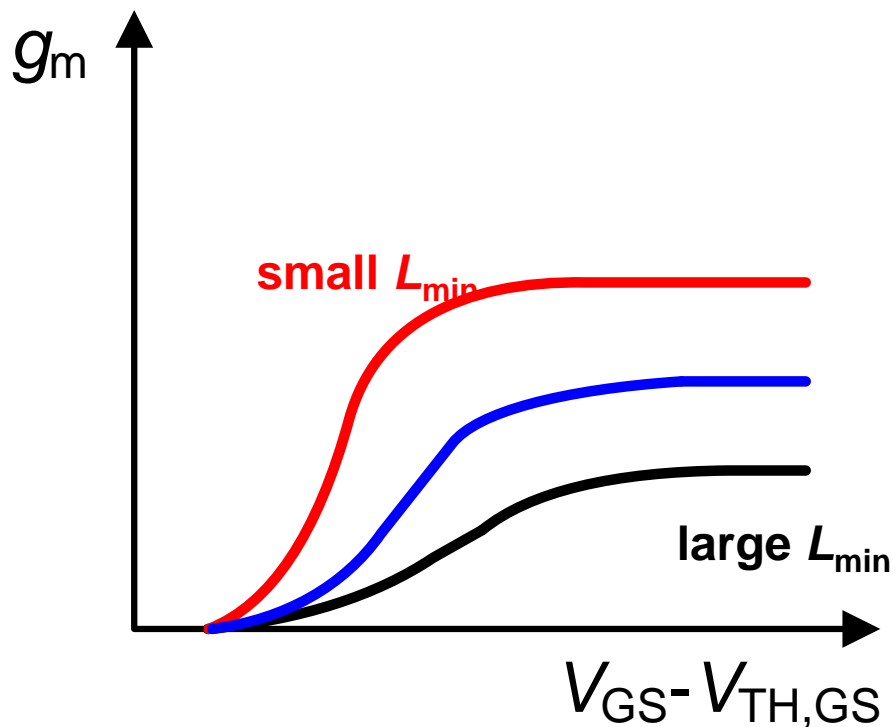
$$W = ct$$



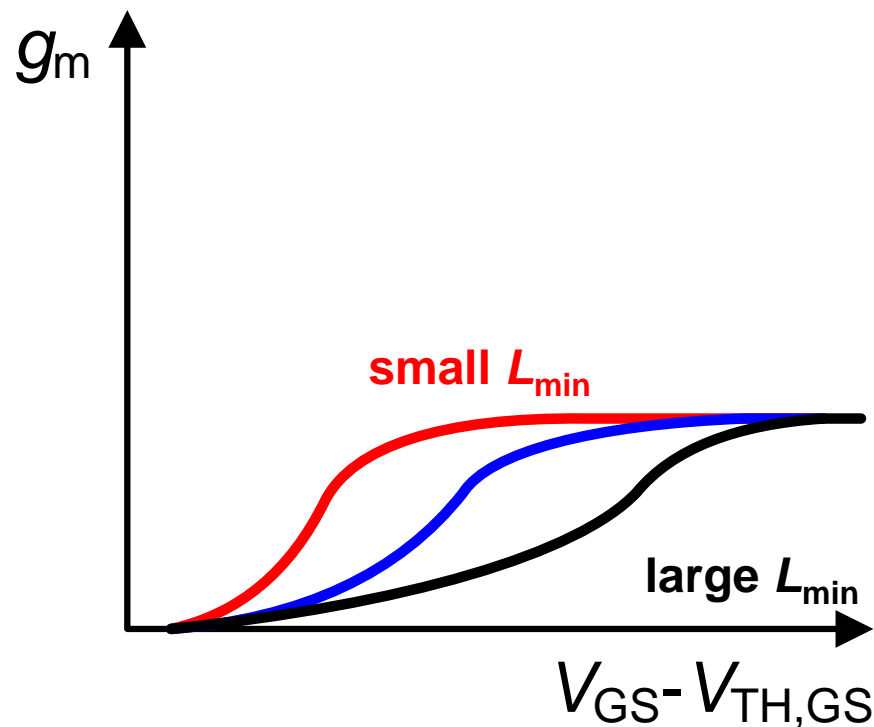
$$\frac{W}{L} = ct$$

练习2: 不同工艺下, L_{\min} 值,

不同 t_{ox} 值!



$$W = ct$$



$$\frac{W}{L} = ct$$

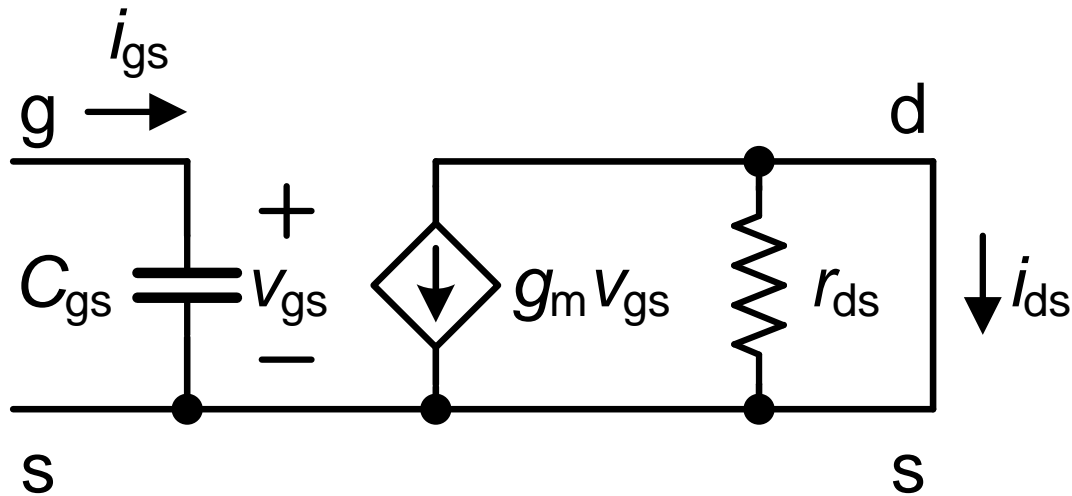
MOST的 I_D 、 g_m 和 g_m/I_D

摘要：关于 I_D 、 g_m 和 g_m/I_D 的公式

	I_D	g_m	$\frac{g_m}{I_D} = f(V_{GS} - V_{TH,GS})$	$\frac{g_m}{I_D} = f(I_D)$
Wi	$I_t \frac{W}{L} e^{\frac{V_{GS}-V_{TH,GS}}{nV_T}}$ (1-25a)	$\frac{I_t}{nV_T} \frac{W}{L} e^{\frac{V_{GS}-V_{TH,GS}}{nV_T}}$ (1-25b)	$\frac{1}{nV_T}$ (1-26b)	$\frac{1}{nV_T}$ (1-26b)
WS			$(V_{GS} - V_{TH,GS})_{ws} = 2nV_T$	$I_{D,ws} = \frac{KP}{2n} \frac{W}{L} (2nV_T)^2$
Si	$\frac{KP}{2n} \frac{W}{L} (V_{GS} - V_{TH,GS})^2$ (1-18c)	$2 \frac{KP}{2n} \frac{W}{L} (V_{GS} - V_{TH,GS})$ (1-22a)	$\frac{2}{V_{GS} - V_{TH,GS}}$ (1-26a)	$2 \sqrt{\frac{KP}{2n} \frac{W}{L} \frac{1}{I_{DS}}}$ (1-26a)
SV	$I_{D,si} = I_{D,vs}$	$\frac{g_{m,si}}{I_{D,si}} = \frac{g_{m,vs}}{I_{D,vs}}$	$(V_{GS} - V_{TH,GS})_{sv} = \frac{2nLC_{ox} v_{scl}}{KP}$	$I_{D,sv} = \frac{2nWLC_{ox}^2 v_{scl}^2}{KP}$
		$g_{msi} = g_{mvs}$	$(V_{GS} - V_{TH,GS})_{sv} = \frac{nLC_{ox} v_{scl}}{2KP}$	$I_{D,sv} = \frac{nWLC_{ox}^2 v_{scl}^2}{2KP}$
			$(V_{GS} - V_{TH,GS})_{sv} = \frac{2nLC_{ox} v_{scl}}{2KP}$	$I_{D,sv} = \frac{2nWLC_{ox}^2 v_{scl}^2}{2KP}$
VS	$WC_{ox} v_{sat} (V_{GS} - V_{TH,GS})$ (1-38b)	$WC_{ox} v_{scl}$ (1-39)	$\frac{1}{V_{GS} - V_{TH,GS}}$	$\frac{WC_{ox} v_{scl}}{I_{D,vs}}$

Ref.: Laker, Sansen : Design of analog ..., MacGrawHill 1994; Table 1-4

当 $i_{ds} = i_{gs}$ 时, MOST的特征频率 f_T



$$\begin{cases} i_{gs} = V_{gs} C_{gs} s \\ i_{ds} = g_m V_{gs} \end{cases}$$

$$C_{gs} = \frac{2}{3} W L C_{ox} \quad g_m = 2K' \frac{W}{L} (V_{GS} - V_{TH,GS}) \quad K' = \frac{\mu C_{ox}}{2n}$$

$$f_T = \frac{g_m}{2\pi C_{gs}} = \frac{1}{2\pi} \frac{3}{2n} \frac{\mu}{L^2} (V_{GS} - V_{TH,GS})$$

$$\frac{1}{2\pi \cdot L/v_{scl}} = \frac{v_{scl}}{2\pi L} \times \frac{3}{2} ?$$

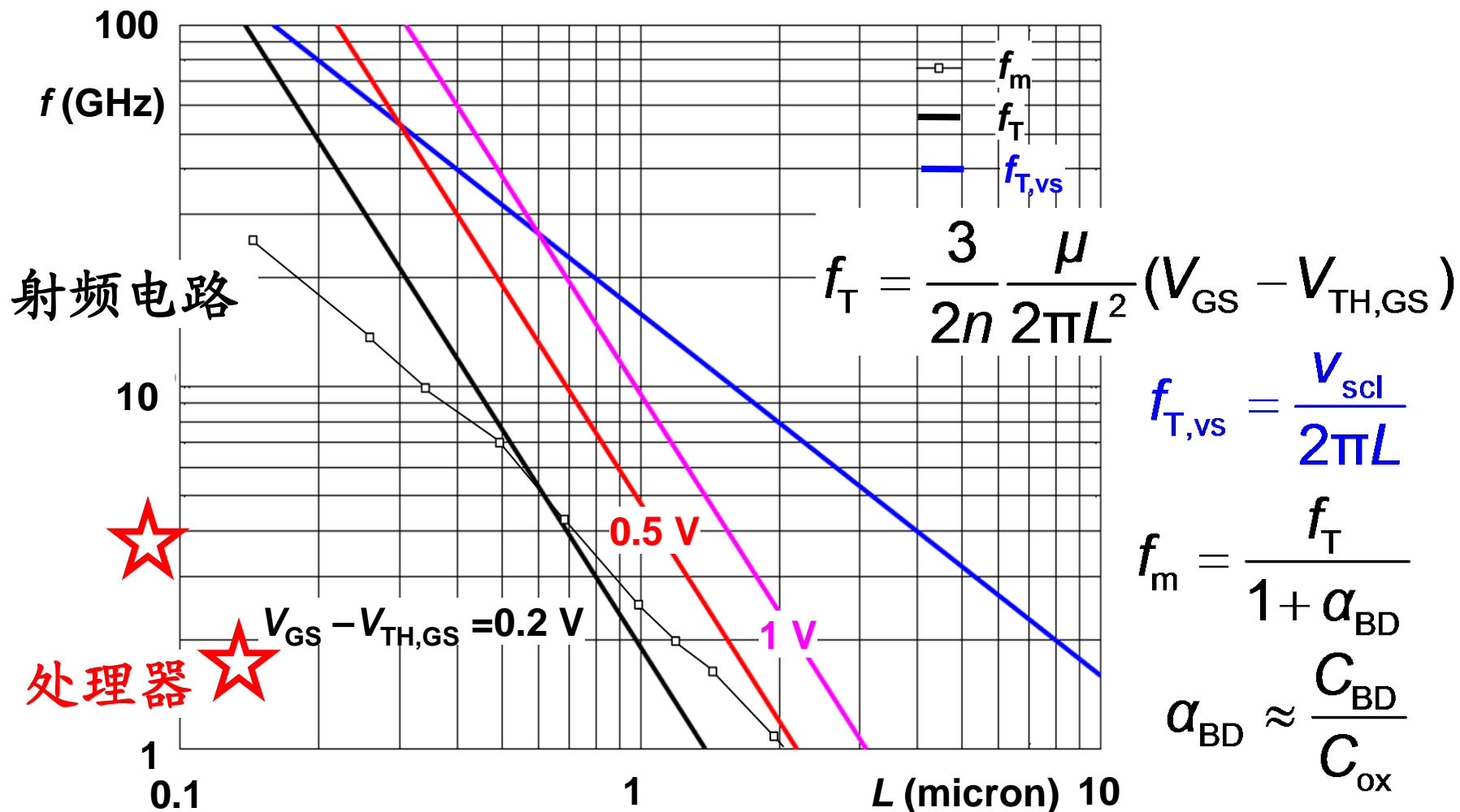
$$g_m = W C_{ox} v_{scl}$$

高速设计

	高增益	高速
$V_{GS} - V_{TH,GS}$	低(0.2 V)	高(0.5 V)
L	大	小

$V_{GS} - V_{TH,GS}$ 决定 g_m/I_D 值，能效比!

最大特征频率 f_T 与沟道长度 L 的关系



饱和区和速度饱和区的特征频率 f_T

$$f_T = \frac{g_m}{2\pi C_{gs}} \quad C_{gs} = kW \quad k = 2 \text{ fF}/\mu\text{m} = 2 \times 10^{-11} \text{ F/cm}$$

$$g_m = \frac{W}{L_{\min}} \frac{17 \times 10^{-5}}{1 + 2.8 \times 10^4 L_{\min} / V_{\text{GST}}} \quad L \text{ 的单位为 cm}$$

$$f_T = \frac{1}{L_{\min}} \frac{13.5}{1 + 2.8 L_{\min} / V_{\text{GST}}} \text{ GHz}$$

L 的单位为 μm

当 $V_{\text{GST}} = 0.2 \text{ V}$, $L_{\min} < 65 \text{ nm}$;

或 $V_{\text{GST}} = 0.5 \text{ V}$, $L_{\min} < 0.18 \mu\text{m}$ 时, 晶体管进入速度饱和区

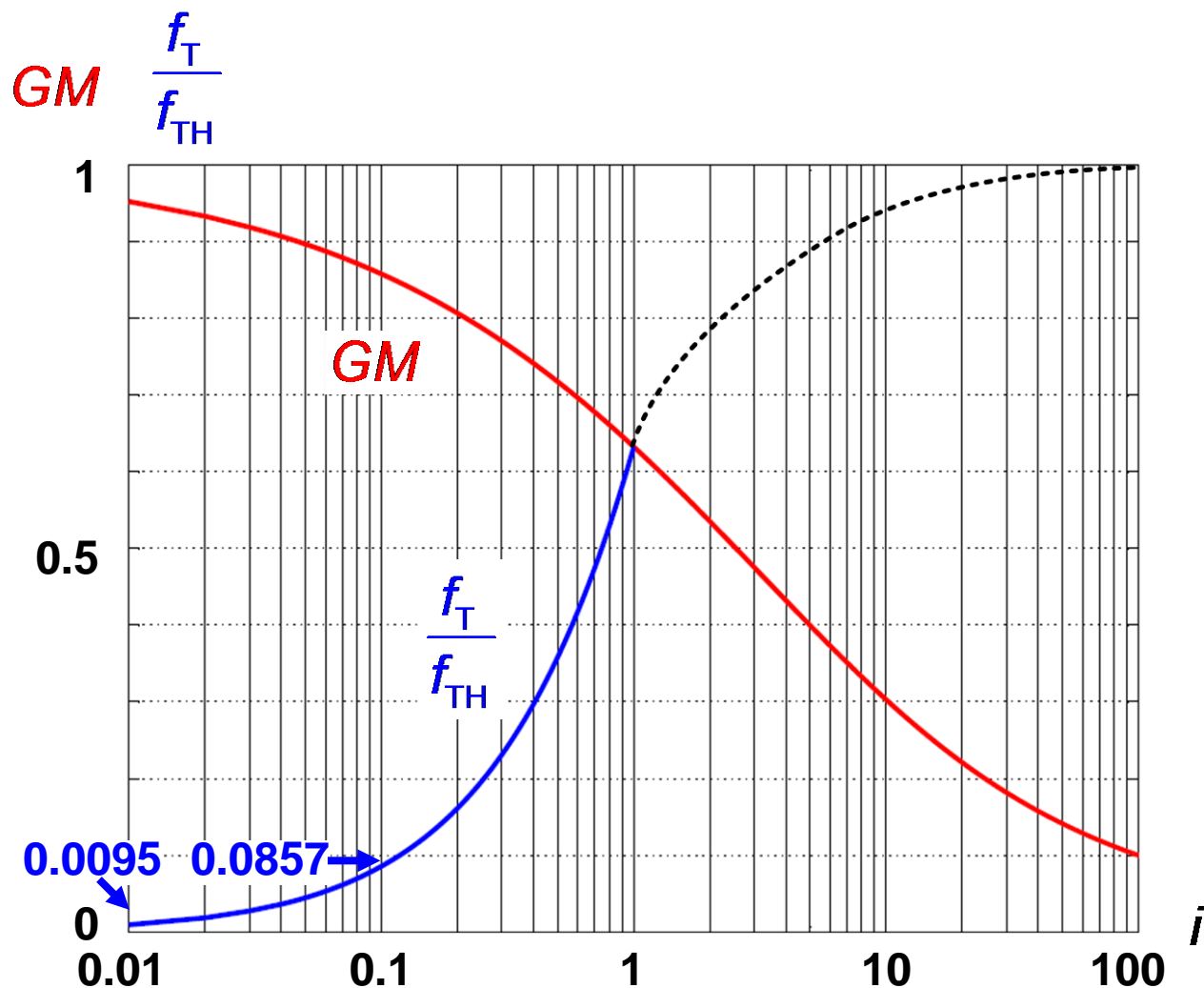
饱和区和弱反型区的特征频率 f_T

$$\left. \begin{aligned}
 GM &= \frac{1 - e^{-\sqrt{i}}}{\sqrt{i}} \\
 I_D &= i \times I_{D,ws}
 \end{aligned} \right\} \begin{aligned}
 g_m &= \frac{I_{D,ws}}{nV_T} \sqrt{i}(1 - e^{-\sqrt{i}}) \\
 \frac{f_T}{f_{TH}} &= \sqrt{i}(1 - e^{-\sqrt{i}})
 \end{aligned} \left. \begin{aligned}
 f_T &= \frac{g_m}{2\pi C_{GS}}
 \end{aligned} \right\}$$

$$f_{TH} = \frac{I_{D,ws}}{2\pi C_{gs} nV_T} = \frac{K' \frac{W}{L} V_{GST,ws}^2}{2\pi \frac{2}{3} WLC_{ox} nV_T} = \frac{3}{2\pi} \frac{\mu V_T}{L^2}$$

当 i 较小时: $\frac{f_T}{f_{TH}} = \sqrt{i}(1 - e^{-\sqrt{i}}) \approx i$

特征频率 f_T 与反型系数 i 的关系



$$\frac{f_T}{f_{TH}} = \sqrt{i}(1 - e^{-\sqrt{i}})$$

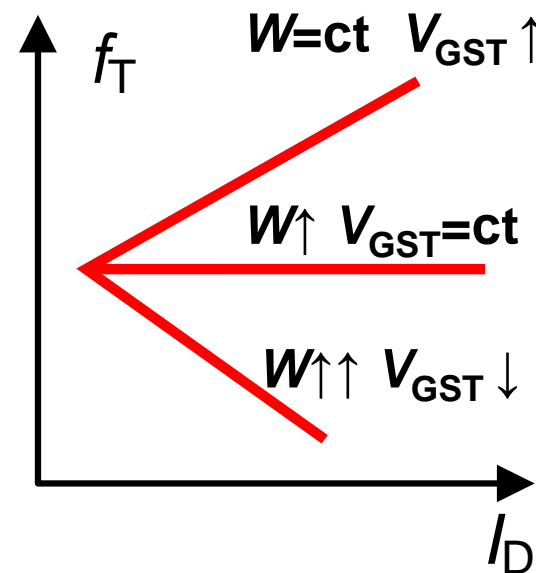
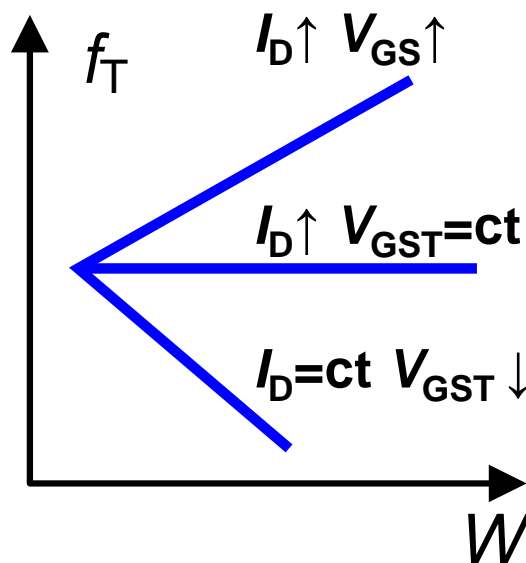
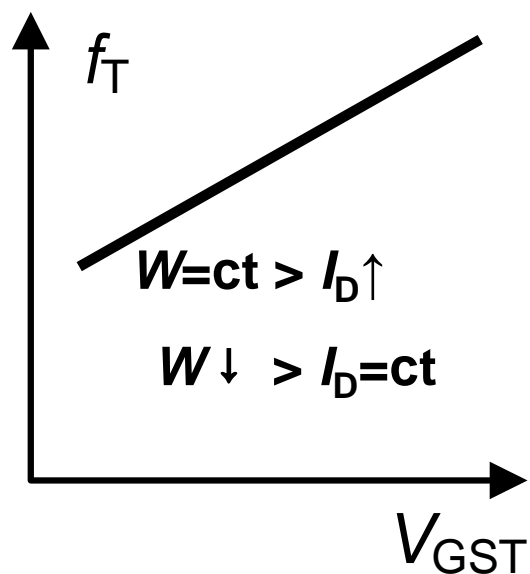
$$GM = \frac{1 - e^{-\sqrt{i}}}{\sqrt{i}}$$

$$i = \frac{I_D}{I_{Dt}}$$

练习3: MOST的特征频率 f_T ?

所有 $L=L_{\min}$

$$f_T = \frac{1}{2\pi} \frac{3}{2n} \frac{\mu}{L_{\min}^2} (V_{GS} - V_{TH,GS}) = \frac{3}{2} \frac{\sqrt{K' I_D}}{\pi C_{ox} \sqrt{WL_{\min}^3}} = \frac{3}{2} \frac{I_D}{\pi WL_{\min} C_{ox} (V_{GS} - V_{TH,GS})}$$



“单页” MOST型晶体管模型

$$I_{DS} = K' \frac{W}{L} (V_{GS} - V_{TH,GS})^2$$

$$K' = \frac{\mu C_{ox}}{2n}$$

$$V_{GS} - V_T \approx 0.2 \text{ V}$$

$$K'_n \approx 100 \mu\text{A/V}^2$$

$$K'_p \approx 40 \mu\text{A/V}^2$$

$$g_m = 2K' \frac{W}{L} (V_{GS} - V_{TH,GS}) = 2\sqrt{K' \frac{W}{L} I_D} = \frac{2I_D}{V_{GS} - V_{TH,GS}}$$

$$r_{ds} = \frac{V_E L}{I_D}$$

$$V_{En} \approx 5 \text{ V}/\mu\text{m}$$

$$V_{Ep} \approx 8 \text{ V}/\mu\text{m}$$

$$f_T = \frac{1}{2\pi} \frac{3}{2n} \frac{\mu}{L^2} (V_{GS} - V_{TH,GS}) \approx \frac{V_{scl}}{2\pi L}$$

$$v_{scl} \approx 10^7 \text{ cm/s}$$

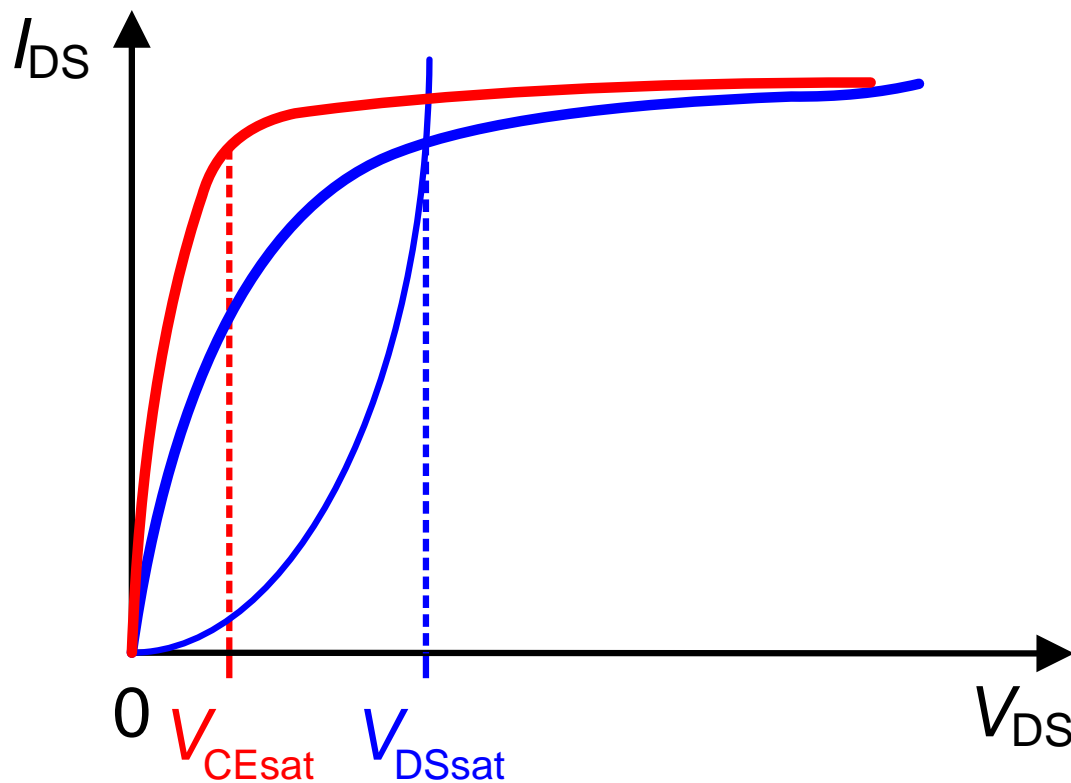
MOS型与BJT型晶体管的比较

表2-8 MOS型与BJT型晶体管的比较

Specification	MOST	Bipolar transistor
1. I_{IN} R_{IN}	0 ∞	I_C/β $\beta ?$ $r_{\pi} + r_B$
2. V_{DSsat}	$V_{GS} - V_{TH,GS} = \sqrt{\frac{I_D}{K' W/L}}$	few V_T
3. $\frac{g_m}{I}$	<div style="display: flex; align-items: center;"> wi $\frac{1}{nV_T}$ </div> <div style="display: flex; align-items: center;"> si $\frac{2}{V_{GS} - V_{TH,GS}}$ </div> <div style="display: flex; align-items: center;"> vs $\frac{1}{V_{GS} - V_{TH,GS}}$ </div>	<div style="display: flex; align-items: center;"> $\frac{1}{V_T}$ $n = 1 + \frac{C_j}{C_{ox}}$ </div> <div style="display: flex; align-items: center;"> $\frac{1}{V_T}$ 4...6 X </div> <div style="display: flex; align-items: center;"> $\frac{1}{V_T}$ </div>

Ref.: Laker Sansen Table 2-8

MOST-BJT的比较：最小 V_{DS}



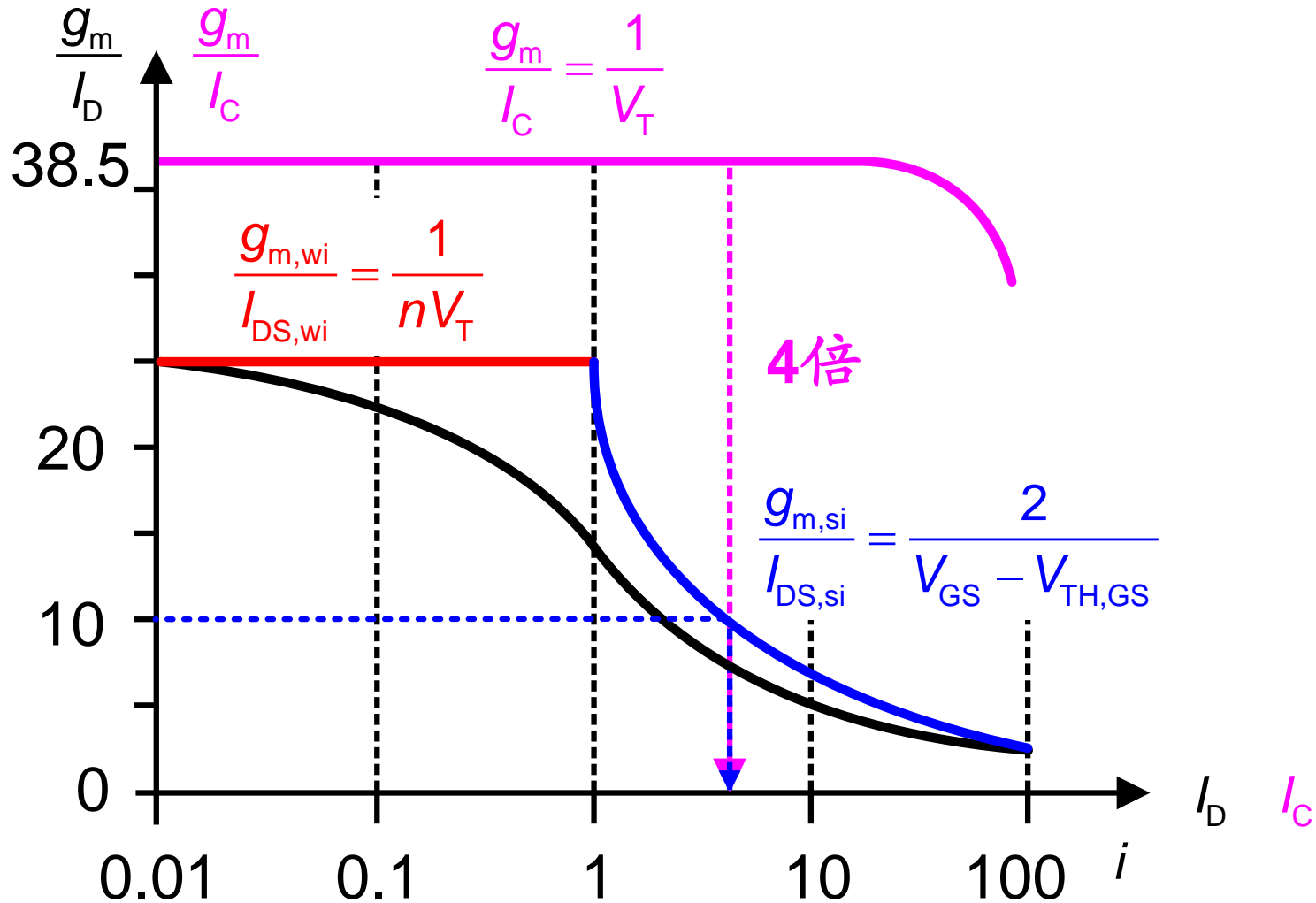
$$V_{DSsat} \approx V_{GS} - V_{TH,GS}$$

$$V_{GS} - V_{TH,GS} \approx \sqrt{\frac{I_D}{K' \frac{W}{L}}}$$

$$V_{CEsat} \approx V_T 'S$$

Ref.: Laker Sansen Table 2-8

MOST-BJT的比较: 能效比 g_m/I_D



g_m 的设计流程

$$I_D = K' \frac{W}{L} (V_{GS} - V_{TH,GS})^2$$

$$g_m = 2K' \frac{W}{L} (V_{GS} - V_{TH,GS}) = 2\sqrt{K' \frac{W}{L} I_D} = \frac{2I_D}{V_{GS} - V_{TH,GS}}$$

2个方程，4个变量 \gg 2个变量不受约束

选择 $V_{GS} - V_{TH,GS}$ 和 L !

MOS型与BJT型晶体管的比较

表2-8 MOS型与BJT型晶体管的比较

Specification	MOST	Bipolar transistor
4. Design planning	$\frac{W}{L}, V_{GS} - V_{TH,GS}$	V_T
5. I -range	1 decade	7 decade
6. Max f_T	low / C_{GS}, C_{GD} high / v_{scl}/L	C_j, C_μ v_{scl}/W_B
7. Noise $\overline{dv_i^2}$	Therm. $4kT(\frac{2/3}{g_m} + R_G)$ 1/f 10X	$4kT(\frac{1/2}{g_m} + R_B)$
8. Offset	10X	$v_{scl} \approx 10^7 \text{ cm/s}$

Ref.: Laker Sansen Table 2-8

关于晶体管模型的参考书目

- ◆ Y. Tsividis, “*Operation and Modeling of the MOS Transistor*”, McGraw-Hill, 1987, Oxford, 2004/2011.

关于模拟电路设计的参考书目

- ◆ P. R. Gray, P. J. Hurst, S. H. Lewis, R. G. Meyer, “***Analysis and Design of Analog Integrated Circuits***”, John Wiley & Sons, 1977/84/93/2001/09
- ◆ T. C. Carusone, D. A. Johns, K. W. Martin, “***Analog Integrated circuit design***”, John Wiley & Sons, 1997/2012.
- ◆ P. E. Allen, D. R. Holberg, “***CMOS Analog Circuit Design***”, Holt, Rinehart and Winston. 1987, Oxford Press 2002/12.
- ◆ B. Razavi, “***Design of Analog CMOS Integrated Circuits***”, McGraw Hill, 2001.
- ◆ K. R. Laker, W. Sansen, “***Design of Analog Integrated Circuits and Systems***”, McGraw Hill, 1994.
- ◆ R. Gregorian, G. C. Temes, “***Analog MOS Integrated Circuits for Signal Processing***”, John Wiley & Sons, 1986.
- ◆ W. M. C. Sansen, “***Analog Design Essentials***,” Springer 2006.